

Addendum to ICSBEP Logbooks 12r, 13r, 14r and 15r for Polyethylene and Graphite Reflected HEU Metal Critical Experiments



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October 2023

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Nuclear Energy and Fuel Cycle Division

**ADDENDUM TO ICSBEP LOGBOOKS 12R, 13R, 14R AND 15R FOR POLYETHYLENE
AND GRAPHITE REFLECTED HEU METAL CRITICAL EXPERIMENTS**

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ABSTRACT

This report documents the experimenters' data sheets that were recently (2023) discovered for critical experiments with highly enriched uranium metal with polyethylene and graphite reflectors. These data sheets were produced at the time of the measurements, when the dimensional inspection reports for the polyethylene and graphite were available. However, at this writing, those inspection reports are not available but may be in unmarked storage for the Y-12 National Security Complex. However, the data sheets presented herein contain sketches of the experimental configurations and other additional information that is not in the logbooks, such as dimensions and masses of the graphite measurements. This report reproduces the experimental data sheets that complement the logbooks. Some of the data on these sheets and the logbooks can be used to infer the dimensions and masses that are not documented. Some obvious mistakes in the logbook and data sheets have been corrected. In the reproduced data sheets, some of the information is not clearly visible: some information, such as average values, can be obtained from other data in the sheets or logbook. This report should be sent to the International Criticality Safety Benchmark Program at Idaho National Laboratory to complement the existing Oak Ridge Critical Facility logbooks there.

1. INTRODUCTION

This report documents the experimenters' data sheets that were recently (2023) discovered for critical experiments with highly enriched uranium (HEU) metal with polyethylene and graphite reflectors that were performed in the early 1960s at the Oak Ridge Critical Experiments Facility (ORCEF). These data sheets were produced at the time of the measurements, when the dimensional inspection reports for the reflector materials were available. However, at this writing, those dimensional inspection reports are not available but may be in unmarked storage for the Y-12 National Security Complex. However, the data sheets presented herein contain sketches of the experimental configurations and other additional information that is not contained in the logbooks, such as the dimensions and masses of the measurement materials. This report reproduces the data sheets that complement the logbooks. Some of the data on these sheets and the logbooks can be used to infer the dimensions and masses that are not documented. Some obvious mistakes in the logbook and data sheets have been corrected. In the reproduced data sheets, some of the information is not clearly shown: some information, such as average values, can be obtained from other readable data on the sheets or the logbook. Three documents related to these experiments have been published: a Y-12 report [1], a journal paper [2], and an ICSBEP benchmark, HEU-MET-FAST-071 [3]. In addition, a three-year effort is underway at the University of Tennessee, Knoxville's Department of Nuclear Engineering, supported by the DOE Office of Nuclear Energy's Nuclear Energy University Programs, to benchmark additional ~80 graphite-reflected critical experiments with HEU metal reflected with graphite greater than 2 in. thickness. This report should be sent to the International Criticality Safety Benchmark Program (ICSBEP) at Idaho National Laboratory to complement the existing Oak Ridge Critical Facility logbooks there. ICSBEP logbooks 12r, 13r, 14r and 15r correspond to ORCEF logbooks E-19, E-20, E-21 and E-22. The publication of this report was supported by Nuclear Data, Criticality Safety, and Radiation Transport Section of ORNL and the DOE/NNSA Nuclear Criticality Safety Program.

2. TYPES OF CRITICAL ASSEMBLIES

Three types of reflected HEU metal cylindrical and annular critical experiments were performed with the vertical assembly machine [4] at the Oak Ridge Critical Experiments Facility: (1) graphite reflected HEU metal assemblies with reflector under 10 in., (2) graphite reflected HEU metal assemblies with reflectors greater than 9 in., and (3) thick polyethylene reflected HEU metal assemblies. For the thick graphite and polyethylene reflected assemblies, the HEU metal and bottom reflector were assembled on the vertical lift

table that was inserted into the top and side reflector. A photograph of a graphite reflected assembly in the disassembled configuration is given in Figure 1. A photograph of an HEU metal polyethylene reflected assembly in the disassembled condition is shown in Figure 2.

Figure 3 shows a photograph of an unreflected uranium metal critical experiment in the disassembled condition from ICSBEP benchmark HEU-MET-FAST-051 [5]; this experiment used the same support structure and assembly procedures as those of the graphite reflected HEU metal experiments with reflectors smaller than 10 in. The low-mass support structure details are documented in an appendix of Reference 6.

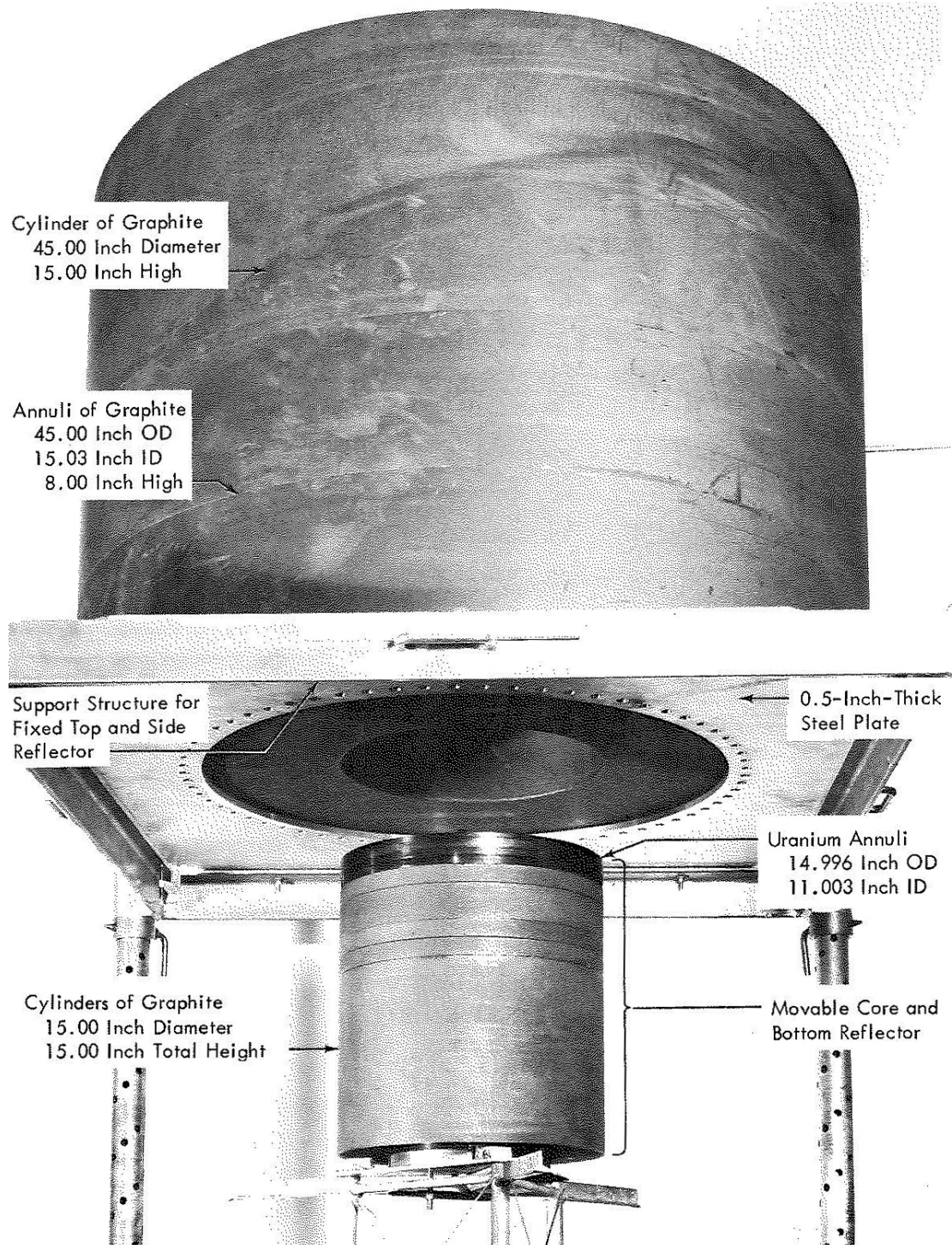


Figure 1. Typical configuration of HEU metal annulus with 15 in. thick graphite reflector on the vertical assembly machine in the disassembled condition. (The upper part of the low-mass lower support is shown under the bottom reflector in this photo.)

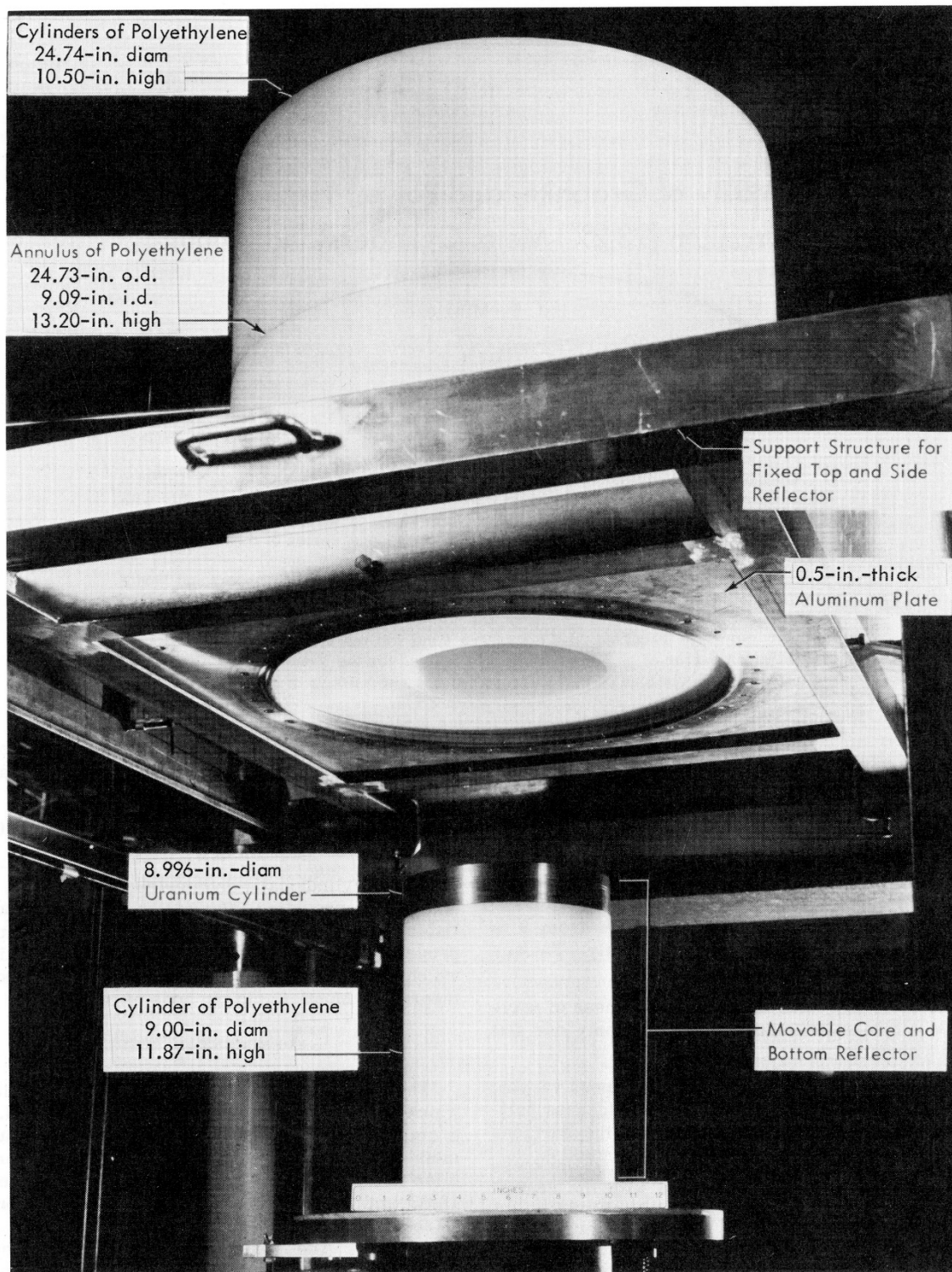


Figure 2. Typical polyethylene reflected HEU metal cylinder in the disassembled condition on the vertical assembly machine at ORCEF. (The upper part of the low mass support structure mounted on the aluminum support table of the vertical lift of the vertical assembly machine at ORCEF is shown in the bottom of this photograph.)

A photograph of an unreflected HEU metal cylinder on the vertical assembly machine with the upper section supported on the thin stainless-steel diaphragm and the lower section on a low-mass support stand is given in Figure 3. For the graphite reflected critical experiments, this support structure was used. The lower section was composed of HEU metal with the bottom and radial reflector, and the top section on the diaphragm consisted of the upper HEU metal and top and radial reflector. For some experiments all the HEU metal was on the upper section and the lower section was bottom reflector.

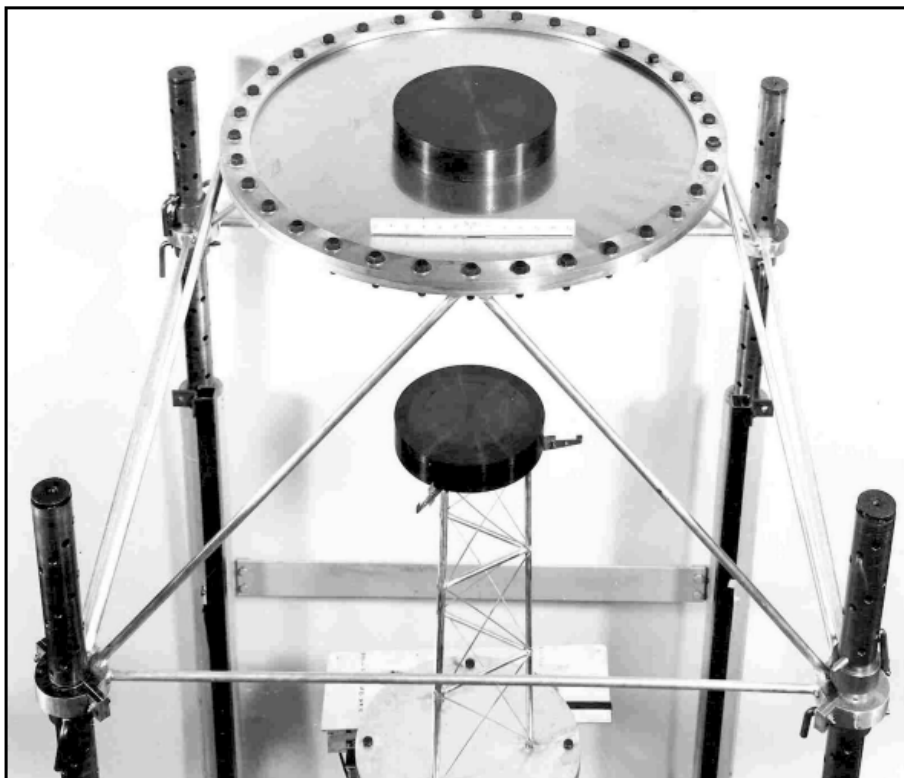


Figure 3. A typical uranium metal assembly for a solid 11 in. diameter uranium (93.14 wt % ^{235}U) metal cylinder of two interacting 11 in. diameter cylinders at close spacing in disassembled condition (from ICSBEP benchmark HEU-MET-FAST-051; this same low mass support structure was used for graphite reflector thickness less than 10 inches).

3. EXPERIMENTERS DATA SHEETS

The file for all experimental data sheets for these experiments is given in Appendix A. The information contained within the experimenters' data sheets is discussed for two examples of two HEU metal system: one with a thin graphite reflector and one with a thick graphite reflector. The discussion of these examples identifies the locations of various information on the data sheets. However, this can vary depending on the data sheet for a particular experiment. In addition, other data sheets can contain other information not in these examples. The experiment data sheets chosen as examples are as follows. (1) A 1 in. thick graphite reflected HEU metal annulus with an outside diameter of 13 in. and inside diameter of 7 in. with void inside the HEU metal. This experiment, which was performed on October 28, 1963, is a repeat of a previous experiment performed on January 25, 1963, with different HEU metal parts. This assembly has been benchmarked in HEU-MET-FAST-071 [3]. (2) An HEU metal cylinder reflected by 12 in. thick graphite reflector. Dimensions given as whole numbers or fractions are nominal. If the dimension contains numbers to the right of the decimal point, they are measured dimensions. Sometimes, a single experimental data sheet contains information for both configurations with both void and graphite inside

the HEU metal. In these cases, on the back side of the experimental data sheet, usually the data for the void assembly is on the left, and that for the graphite in the center is on the right.

3.1 HEU METAL ANNULUS WITH OUTSIDE AND INSIDE DIAMETERS OF 13 IN. AND 7 IN. WITH 1 IN. GRAPHITE REFLECTOR

Copies of back and front of sections of the experimental data sheets are isolated in different figures for discussion.

3.1.1 Top of the Front Page of the Experimental Data Sheet

The top of the front page of the data sheet (Figure 4) contains the experiment title on the upper left, and on the upper right at the top is a reference to the ORCEF logbook, page number and run number. The title of the experiment on the far left is the outer and inner diameter in inches of the HEU metal. In the center is the thickness of the graphite reflector, which in this case is 1 in. "No core" means no graphite in the center of the HEU metal annulus. In this case, the ORCEF logbook is 2 (E-20), page 252 and Run 70. Below this is a drawing of the assembled system. The assembly is divided with an upper section on a diaphragm and a lower section on a low-mass support stand. The diaphragm is designated as a horizontal line on the drawing that extends to the right and left beyond the reflector parts. The experimental geometries are all cylindrically symmetric with the centerline indicated as a dashed vertical line on the right of the assembly sketch.

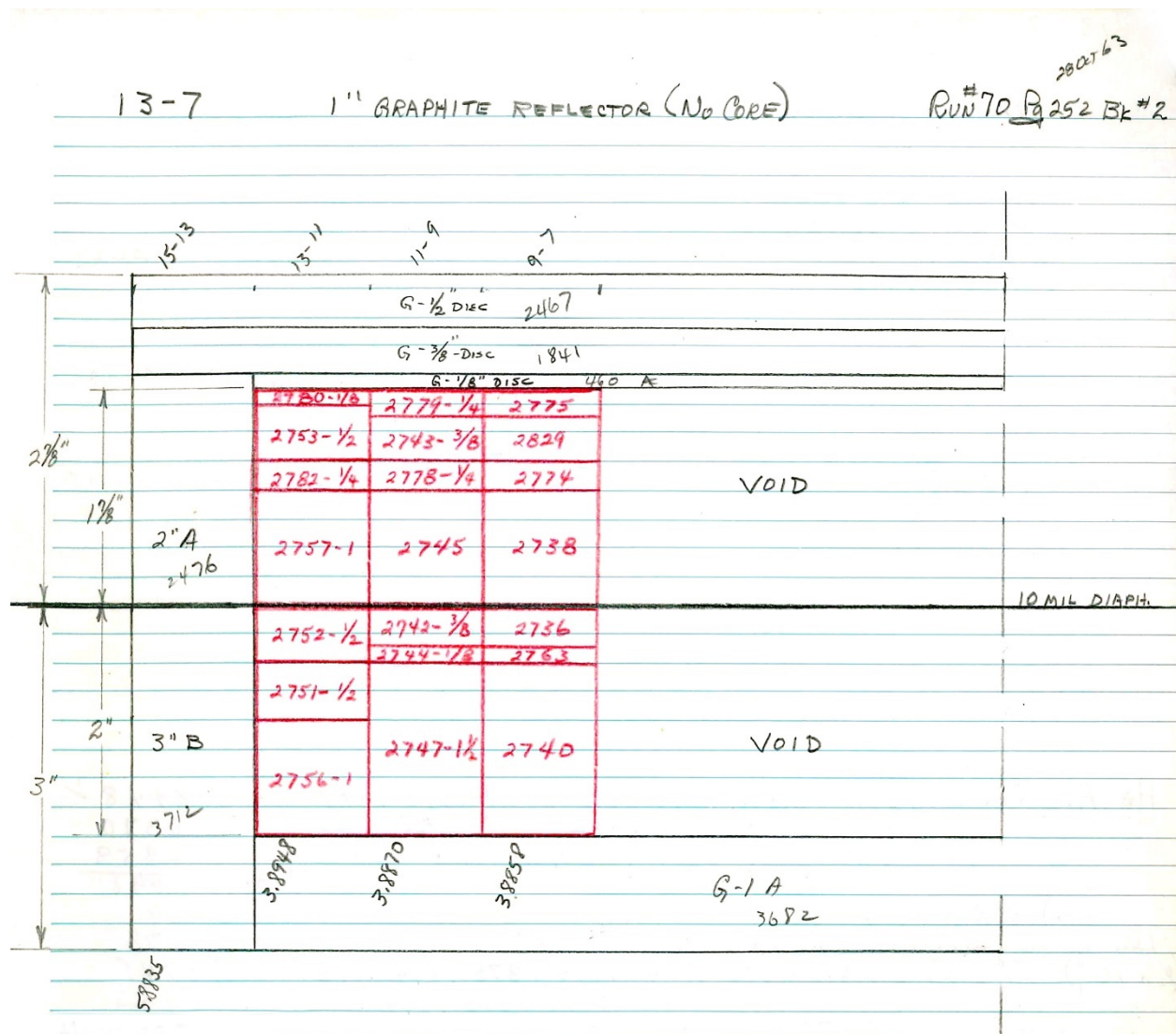


Figure 4. Title, logbook, run number (sometimes), and page number and sketch of the assembled system. (Red indicates HEU metal.)

There is usually a variety of information on the sketch. The HEU metal parts are outlined in red, and their numbers are designated in red. In this sketch, after the four-digit part numbers are some fractional thicknesses. For some of the drawings, the identification of the HEU metal parts provides only the last two or last four digits of the part number. Below the HEU metal parts in red, there are sometimes the measured (obtained as described in reference 6) height of a particular section of the HEU metal parts. For example, for the 13-11 annular HEU metal section, the measured height is 3.8948 in. Measured heights of stacks of HEU metal or graphite do not include the diaphragm thickness. The materials not designated in red are graphite parts. The annular sections of the experiment are labeled on top of the sketch: in this case, 15-13, 13-11, 11-9, and 9-7, where these numbers are the outside and inside diameter of the HEU metal region. The nominal thicknesses of the graphite parts are given as whole numbers or fractions. If there more than one graphite part of the same dimensions was available, an additional letter was added to the thickness—for example 3" A. Within the sketch of each graphite part is a number that gives the mass of the part in grams to an uncertainty of 0.5 grams. For example, the reflector mass of the bottom 13 in. OD graphite reflector cylinder on the lower support structure is given as 3682 grams on the lower support stand. In some sketches like this one, the total measured heights of the HEU metal sections (sum of

heights on lower support stand and on the diaphragm) are given under the HEU metal sections in the bottom reflector. For example, in this sketch, the average measured height of the 13 in. OD, 11 in. ID HEU metal ring is 3.8958 in. using the procedures for height measurement described in HEU-MET-FAST-051 [5]. There may be other notes on the sketch that provide other information such as the actual measured thickness of the graphite parts. Some nominal heights are given on the far left of the sketch and are indicated by arrows. For this sketch, the measured height of the 15-13 annular graphite section on top and bottom is 5.8935 in. The sketch may also contain letters such as A, B, C, etc. with arrows that indicate height measurements for sections of the assembly, with the numerical values given on the back of the data sheet. These multiple thickness measurements are given, most of the time with an average value that is sometimes not readable even with a magnifying glass. In these cases, the average can be calculated from the multiple individual thicknesses. For some of the 15 in. thick graphite reflected systems, it is easier to consult the logbook for the HEU metal part stacking.

3.1.2 Other Information under the Sketch on the Front of the Data Sheet

Information on the masses and volumes is given on the front of the data sheet, below the sketch of the assembly. The numbers on the data sheets have too many significant figures beyond the decimal point, but that is the way they were listed at the time of the measurements. A typical bottom of the front page of an experimental data sheet is given in Figure 5 for the measurement shown in Figure 4.

MASS OF TOP FUEL = 54,246 gm	TOTAL = 112.138 Kg
BOTTOM = 57,892	
MASS OF TOP GRAPHITE = 7,244	TOTAL = 14.638 Kg
BOTTOM = 7,314	
AVG O.D. (w't'd) ALL FUEL = 12.99616"	168.900174
AVG I.D. (w't'd) ALL FUEL = 7.00307"	49.042989
	3.889797
AVG Ht (w't'd) ALL FUEL = 3.890064	
FUEL Vol = 6000.4790 cm ³	
FUEL ρ = 18.6881 gm/cc	
Vol of graphite = 8582.05072 cm ³	
ρ = 1.70565 gm/cc	
Aug Refl = 0.999"	

Figure 5. Information below the sketch on the front of the experimental data sheet.

On this data sheet, the mass of HEU metal in the top section (54,246 g), the mass of HEU metal in the bottom section (57,892 g), and the total HEU metal mass (112,138 g) are given. On this data sheet, the mass of the graphite in the top section (7,244 g), the mass of graphite in the bottom section (7,314 g), and the total graphite mass (14,636 kg) are given.

In some of the drawings, the HEU metal part numbers may not be legible. Masses given can sometimes be used to determine the unknown part's mass: for example, the case in which there are just three parts in an assembly and two of them are clearly marked. The known masses of the two identified parts can be subtracted from the total mass to obtain the mass of the unknown uranium part number. The masses listed in descriptions of the HEU metal parts for the subtracted masses can be observed to determine the unknown part number by searching for a part in the list of HEU metal parts with the subtracted mass. For experiments after January 1965, most of the 7 in. diameter cylindrical parts had 0.375 in. diameter holes that were filled with 0.0365 in. diameter HEU metal plugs. In these cases, the fuel mass given on the front of the data sheet shows the addition of these masses with the total from the major parts to give the total mass of the assembly. The total volume of the HEU metal was and can now also be calculated from the descriptions of the HEU metal parts from the inspection report data included in reference [6]. With the total HEU metal mass and volume, an average density can be calculated for the assembly and is included on the front of the experimenters' data sheet. The average OD and ID of this HEU metal assembly with the weighted average calculated with the inner and outer part heights as weights were 7.00307 and 12.99599 in., respectively. For some reason, the square of these diameters is also given—not on this data sheet but on others.

The next item down on the data sheet is the volume of the HEU metal (designated as *Fuel* in the data sheet) of 6000.479 cm³. These are extremely accurate because the dimensions of the HEU metal parts are measured to 0.0001 in. [6]. Calculation of the HEU metal density for this experiment yields 18.6881 g/cm³.

At the time these experimental data sheets were prepared, the dimensional inspection reports for the graphite were available. Using these inspection report dimensions, the volume of the graphite was calculated and included on these data sheets. These volumes can be used to verify the assumed dimensions of the graphite parts in cases where they were not measured. These volumes can also be used in some cases to determine the dimensions. Using the graphite masses and the graphite volume, an average graphite density can be calculated: for this assembly, it was 1.68457 g/cm³. At the very bottom of this data sheet is an average reflector thickness.

3.1.3 Information on Top of the Back of the Data Sheet

A copy of the top of the back of an experimental data sheet is shown in Figure 6.

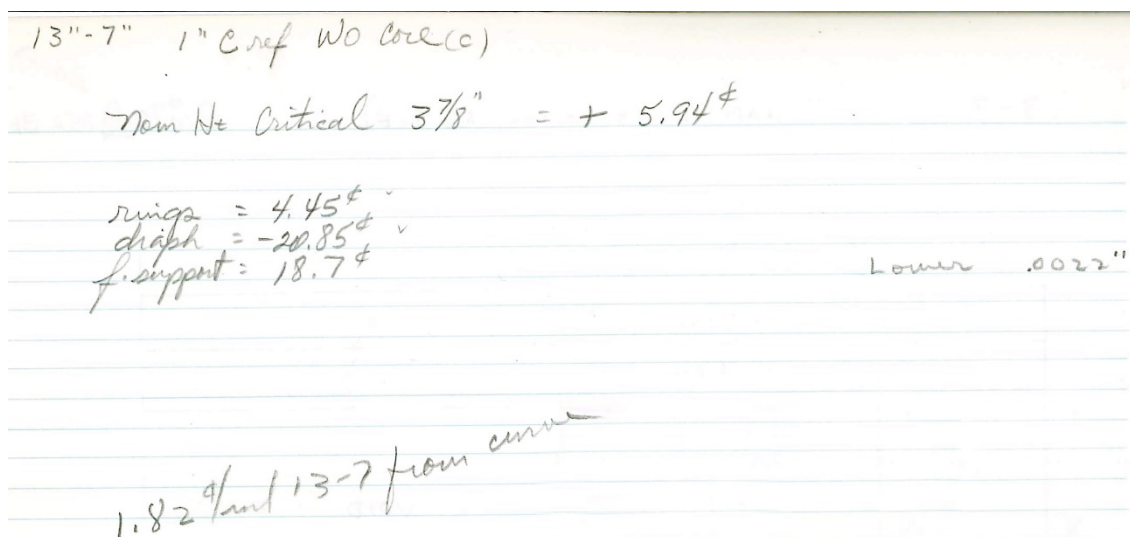


Figure 6. Information from the top of the back of the experimental data sheet.

The experiment identification is given at the very top, followed by the nominal height and the measured reactivity of the experimental configuration. The various reactivities that were measured are usually given in this part of the data sheet.

On this sheet, just below the nominal critical heights were the change in reactivities associated with the support structure, which consisted of the support ring for the stainless-steel diaphragm, the stainless-steel diaphragm that supported the upper section of the assembly, and the lower support structure. The removal of the support ring and the lower support stand reduced the reactivity because they reflect neutrons back into the assembly. The removal of the diaphragm increases the reactivity because the lower HEU metal gets closer to the upper portion. To evaluate these effects, a lower support stand was added to the top of the top reflector (supported by a crane adjacent to the top reflector but not touching it). To evaluate the diaphragm support ring, its thickness was doubled. The associated reactivity changes were + 4.45 cents for the addition of the diaphragm support ring, -20.85 cents for the doubling of the diaphragm thickness, and +18.7 cents for the addition of the support stand. Thus, the net change in reactivity associated with removal of the support structure was 2.3 cents. A correction should be made to the reactivity of the diaphragm because the effect is not linear with thickness, as demonstrated by other measurements [7]. This correction can be determined from calculations.

On this experimental data sheet, the next item down was an estimate of the reactivity as 1.82 cents per mil (0.001 in.).

Next down the page are the reactivity effects of changing the HEU metal heights of each radial section of the assembly, usually by 1/32 in. For this assembly, increasing the HEU metal height 1/16 of an inch increased the reactivity of the 9-7 ring, 11-9 ring, and 13-11 ring increased the reactivity 36.32, 39.17, and 26.80 cents, respectively for a total value of 102.39 cents. Adjacent to these measurements, the results are sometimes given in cents per thousandth of an inch or cents/mil. A measurement was performed for increasing the height of the annular 15-13 graphite ring around the HEU metal, and an estimate is given below these fuel values of 0.024 cents per mil.

3.1.4 Information on the Bottom of the Back of the Data Sheet

A copy of the lower half of the back of the experimental data sheet is shown in Figure 7.

$$\begin{array}{l}
 \text{Ht AEL FUEL } 13-11: 3.895, 3.893, 3.895, 3.894, 3.895, 3.897 = 3.8948 \checkmark \\
 11-9: 3.885, 3.886, 3.885, 3.887, 3.891, 3.888 = 3.8870 \\
 9-7: 3.887, 3.887, 3.885, 3.885, 3.886 = 3.8858 \\
 \text{w avg} = 3.8898'' \\
 2''A + 3''B = 5.009'' = 5.009 \\
 \text{High fuel ring} + (1 \times 13 \text{ disc}) + (1/8 \times 13 \text{ disc}) = 5.0178 = 5.0178 \\
 (1/2 \times 15'') + (3/8 \times 15'') = 0.875, 0.875, 0.874, 0.874, 0.875, 0.874, 0.875 = 0.8745 \\
 \text{sum} = 5.8923 \\
 \text{EVEN FUEL HT.} = 3.8898'' \\
 \text{SKY HOOK REACT.} = +3.64\% \\
 \text{O Reactivity Ht} = 3.8876'' \checkmark \\
 \text{React} = \text{---} = +5.94\% \\
 \text{all support} = -2.30 \\
 13-7 = \text{---} = 0 \\
 \text{---} = +3.64 \\
 O = 3.8898 - 0.0020 = 3.8878''
 \end{array}$$

Figure 7. Bottom section of the back of the data sheet.

In this section of the lower back of the data sheet, the measurements of the height of the different radial HEU metal sections and graphite sections are given. Each HEU metal section (both that on the diaphragm and the lower support stand) and measurements made at various azimuthal positions (in this case, six measurements) are given as described in reference [3], and the values are averaged. The measurement for this configuration were as follows: for the 13-11 HEU metal ring 3.895 three times, 3.894 and 3.897 for an average of 3.8948 in.; for the 11-9 HEU metal ring 3.885 twice, 3.886, 3.887, 3.891, 3.888 and an average of 3.8870 in.; for the 9-7 HEU metal ring 3.887 twice, 3.885 three times, and 3.886 for an average of 3.8858 in.

From these data, measured heights of the individual sections and the sum of the HEU metal part heights from the inspection reports can be used to obtain the average gap between parts vertically by subtracting the sum from the measured height and dividing by one less than the number of parts in the section.

Below the HEU metal section measurements are some dimensional measurements for the graphite parts. On this data sheet, the height of the two annular side reflectors is given as 5.009 in. Looking at the sum of the measured heights of these two parts as 5.0073 from the inspection reports available at the time of the measurements, there is a gap of 0.0017 in. between annular graphite parts, vertically.

Below these measurements is the measured height of the sum of the heights of the 13-11 HEU metal plus the height of the graphite part below it and the 0.125 in. thick metal ring: 5.0178 in. These two values were copied onto the data sheets from the dimensional inspection reports available at the time of the measurements and at the present time are only recorded here. On many data sheets it is stated that these parts are looked up, which means the values come from the inspection reports available at the time of the measurement.

Below this, measurements are given for the total height of the two 15 in. diameter parts of the top reflector: 0.875 four times and 0.874 three times, for an average value of 0.8746 in. At the bottom of the page on the left is an HEU metal height corrected to 3.8898 in. with a reactivity estimate of +3.64 cents above delayed critical. Below that is a height estimate for the assembly with an even height of 3.8876 in.

and exactly at delayed critical ($k_{eff} = 1$). On the bottom right, partially circled in red are the calculations to obtain these values.

On the right of this average is the difference between the measured height and the sum of the parts, or 0.026 in. So, the sum of the individual heights is 5.756 in. This annular section consists of three parts with existing measured heights. For the two parts with nominal heights of 2 and 3 in., the actual heights are known to be 2.0042 and 3.0030 in. Subtracting these two values from 5.756 in. gives the height of the remaining part as 0.749 inches. This is an example of how presently known data can be used to determine the presently unknown thickness of a part.

3.1.5 Information at the Bottom of the Back of the Data Sheet

This information can vary depending on the data sheet. For this particular data sheet, the reactivity of an even HEU metal height with no support structure as 3.8263 in. with a positive reactivity of +40.35 cents. This was determined from the reactivities measured as the HEU metal height was varied and from the correction for the support structure. Also given are some calculations that give a flat height of the HEU metal and graphite core at exactly delayed critical with a height of the fuel and graphite of 3.8074 in.

3.2 EXPERIMENT WITH A THICK GRAPHITE REFLECTOR

The experiment chosen as an example is a 12 in. thick graphite reflected HEU metal annulus with an OD of 11 in. and ID of 0 in. Items on the experimental data sheet discussed in Section 3.1 will not be repeated in discussion in this section, but the top and bottom sections of the front and back of the data sheet are presented.

3.2.1 Sketch of the Assembly

The sketches on this data sheet for the thick reflected experiments (Figure 8) are closer to scale. As a result, the last two digits of the HEU metal parts numbers are sometimes not given and not readable without a magnifying glass. In these cases, the logbook can be consulted for most experiments for a more enlarged drawing of the HEU metal section.

1" DIA CYL. (SOLID) ; 12" GRAPHITE REF.

4-112

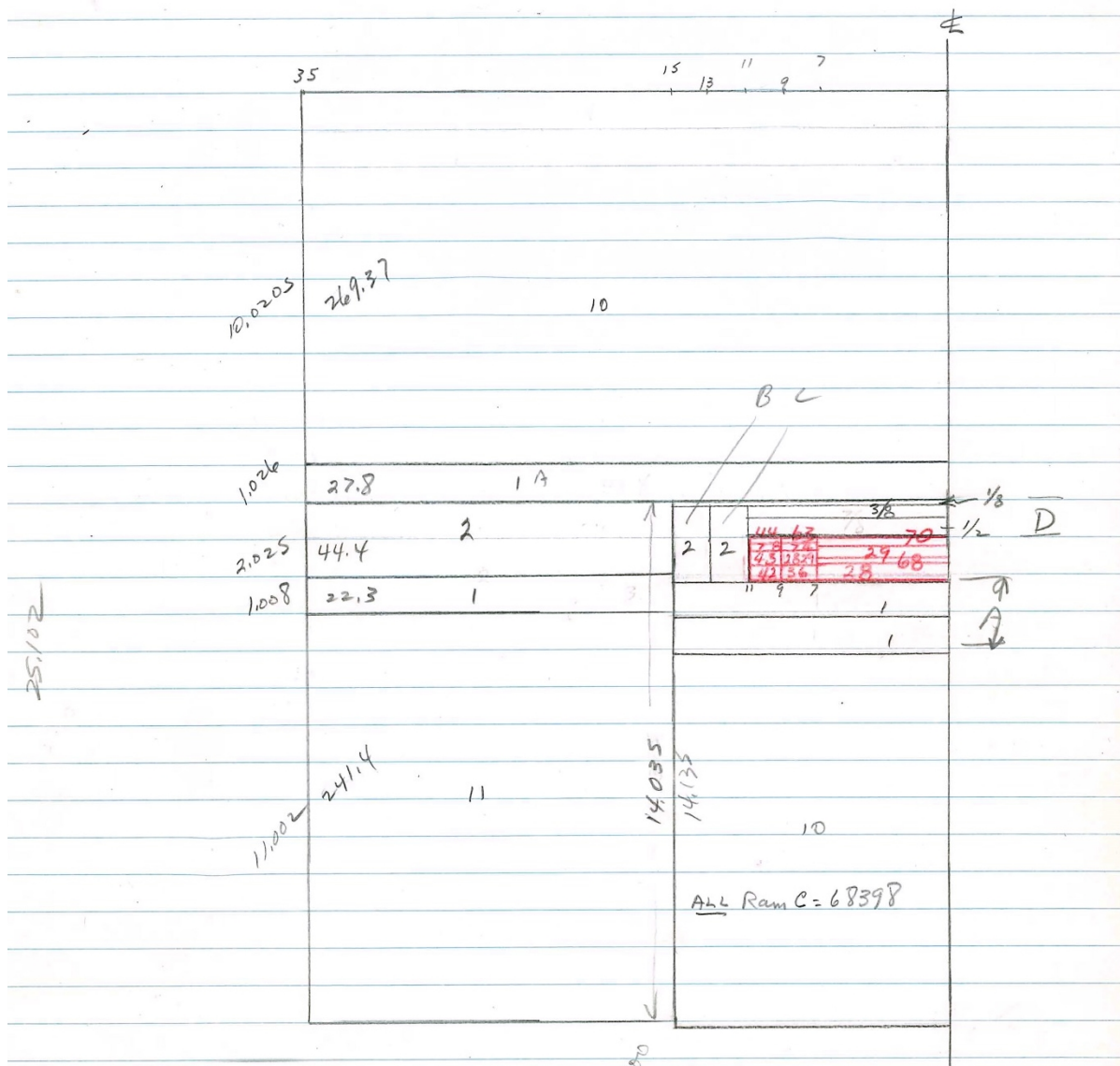


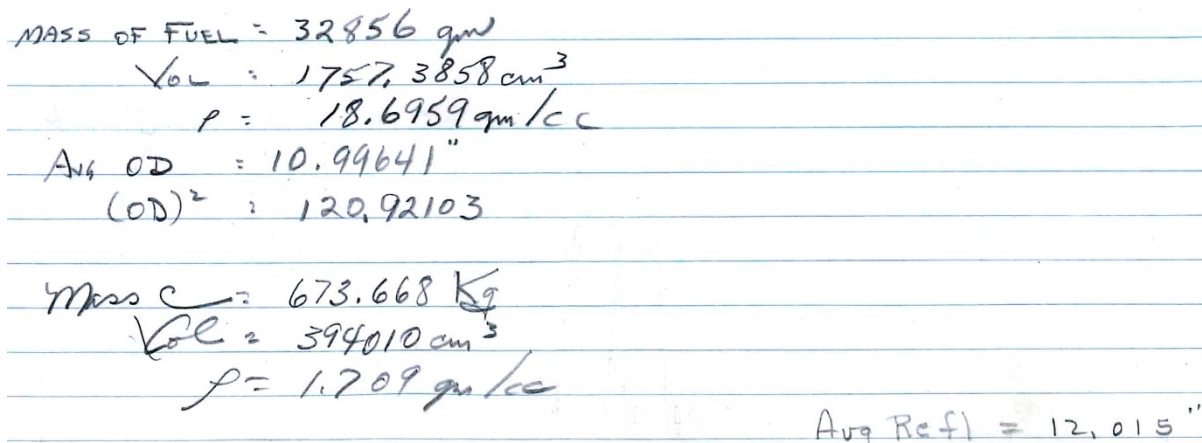
Figure 8. Sketch of the 11 in. diameter HEU metal cylinder with 12 in. thick graphite reflector.

On the far left of the sketch is the measured height from the bottom of the side reflector to the top of the top reflector. This measurement, with the thicknesses of the top and side reflector parts, can be used to determine the average gap between the top and side reflector parts. Nearly adjacent to the top and side reflector boundary are measurements of the thickness of the top and side reflector parts from the then available dimension analysis reports. For example, for the thicknesses at the boundary between the bottom reflector on the vertical lift and the side reflector, there are two measured heights. One is the measured height on the side reflector (14.035 in.), and the other is the measured height (14.135 in.) of the material on the vertical lift. The material on the vertical lift is slightly higher than the side reflector. As a result, on the assembly, the bottom of the bottom reflector protrudes slightly below the bottom of the side reflector.

On this sketch are certain capital letters that indicate measured heights for individual or combinations of parts such as A, B, C, and D. These results are given on the back of the experimental data sheets.

3.2.2 Information below the Sketch on the Front of the Experimental Data Sheet

The information below the sketch is of the same type as that described in Section 3.1.2 Figure and will not be repeated here.



MASS OF FUEL = 32856 gm
Vol = 1757.3858 cm³
ρ = 18.6959 gm/cc
Avg OD = 10.99641"
(OD)² = 120.92103

Mass C = 673.668 Kg
Vol = 394010 cm³
ρ = 1.709 gm/cc

Avg Refl = 12.015"

Figure 9. Information below the sketch on the front of the experimental data sheet below the sketch.

3.2.3 Information on Top of the Back of the Data Sheet

A copy of the top of the back of an experimental data sheet is shown in Figure 10. Some additional information appears on the back, such as the reactivities associated with 1/32 in. changes in height of two of the HEU metal ring sections, the 11-7 in. and the 9-7 radial sections. The change in height of the HEU metal in the center section was too large to measure.

Next down the page are reactivities associated with the addition of graphite to the top graphite reflector. Adding a 35 in. OD, 15 in. ID, 0.525 in. thick graphite section increased the reactivity 10.52 cents: adding 15 in. OD, 0 in. ID, 0.25 in. thick graphite cylinder inside the previous addition increased the reactivity another 7.02 cents: then adding an additional 15 in. OD, 0 in. ID, 0.5 in. thick on top of the previous addition increase the reactivity another 11.81 cents.

Next are the height of the three radial sections of HEU metal, discussed in a previous section of this report.

Next down the page are the measured heights of various sections of graphite reflector. Section A consists of two pieces of bottom reflector with a thickness of 2.0022 in., which were measured for another measurement on Page 124 of ORCEF logbook 4 (E-22). Annular section B consists of one annular graphite part whose height was looked up in the dimensional inspection reports available at the time of the measurements and was 2.0043 in. Annular section C consists of one annular graphite part whose height was looked up in the dimensional inspection reports available at the time of the measurements and was 2.0020 in.

On top of the HEU metal were three 11 in. diameter graphite cylindrical parts with five measured thicknesses: 1.002 three times and 1.001 twice for an average value of 1.0016 in. (average is a correction of the data sheet).

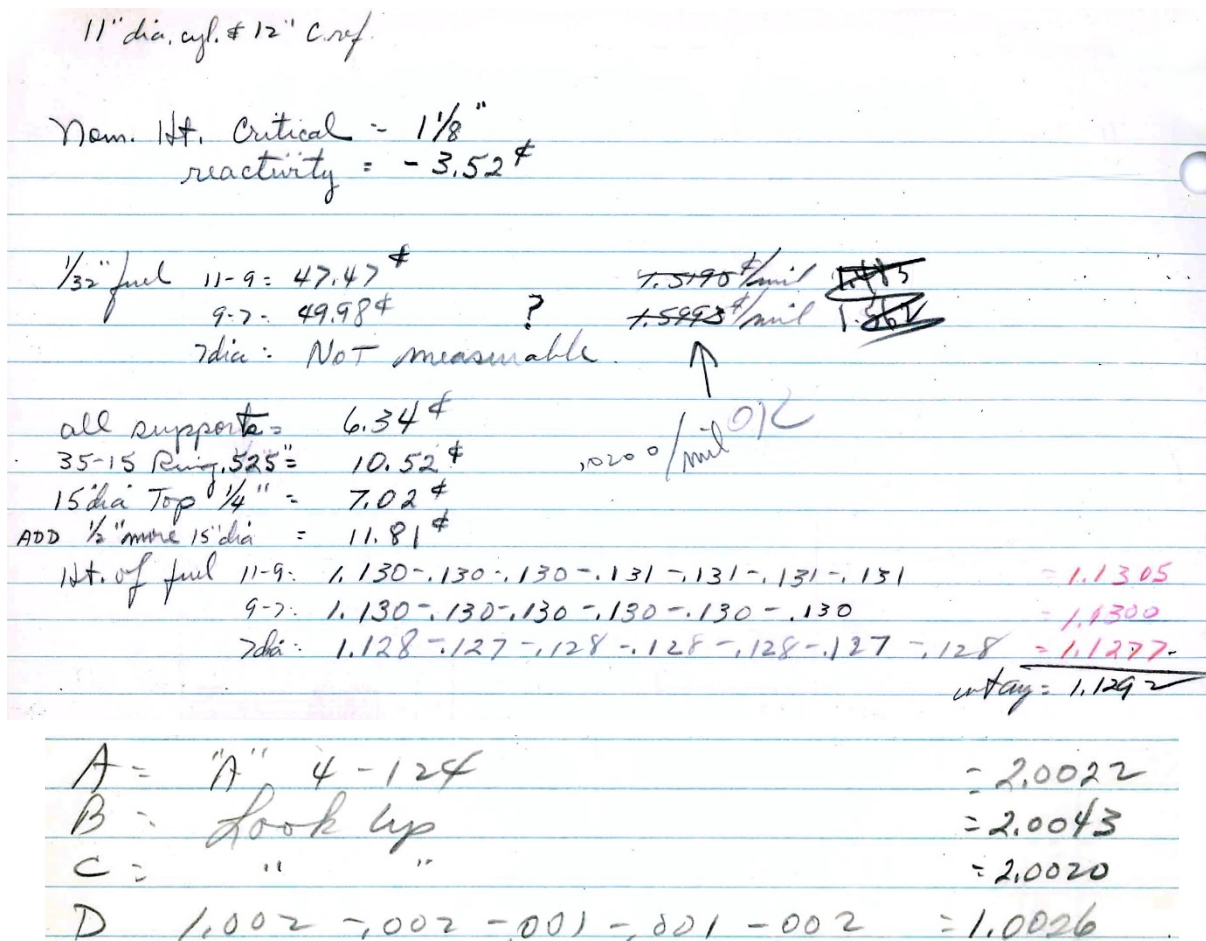


Figure 10. Information from the back of the experimental data sheet.

4. CONCLUSIONS

This report documents experimental data from the experimenters' data sheets filled out at the time of the measurements when all inspection reports were available. The report described in detail the information on two data sheets. The HEU metal used for the experiments was well documented in previous reports. Not all the dimensional analyses for the graphite parts are presently available, but some of it can be obtained from these experimental data sheets. These dimensional analyses may be in unmarked boxes in Y-12 storage and are not retrievable at this time. This report presents experimental data such as some masses and dimensions not in the logbooks (ORCEF logbooks E-19, E-20, E-21, and E-22).

5. REFERENCES

1. J. T. Mihalcz, "Graphite and Polyethylene Reflected Uranium-Metal Cylinders and Annuli", Y/DR-81, Union Carbide Corp. Nuclear Division, Oak Ridge Y-12 Plant (April 1972).
2. J. T. Mihalcz, "Criticality of Graphite- and Polyethylene-Reflected Uranium (93.2) Metal Cylinders and Annuli," *Nucl. Sci. Eng.*, 49, 489-504 (1972).

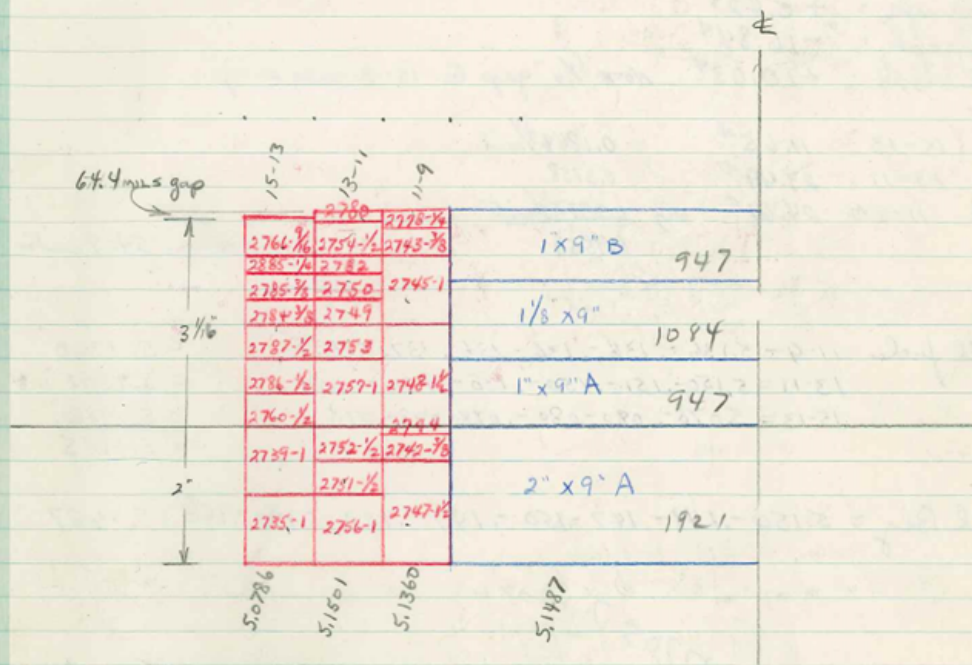
3. Shane E. Parkey, John T. Mihalczo, Raymond L. Reed, “Uranium (93.14) Metal Annuli with One-And Two-Inch Graphite Reflectors”, NEA/NSC/DOC(95)03/II Volume II, HEU-MET-FAST-071 (2006).
4. “Oak Ridge Critical Facility Operating Procedures” Oak Ridge Y-12 Plant (Y-12), Oak Ridge, TN (United States) Y/DR-54 (1971) [OSTI #1894661].
5. Robert H. Elwood and John T. Mihalczo “Uranium (93.2) Metal Cylinders (7-inch, 9-inch, 11-inch, 13-inch, 15-Inch Diameter Cylinders and Two 11-Inch Diameter Interacting Uranium (93.2) Metal Cylinders” NEA/NSC/DOC(95)03/II Volume II, HEU-MET-FAST-071 (2006) HEU-MET-FAST-051 (2002).
6. John T. Mihalczo, “Three Delayed Critical 15-inch-Diameter Interacting Enriched (93.14) Uranium Metal Cylinders without Moderator and Reflector” ORNL/TM-2019/1456 (Dec 2020) [OSTI #1735460].
7. John T. Mihalczo, “Uranium-Molybdenum Alloy Critical Experiment for the Health Physics Research Reactor” ORNL/TM2021/2234 (June 2022) [OSTI #1887715].

APPENDIX A.

This appendix contains copies of all the experimenters' data sheets prepared at the time of the measurements, when all the inspection reports were available. Some of the data on these data sheets are not available in the logbooks. Any errors in the data on the sheets have not been corrected but can be resolved by information in the logbooks.

15"-9" BARE + POLYETHYLENE CORE

Pg 71



MASS TOP FUEL = 107711 gm
BOTTOM = 69346 gm

TOTAL = 177.057 Kg

MASS TOP POLY = 2978 gm
BOTTOM = 1921 gm

TOTAL = 4.899 Kg

AVG. O.D. ALL FUEL (O.T.D) = 14.99505"
AVG. I.D. ALL FUEL (W.T.D) = 9.00215"

OD² = 224.85152
ID² = 81.03870

FUEL VOLUME = 9473.86788 cm³
 ρ = 18.68898 gm/cc

POLY VOLUME = 5370.12870 cm³
 ρ = 0.912268 gm/cc

15-9 $\frac{1}{16}$ " Poly Core

Mem. Wt. Critical $15-13 = 5\frac{1}{16}"$
 $13-9 = 5\frac{1}{8}" = +33.58^{\#}$

Rings = $+5.42^{\#}$

Druph = $-16.84^{\#}$

S. Stand = $+10.03^{\#}$ NOTE $\frac{1}{16}"$ gap @ 15-13 area only

$\frac{1}{16}"$ 15-13 = $11.65^{\#}$ $0.1864^{\#}/\text{mil}$

$\frac{1}{16}"$ 13-11 = $23.49^{\#}$ 0.3758

$\frac{1}{16}"$ 11-9 = $24.61^{\#}$ or $0.3937^{\#}/\text{mil}$
 0.9559

reduce 54.9 mils

Wt. all fuel	11-9 = 5.136 - .136 - .136 - .136 - .1375 - .135	= 5.1360"	+12.7
	13-11 = 5.150 - .151 - .150 - .150 - .150 - .150	= 5.1501"	- 1.4
	15-13 = 5.078 - .080 - .080 - .078 - .078 - .078	= 5.0786"	+70.1
		= 5.1185"	

Wt all Poly = $5.150 - .141 - .147 - .150 - .147 - .152 - .150 - .146 = 5.1487$

$5.1185 = 177.05^{\#}$
 $34.59157 \text{ Kg}/\text{in}$

EVEN FULL HT = $5.1487"$

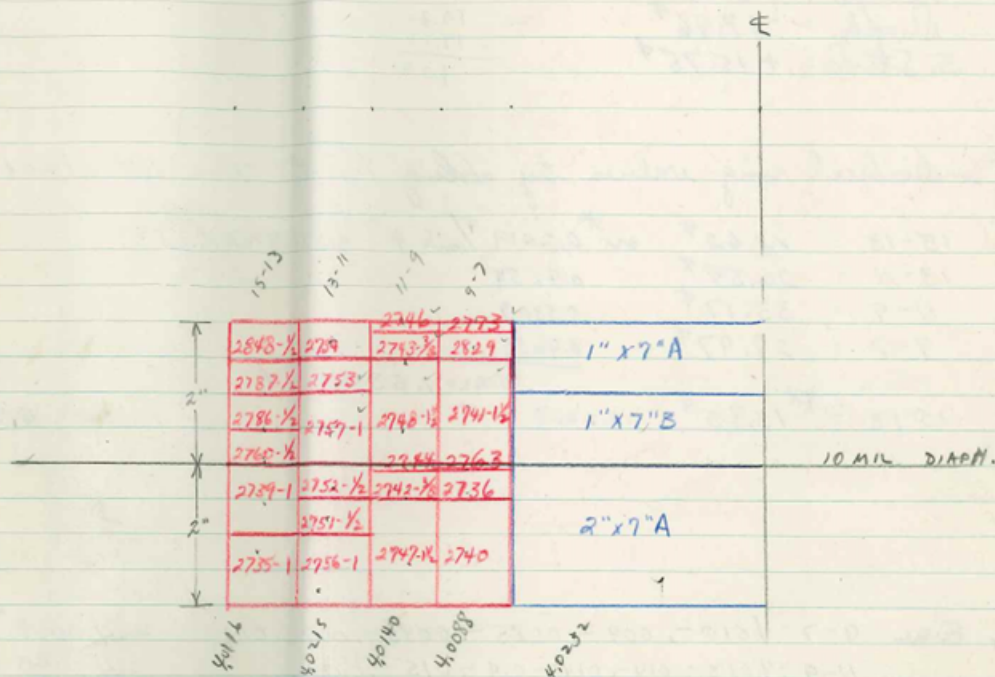
SKY Hook REACT = $+52.51^{\#}$

-1.8990 Kg

Or reactivity = $5.0938"$ (not consid. poly)

15" - 7" BARE + POLYETHYLENE CORE

Fig 74



MASS OF TOP FUEL = 84925 gm
BOTTOM 84762 gm

TOTAL = 169,687 Kg

MASS OF TOP POLY = 1163 gm
BOTTOM = 1163

TOTAL POLY MASS = 2.326 Kg

AVG I.D. ALL FUEL (WIT'D) = 7.00258"
AVG O.D. ALL FUEL (WIT'D) = 14.99493"
AVG HT. ALL FUEL (WIT'D) = 4.01434"

FUEL VOLUME = 9083.5743 cm³
FUEL ρ = 18.68064 gm/cc
CORE VOLUME (mech ID) = 2539.1101 cm³
CORE ρ = 0.91607

15-7 Bare + Poly Core

Nom. Ht. Critical = 4" + 4.51¢ reactivity

Rings : + 3.55¢
 Graph : - 17.96¢
 S. Stand : + 15.75¢

$$\begin{array}{r} 19.80 \\ - 17.96 \\ \hline 1.84 \end{array}$$

Get individual ring values by adding $1/16$ " to Nom. Ht. above.

+	$1/16$ "	15-13 :	12.62¢	or	* 0.2019 ¢/mil + ** 0.2208 = Avg. 2113
+		13-11 :	26.59¢		0.4254
+		11-9 :	33.17¢		0.5307
+		9-7 :	28.97¢		0.4635

TOTAL = 1.6309 ¢/mil

- $1/16$ " 15-13 : ** 13.80¢ 0.2208

reduce 10.9 mils

ALL FUEL	9-7 =	4.010 - .009 - .0085 - .0085 - .007 - .010	=	4.0088"	+14.4
	11-9 =	4.013 - .014 - .014 - .014 - .015 - .014	=	4.0140	+9.2
	13-11 =	4.022 - .021 - .020 - .020 - .023 - .023	=	4.0215	+1.7
	15-13 =	4.010 - .013 - .013 - .010 - .012 - .012	=	4.0116	+11.6
				4.0143"	

Ht. of Poly = 4.023 - .021 - .023 - .025 - .021 - .023 - .026 - .024 = 4.0232 ✓

Even Fuel Height = 4.0232"
 Skyhook Reactivity = +17.79¢

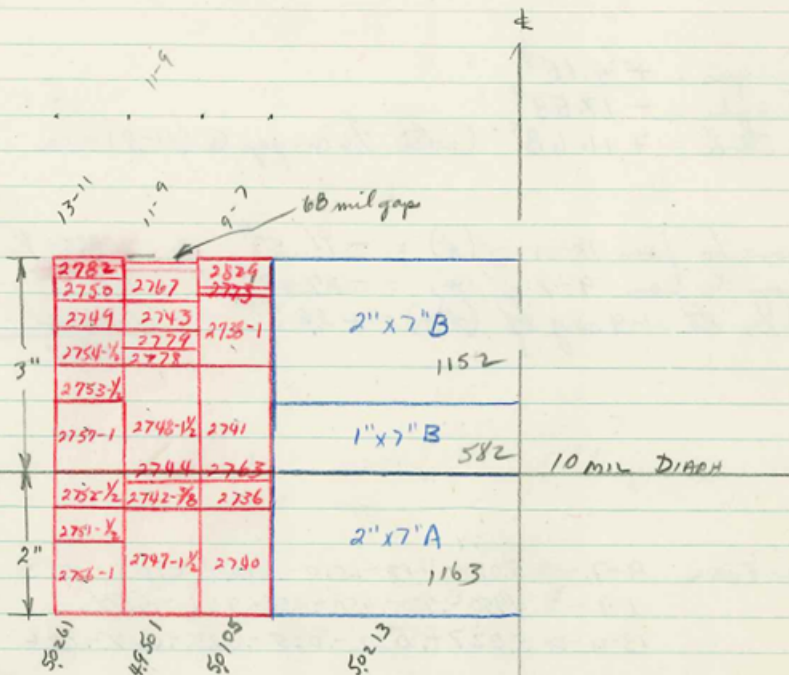
42.279 mil

O-reactivity = 4.0123" (not consid. Poly)

10.9 mils :

13"-7" BARE + POLYETHYLENE CORE

B-81



FUEL TOP 86249 gm FUEL BOTTOM 57892 gm
TOTAL MASS OF FUEL = 144.141 Kg

MASS OF TOP POLY = 1734 gm
BOTTOM = 1163 gm

TOTAL: 2.897 Kg

AVG. O.D. all fuel (w't'D) = 12.995899"
AVG. I.D. all fuel (w't'D) = 7.002813"

(OD)² = 168.89339
(ID)² = 49.03938

FUEL VOLUME = 7707.60168 cm³
 ρ = 18.701148 gm/cc

POLY Vol = 3169.244766 cm³
 ρ = 0.914097 gm/cc

13-7 Bare + Poly Core

$$* \left[\text{Nom. Ht. Critical} = (13-11) \div (9-7) = 5'' \right. \\ \left. 11-9 = 4\frac{5}{16}'' \right] \rightarrow +21.22^\circ$$

Rings = +4.15⁺

Diaph. = -17.53⁺

5. Stand = +11.68⁺ (with 1/16" air gap @ (11-9) area)

$$\begin{array}{l} \text{Remove } 1/16'' \text{ from } 13-11 \text{ of } (*) = -11.57^\circ \text{ or } 0.1851 \text{ mil} \\ \text{Remove } 1/16'' \text{ from } 9-7 \text{ of } (*) = -27.40^\circ \text{ or } 0.4384 \\ \text{Add } 1/16'' \text{ to } 11-9 \text{ ring of } (***) = +26.89^\circ \text{ or } 0.4302 \\ \hline 1.0537 \end{array}$$

reduce 54.4 mil

$$\begin{array}{l} \text{ALL FUEL } 9-7 \rightarrow 5.010, .010, .010, .010, .0105, .013 = 5.0105'' +10.8 \\ 11-9 \rightarrow 4.950, .950, .950, .950, .951, .950 = 4.9501'' +71.2 \\ 13-11 \rightarrow 5.027, .027, .025, .025, .027, .026 = 5.0261'' -4.8 \\ \text{wT. avg} = 4.9966'' \end{array}$$

all
Ht of Poly = 5.020, .020, .018, .024, .022, .026, .021, .020 = 5.0213 ~

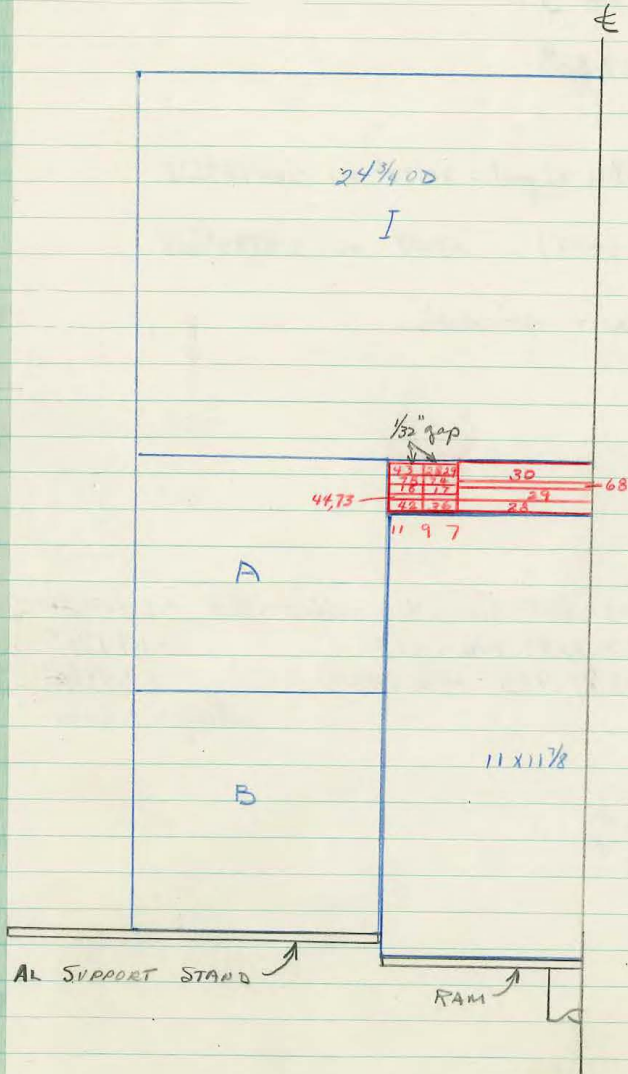
#Poly
EVEN FUEL HT = 5.0213"
SKY Hook Reactivity = +57.39⁺

O reactivity = 4.9669" (Poly not consid)

29.7 mils

SOLID
11" DIA. CYLINDER "INFIN." POLYETHYLENE REFLECTOR

Bg 240



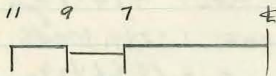
MASS OF FUEL = 41431 gm
VOLUME = 2219.80046 cm³
 $\rho = 18.66429 \text{ gm/cc}$
MASS OF POLY =
VOLUME:
 $\rho = 0.916 \text{ gm/cc}$
Avg. O.D. FUEL = 10.99698"
(*) = 120.93356

11" DIA. SOLID Inf. Poly ref.

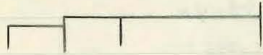
Nom. Inf. Critical: $\left. \begin{array}{l} (11 \times 7) = 1\frac{3}{32} \\ (7 \text{ dia}) = 1\frac{7}{16} \end{array} \right\}$

reactivity = +25.52¢

$\frac{3}{16}$ " GAP BETWEEN I & A = -17.30¢



$\frac{1}{32}$ " (11-9) fuel = 20.31¢ or 0.6499¢/mil



$\frac{1}{32}$ " (9-7) = 27.48 or 0.8793¢/mil

7" DIA = NOT MEAS.

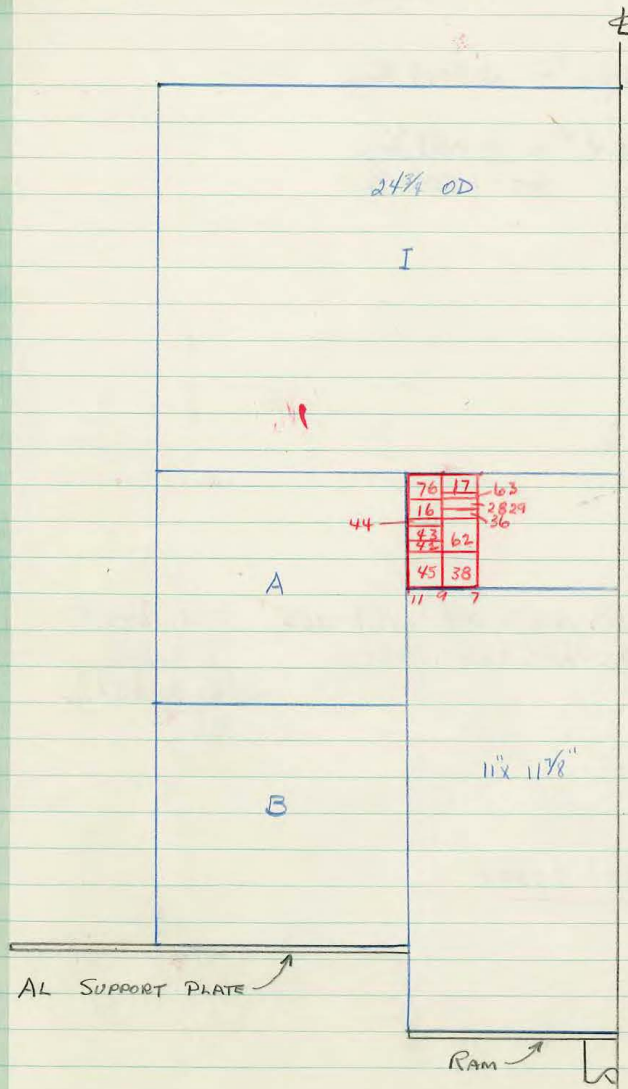
Inf. of fuel ^{1.409}
 $11-9 = 1.409 - .409 - .409 - .409 - .410 - .410 - .409 - .409 = 1.4092"$
 $9-7 = 1.417 - .417 - .417 - .418 - .416 - .417 = 1.4170"$
 $7 \text{ dia} = 1.445 - .447 - .448 - .445 - .446 - .445 = 1.4460"$
 int avg = 1.4261"

7 dia — 0
 9-7 up 29.8 mils +25.49¢
 11-7 up 36.8 mils +32.35¢

83.36¢ = 1.4460"

11"-7" "INFINITE" POLYETHYLENE REFLECTED $\frac{1}{2}$ NO CORE

Pg 229



MASS OF FUEL = 54770 gm
 VOLUME = 2928.25225 cm³
 $\rho = 18.70399 \text{ gm/cc}$
 MASS OF POLY =
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$
 AVG. O.D. FUEL = 10.99671"
 (°) = 120.92763
 AVG. I.D. FUEL = 7.00329"
 (°) = 49.04607

11-7 Dup. Poly. ref. # No Core

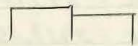
Nom. Ht. Critical: $3\frac{5}{32}"$

reactivity: 23.40^+

" 9 7



$$\frac{1}{32}" (11-9) = 25.06^+ \text{ or } 0.8019 \frac{\text{ft}}{\text{min}}$$



$$\frac{1}{32}" (9-7) = 23.4^+ \text{ or } 0.7488 \frac{\text{ft}}{\text{min}}$$

$$\text{TOT.} = 1.5507 \frac{\text{ft}}{\text{min}}$$

Ht. of fuel

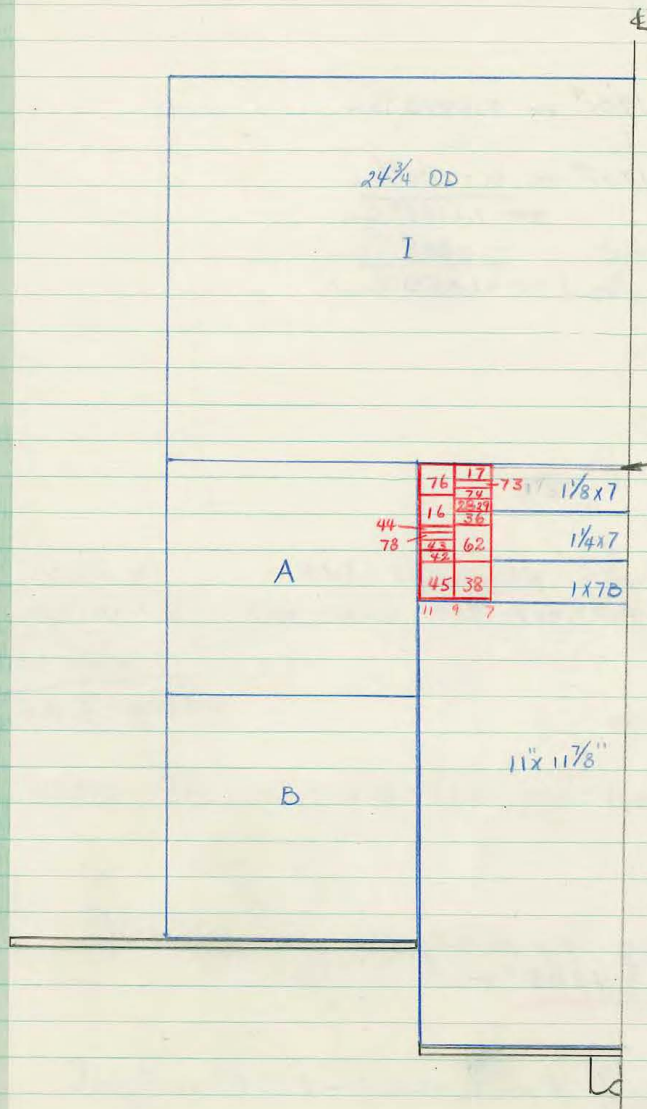
$$\begin{array}{l} 3.158 \\ 11-9 : 3.165, .164, .165, .165, .164, .164, .165 = 3.1645" \\ 3.159 \\ 9-7 : 3.166, .166, .166, .166, .166, .166, = 3.1660" \\ \text{wt. avg } 3.1651" \end{array}$$

$$+ 23.40^+ = 3.1651"$$

$$\text{O react} \rightarrow 3.1651 - .0151 = 3.1500"$$

11-7 "INFINITE" POLYETHYLENE REFLECTOR + POLY CORE

236



MASS OF FUEL = 59120 gm

VOLUME = 3161.18382 cm³

$\rho = 18.70185 \text{ gm/cc}$

MASS OF POLY:

VOLUME:

$\rho = 0.916 \text{ gm/cc}$

Avg. O.D. fuel = 10.99672"

(*) = 120.92785

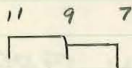
Avg. I.D. fuel = 7.00319"

(*) = 49.04467

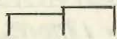
11-7 Inf. Poly ref + Poly Core

Nom. Ht Critical = FUEL = $3\frac{1}{32}"$
P. Core = $3\frac{3}{8}"$

reactivity = -1.97%



$$\frac{1}{32}" (11-9) = 17.01\% \text{ or } 0.5443\%/\text{mil}$$



$$\frac{1}{32}" (9-7) = 17.97\% \text{ or } 0.5750\%/\text{mil}$$

$$\begin{aligned} \text{TOT} &= 1.1193\%/\text{mil} \\ \text{core}^* &= -0.0823\%/\text{mil} \\ \text{Grand TOT} &= 1.0370\%/\text{mil} \end{aligned}$$

Ht of fuel $\begin{matrix} 3.409 \\ 11-9 = 3.415 - .415 - .415 - .415 - .415 - .415 \\ 3.410 \\ 9-7 = 3.427 - .427 - .427 - .427 - .428 - .428 - .427 \end{matrix}$

$$= 3.4150"$$

$$= 3.4272"$$

$$- 8 \text{ mil}$$

$$\text{use } 3.4192"$$

$$\text{wt avg} = 3.4168"$$

$$\text{Ht. of Poly Core} = 3.398 - .400 - .398 - .400 - .399 - .402 - .400 - .398 = 3.3992"$$

$-1.32\% = 3.4192"$ * avg gap in Poly core is considered
Correct $\rightarrow 3.4192 + .0013 = 3.4205"$

* [Core vs No Core DERIVATIONS] 1 mil core = -0.078 mil fuel

Core raise 19.9 mils = -1.63%

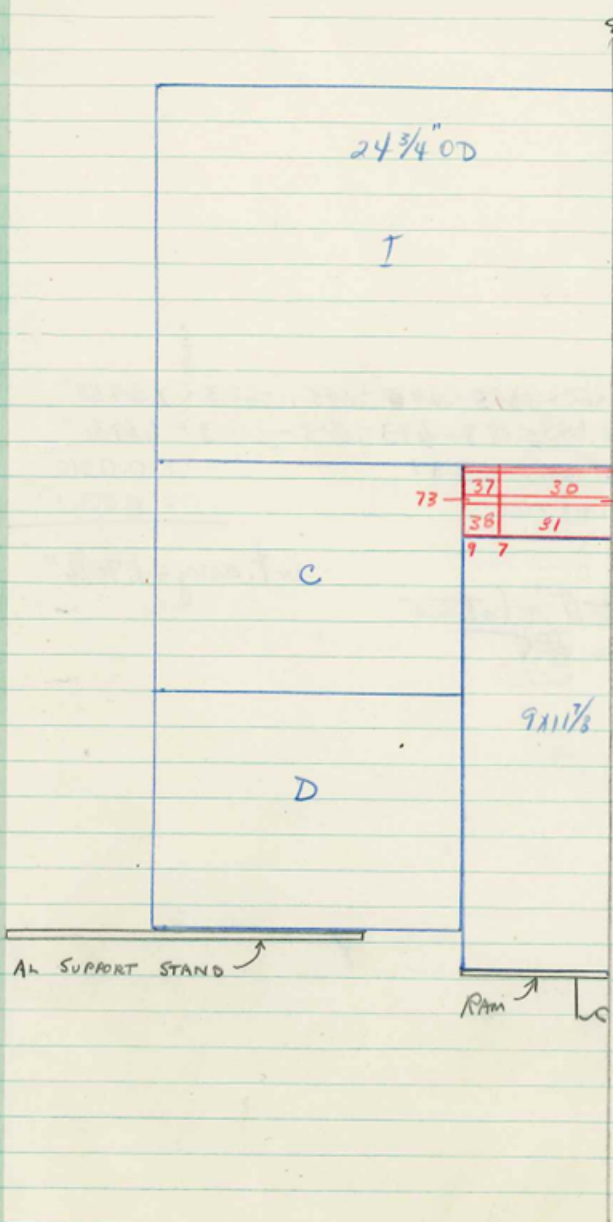
9-7 = 0

11-9 raise 4.2 mils = $+2.28\%$

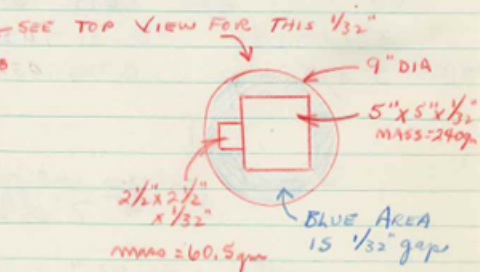
9" SOLID

"INFINITE" POLYETHYLENE REFLECTOR

Pg 244



MASS OF FUEL = 33276 gm
 VOLUME = 1779.84137 cm³
 $\rho = 18.69604 \text{ gm/cc}$
 MASS OF FUEL =
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$
 Avg. D.D. FUEL = 8.99609"
 (*) : 80.92463



9" dia. Solid Inf. Poly. ref.

$$\text{Nom. Wt. Critical} = 1\frac{1}{16}" \left[\frac{1(2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{32})}{+1(5 \times 5 \times \frac{1}{32})} \right] \quad \text{reactivity} = -1.25\%$$

NO EVALUATION OF FUEL

$$\text{At off fuel } 9-7 = 1.693, .693, .693, .695, .695, .695, .693 = 1.6938"$$

$$7 \text{ dia} = 1.693, .693, .693, .693, .693, .693, .693 = 1.6930"$$

$$2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{32} = 0.031, .0305, .0315, .031$$

$$= 0.0310"$$

$$\text{④ 141 D } 5 \times 5 \times \frac{1}{32} = 0.0315, .032, .0315, .031$$

$$= 0.0315"$$

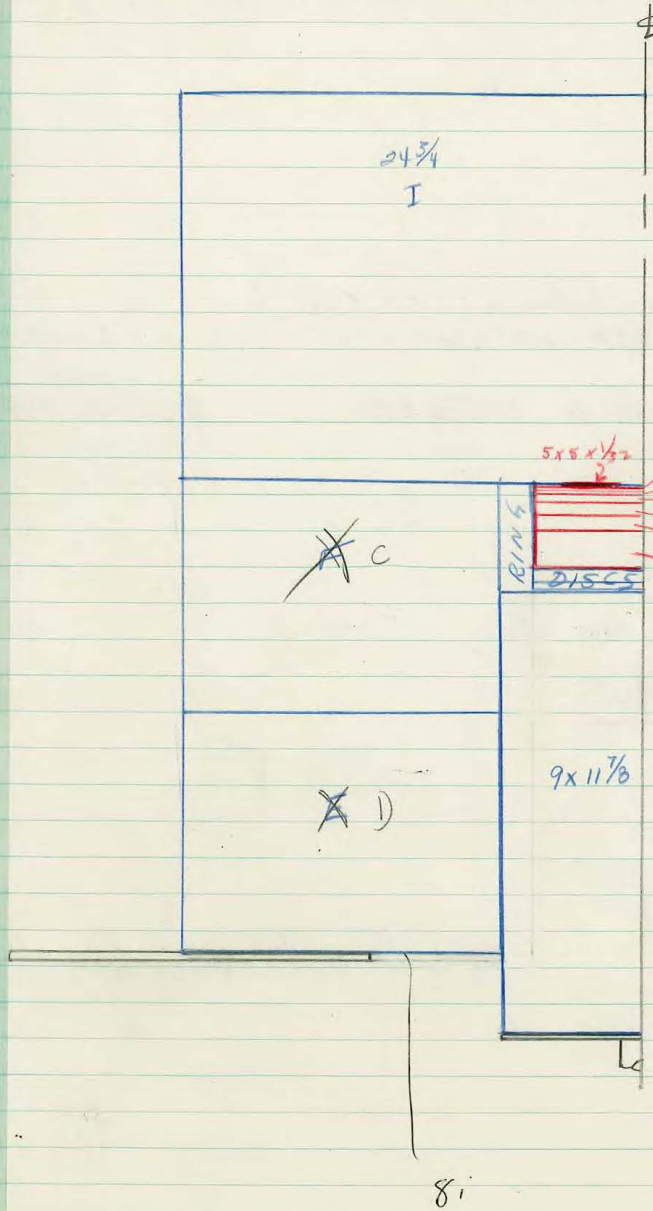
$$\text{wt. avg} = 1.7086"$$

Small pieces weighted relative
to 7" dia. SP

$$\underline{-1.25\% = 1.7086"}$$

7" DIA. SOLID "INFINITELY POLYETHYLENE REFLECTED"

Pg 249



(Incl. 5x5x1/2)
 MASS OF FUEL = 2689.3 gm
 VOLUME = 1435.2340 cm³
 P = 18.7377 gm/cc
 MASS OF POLY =
 VOLUME =
 P = 0.916 gm/cc
 AVG. O.D. OF FUEL = 6.99600"
 (") : 48.94401

2.2574 Fuel height

3.09

3/4 Disc

7" DIA. SOLID

Poly reflected

nom 1st. Critical = $2\frac{1}{4}" + (5 \times 5 \times \frac{1}{32})^{2469m}$ reactivity = 5.84°

4332
2076
2256

fuel height 7" dia (NOT including $(5 \times 5 \times \frac{1}{32})$)

$2.256 - .258 - .257 - .256 - .259 - .258 - .258 \rightarrow 2.2574$

+021

Use 21 mil calc. for 5×5 to 7" dia.

Tot. Ht. = $2.2784"$

React: $+5.84^\circ = 2.2784"$

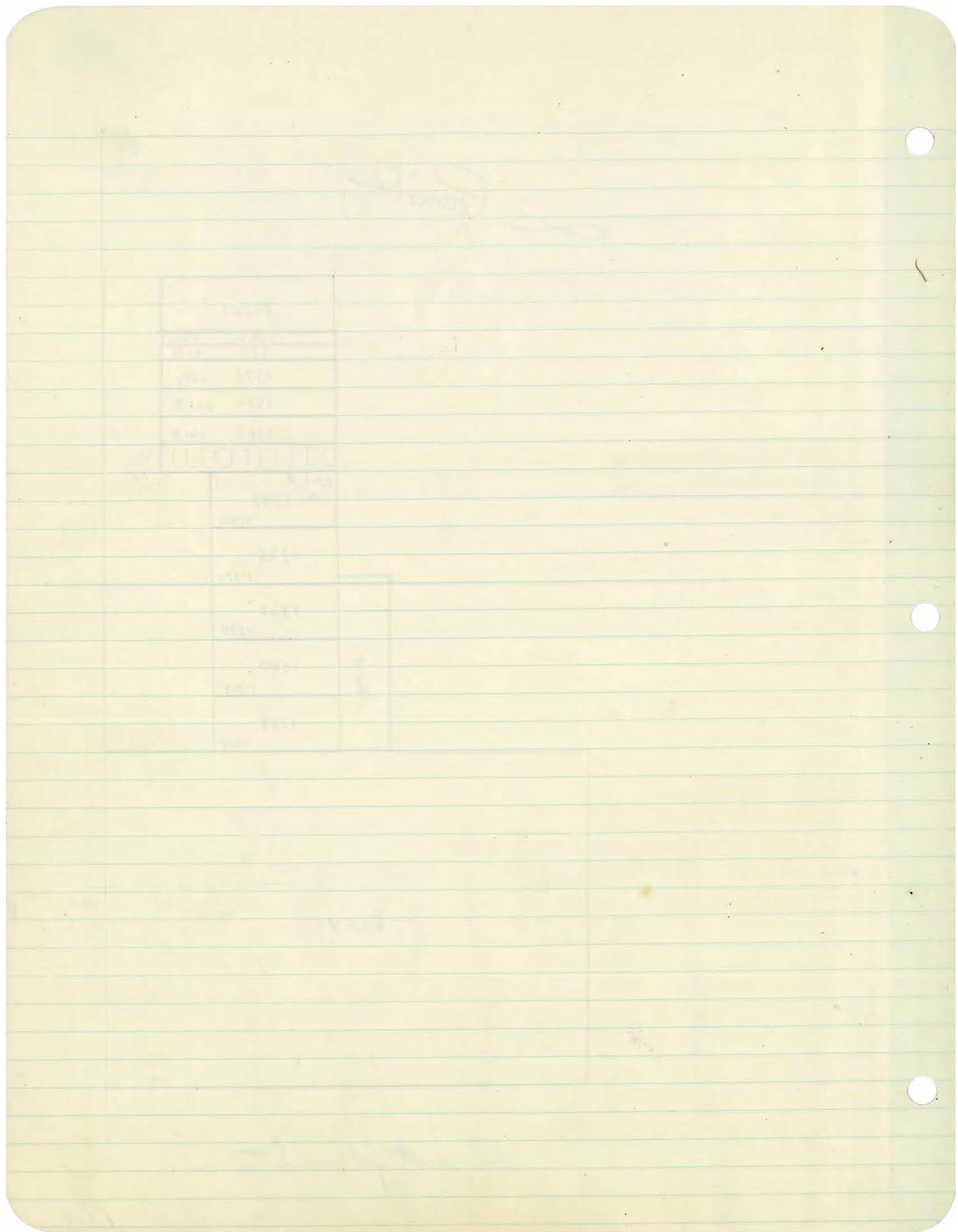
Period

PLEX1	
1362	3201
1370	3291
1373	6592
1400	6603
1368	6614
IIIIIIIIII	
1366 6390	1349
11366	
1365	11370
1361	11385
1360	11364
1359	11377

PLEX1

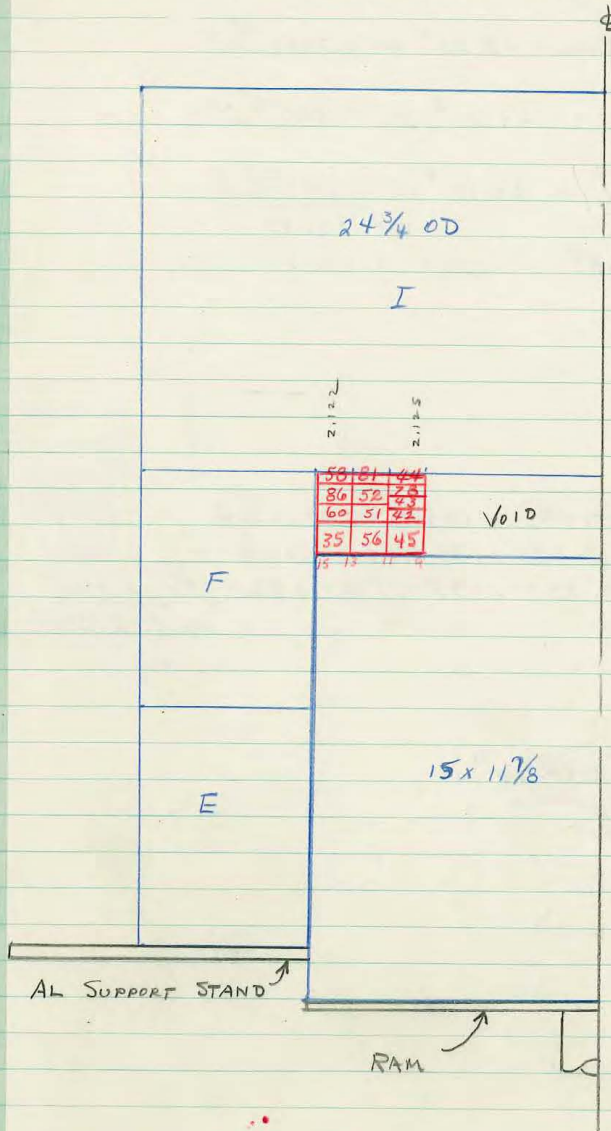
PLEX1

not followed thru.



15"-9" "INFINITE" POLYETHYLENE REFLECTOR & NO CORE

Pg 213



MASS OF FUEL = 73709 gm

VOLUME = 3940.58319 cm³

$\rho = 18.70509 \text{ gm/cc}$

MASS OF POLY =

VOLUME =

$\rho = 0.916 \text{ gm/cc}$

AVG. O.D. FUEL = 14.99439"

(²) = 224.80174

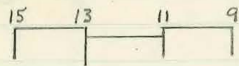
AVG. I.D. FUEL = 9.00179"

(²) = 81.03222

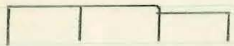
15-9 Poly & No Core

Nom. Ht. Critical = $2\frac{1}{8}"$

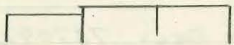
Reactivity = $+8.93\%$



$\frac{1}{32}" (11-9) \text{ FUEL} = 23.26\%$ or $0.7443\%/\text{mil}$



$\frac{1}{32}" (13-11) = 23.21\%$ or $0.7427\%/\text{mil}$



$\frac{1}{32}" (15-13) = 23.13\%$ or $0.7401\%/\text{mil}$

TOT = 2.2271

$\frac{3}{16}" \text{ SEPARATION OF I \& F} = 24.68\%$

Core $\approx 0.2208\%/\text{mil}$

FUEL Ht. 15-13 = $2.124 - .124 - .125 - .124 - .124 - .124 = 2.1241"$

13-11 = $2.132 - .131 - .132 - .130 - .130 - .129 = 2.1306"$

11-9 = $2.136 - .136 - .137 - .137 - .136 - .136 - .135 = 2.1361"$

Avg wt. = $2.1296"$

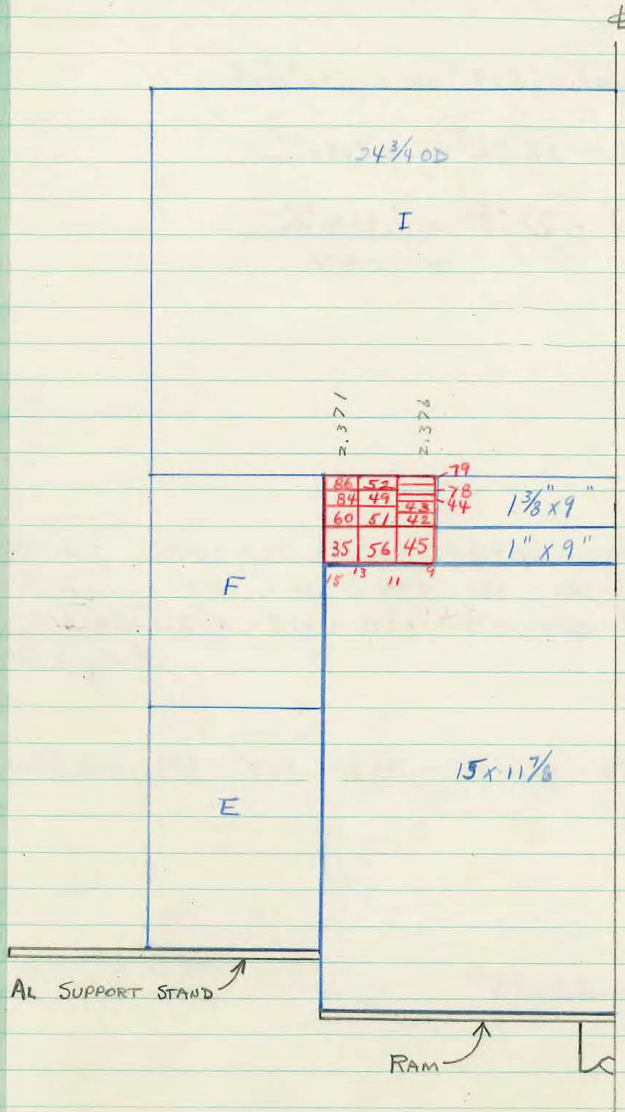
$+8.93\% = 2.1296"$

$O_{\text{react}} = 2.1296 - .004 = 2.1256"$

15" x 9"

"INFINITE" POLYETHYLENE REFLECTOR + POLY CORE

Pg 215



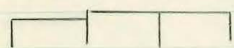
MASS OF FUEL = 82.391 gm
 VOLUME = 4403.24 cm³
 $\rho = 18.71141 \text{ gm/cc}$
 MASS OF POLY =
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$
 Avg. D.D. FUEL = 14.99428"
 (2) = 224.82843
 Avg. I.D. FUEL = 9.00176"
 (2) = 81.03168

15-9 Poly + Core

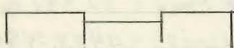
Nom. Ist. Critical = $2\frac{3}{8}"$

Reactivity = $+21.15^{\circ}$

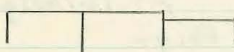
15 13 11 9



$$\frac{1}{32}" (15-13) \text{ fuel} = 18.29^{\circ} \text{ or } 0.5852^{\circ}/\text{mil}$$



$$\frac{1}{32}" (13-11) = 25.76^{\circ} \text{ or } 0.8243^{\circ}/\text{mil}$$



$$\frac{1}{32}" (11-9) = 23.05^{\circ} \text{ or } 0.7376^{\circ}/\text{mil}$$

$$\text{TOT} = 2.1471$$

fuel height 15-13 = 2.372, 372, 376, 373, 375, 377, 377 = 2.3745"

13-11 = 2.382, 382, 382, 381, 382, 381, 380 = 2.3814"

11-9 = 2.383, 384, 384, 383, 383, 383, 383 = 2.3831"

wt. avg = 2.3791"

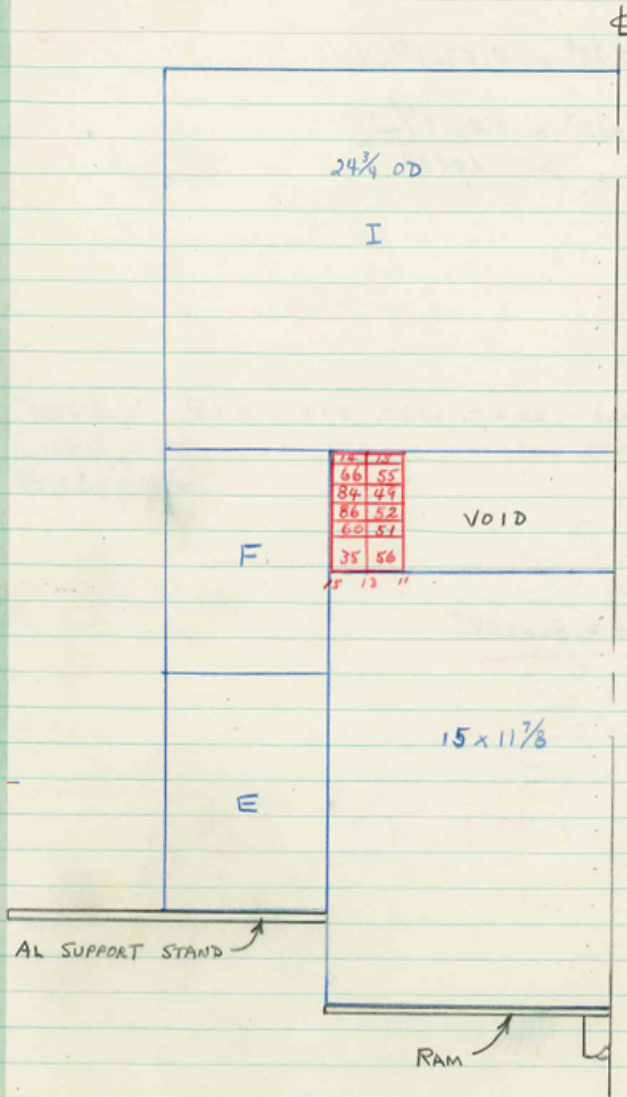
Ist. of Poly Core = 2.382, 382, 382, 381, 381, 383, 384, 382 = 2.3821"

+ $21.15^{\circ} = 2.3791"$

~~O react = 2.3791 - .0098 = 2.3693"~~

15"-11" "INFINITE" POLYETHYLENE REFLECTOR #NO CORE

Pg 208



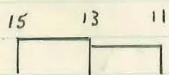
MASS OF FUEL = 80631 gm
 VOLUME = 4307.63973 cm³
 $\rho = 18.71813 \text{ gm/cc}$
 MASS OF POLY
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$
 AVG. O.D. FUEL = 14.99513"
 (2) : 224.85392
 AVG I.D. FUEL = 11.00265"
 (2) : 121.05830

3214	3797
66	7605
84	5039
86	6717
60	6743
35	6743 13409
15	3259
55	6514
49	4360
52	5811
51	5822
56	11567

15-11 Poly # No Core

Nom. 1st. Critical = $3\frac{7}{32}$ "

reactivity = -13.94%



$$\frac{1}{32}" (15-13) = 17.88\% \text{ or } 0.5721\%/\text{mil}$$



$$\frac{1}{32}" (13-11) = 14.12\% \text{ or } 0.4518\%/\text{mil}$$

$$\text{TOT} = 1.0239$$

FUEL HEIGHT $\begin{matrix} 3.216 \\ 15-13 = 3.220 - .221 - .222 - .219 - .219 - .219 = 3.2200" \\ 3.231 \\ 13-11 = 3.229 - .229 - .230 - .229 - .231 - .230 - .231 = 3.2298" \\ \text{w.t. avg} = 3.2245" \end{matrix}$

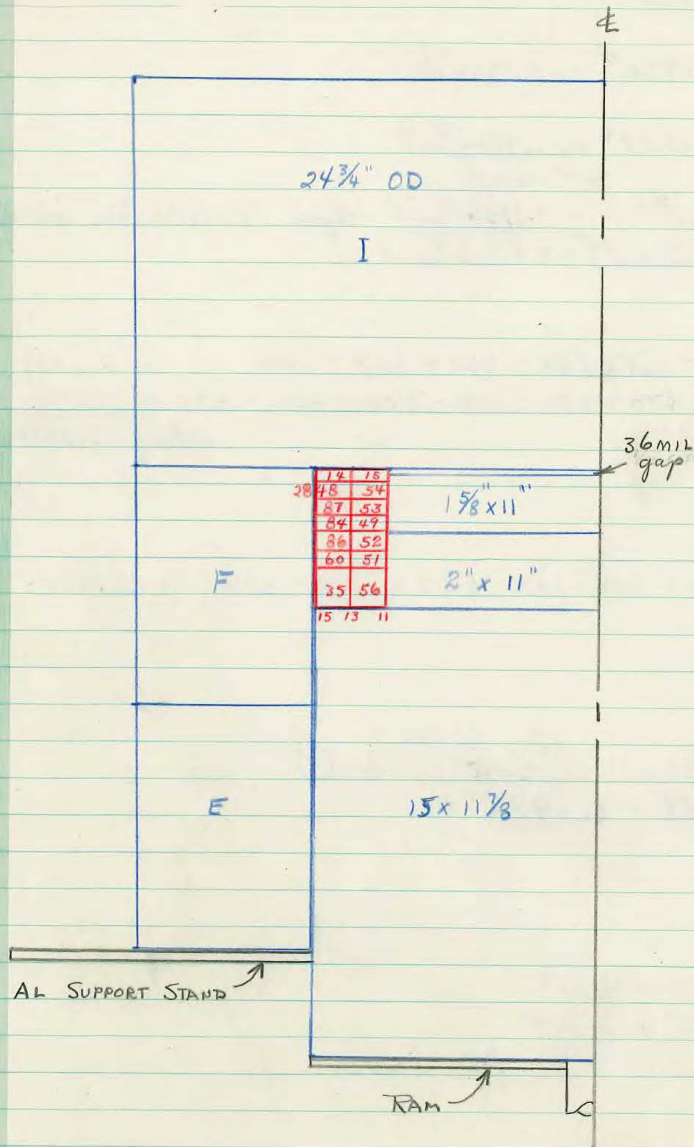
$$+13.94\% = 3.2245"$$

$$\text{Oreact} = 3.2245 - .0136 = 3.2109"$$

less 3409m

15" 11" "INFINITE" POLYETHYLENE REFLECTOR + POLY. CORE

B210



MASS OF FUEL = 91656 gm

VOLUME = 4898.95263 cm³

$\rho = 18.70930 \text{ gm/cc}$

MASS OF POLY =

VOLUME =

$\rho = 0.916 \text{ gm/cc}$

AVG. O.D. FUEL = 14.99507"

(²) = 224.85212

AVG I.D. FUEL = 11.00283"

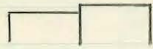
(²) = 121.06226

15-11 Poly + Core

Nom. Ht. Critical = FUEL $3\frac{1}{32}"$
Core $3\frac{5}{8}"$

Reactivity = +20.92%

15 13 11



$$\frac{1}{32}" (15-13) = 17.80\% \text{ or } 0.5696\%/\text{mil}$$



$$\frac{1}{32}" (13-11) = 15.07\% \text{ or } 0.4822\%/\text{mil}$$

$$\begin{aligned} \text{Core}^* & \quad \text{TOT} = 1.0518 \\ & \quad - 0.1156\%/\text{mil} \rightarrow (\text{from Core vs No Core derivation}) \\ \text{Grand T} & = 0.9362\%/\text{mil} \end{aligned}$$

$$\begin{aligned} \text{FUEL HEIGHT} & \quad \begin{matrix} 3.660 \\ 15-13 = 3.663 - .664 - .665 - .667 - .667 - .665 \\ 3.671 \\ 13-11 = 3.670 - .670 - .670 - .670 - .670 - .670 - .670 \end{matrix} \\ & \quad \text{avg} = 3.6673" \end{aligned}$$

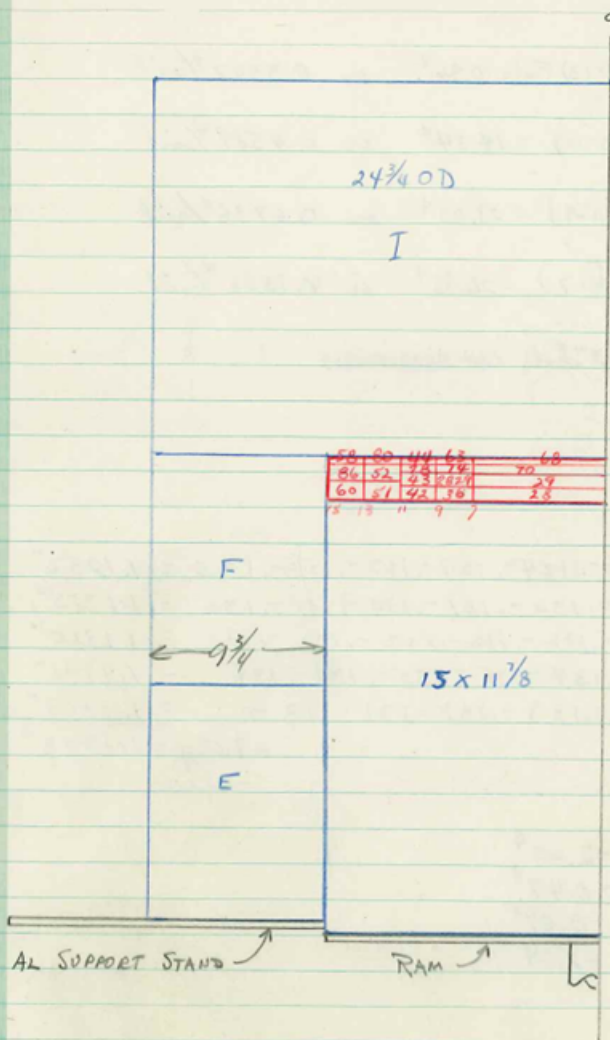
$$\text{Ht. of Poly Core} = 3.632 - .633 - .634 - .633 - .635 - .634 - .634 = 3.6335"$$

$$\begin{aligned} + 19.50\% & = 3.6700" \quad * (\text{36 mil gap / 15 considered}) \\ \text{O}_{\text{react}} & \rightarrow = 3.6700 - .0208 = 3.6492" \end{aligned}$$

$$\begin{aligned} 13-11 & \quad \text{O} \\ \text{Core raise } 36.5 \text{ mil} & = -4.21\% \\ 15-13 \text{ raise } 4.9 & = +2.79\% \end{aligned}$$

15" DIA. SOLID "INFINITELY" POLYETHYLENE REFLECTED

Q224



MASS OF FUEL = 61074 gm

VOLUME = 3271.2196 cm³

$\rho = 18.67010 \text{ gm/cc}$

MASS OF POLY =

VOLUME =

$\rho = 0.916 \text{ gm/cc}$

AVG. OD. FUEL = 14.99516"

(2) : 224.85482

2475
15
575

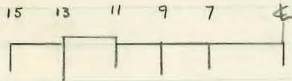
mass./in.³ of 15" dia = 0.05403 Kg

15" DIA. SOLID

POLY. REF.

Nom. Ht. Critical = $1/8"$

reactivity = $+8.77^{\circ}$



$$1/32" (15-13) \text{ Fml} = 10.46^{\circ} \text{ or } 0.3347^{\circ}/\text{mil}$$



$$1/32" (13-11) = 14.34^{\circ} \text{ or } 0.4588^{\circ}/\text{mil}$$



$$1/32" (11-9) = 21.05^{\circ} \text{ or } 0.6736^{\circ}/\text{mil}$$



$$1/32" (9-7) = 26.85^{\circ} \text{ or } 0.8592^{\circ}/\text{mil}$$

$1/32"$ 7" dia "NOT MEASURABLE"

fuel height 1.124

$$15-13 = 1.124 - .126 - .124 - .124 - .127 - .127 - .125 = 1.1252"$$

$$13-11 = 1.132 - .131 - .132 - .131 - .134 - .131 - .130 = 1.1315"$$

$$11-9 = 1.132 - .132 - .132 - .132 - .132 - .132 - .132 = 1.1320"$$

$$9-7 = 1.134 - .134 - .134 - .134 - .135 - .134 - .134 = 1.1341"$$

$$7 \text{ dia} = 1.131 - .132 - .133 - .131 - .131 - .130 = 1.1313"$$

wt. Avg = $1.1303"$

7" dia $\rightarrow 0$

$$9-7 \text{ down} = -2.8 \text{ mil} = -2.40^{\circ}$$

$$11-9 \text{ down} = -0.7 = -0.47^{\circ}$$

$$13-11 \text{ down} = -0.2 = -0.09^{\circ}$$

$$15-13 \text{ Up} = +6.1 = +2.04^{\circ}$$

$7.85^{\circ} = 1.1313"$

$0.20^{\circ} = 1.129"$

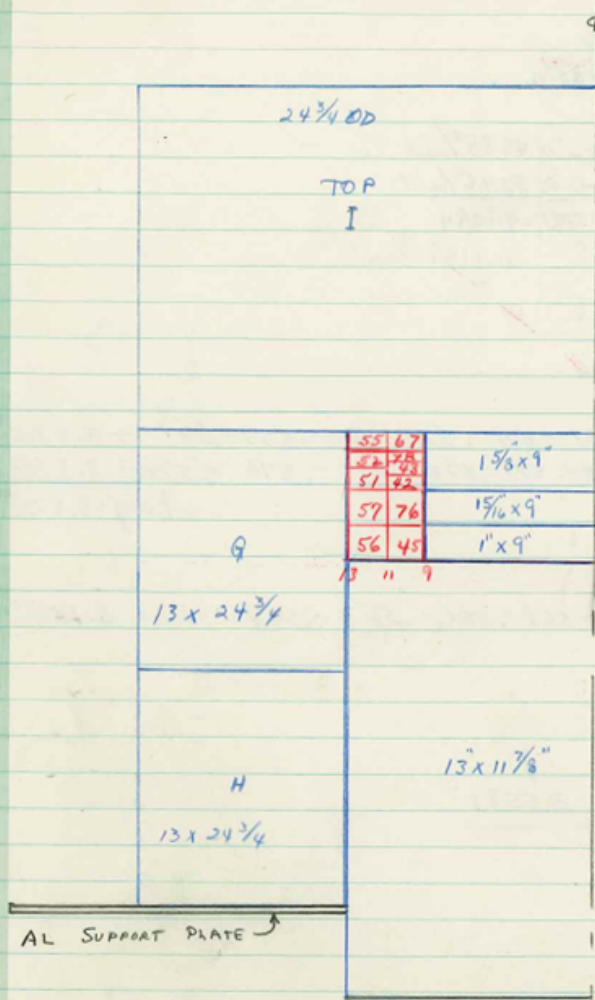
$\approx 60.96 \text{ KG}$

7498
14992

13" - 9"

"INFINITE" POLYETHYLENE REFLECTOR + POLY CORE

Bq193



MASS OF FUEL = 75.626 Kg

VOLUME = 4038.60186 cm³

ρ = 18.72578 gm/cc

MASS OF POLY =

VOLUME =

ρ = 0.916 gm/cc

AVG. OD FUEL = 12.99622"

ID = 9.00142"

AVG. OD POLY =

OD² = 168.90173

ID² = 81.02556

(?) =

13"-9" "INFINITE" POLY REF + POLY CORE

Nom. Ht. Critical = $3\frac{9}{16}"$

reactivity = +13.15¢

SEPARATED G FROM H ($\frac{1}{8}"$) = nil

SEPARATED I FROM G ($\frac{1}{8}"$) = -11.33¢

$\frac{1}{32}"$ FUEL (13"-11") = +15.59¢ or 0.4988¢/mil

$\frac{1}{32}"$ FUEL (11"-9") = +16.55¢ or 0.5296¢/mil

TOT = 1.0284

core = 0.1148¢/mil

FUEL HEIGHT 13-11 = 3.571 - .571 - .571 - .571 - .570 - .571 - .571 = 3.5708"

11-9 = 3.570 - .570 - .571 - .572 - .573 - .570 - .570 = 3.5708"

wt. avg = 3.5708"

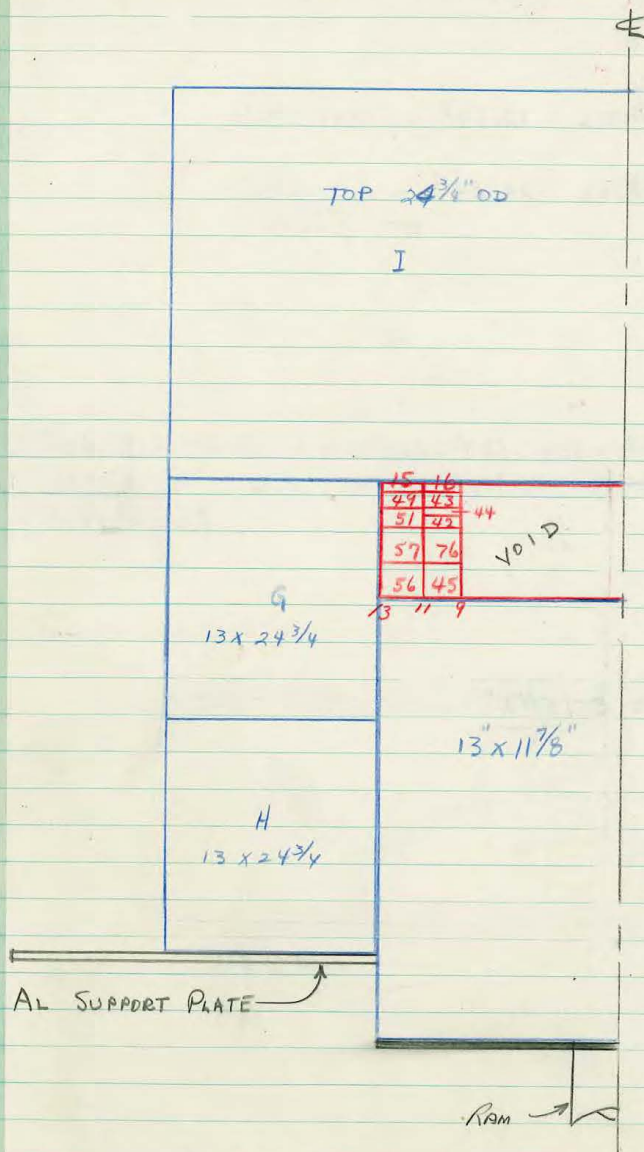
Ht. of Poly Core = 3.567 - .566 - .567 - .568 - .566 - .567 - .567 - .567 = 3.5668"

+ 13.15¢ = 3.5708"

O react = 3.5708 - .0127 = 3.5581"

13"-9" "INFINITE" POLYETHYLENE REFLECTED & NO CORE

Fig 189



MASS OF FUEL = 67.018 Kg

VOLUME = 3581.55294 cm³

$\rho = 18.71199$ gm/cc

MASS OF POLY =

VOLUME =

$\rho = 0.916$ gm/cc

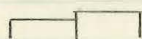
AVG OD FUEL = 12.99627" OD² = 168.90303

AVG ID = 9.00133" ID² = 81.02484

13-9

Inf. Poly ref # No CoreNom. Ht. Critical = $3\frac{5}{32}"$ reactivity = $+8.43\%$

13 11 9

 $\frac{1}{32}"$ (11" x 9") FUEL = 12.83¢ or 0.4105¢/mil $\frac{1}{32}"$ (13" x 11") FUEL = 22.24¢ or 0.7116¢/mil

TOT = 1.1221

FUEL HT = 13-11 = 3.165 - .165 - .164 - .164 - .166 - .165 - .165 = 3.1648"

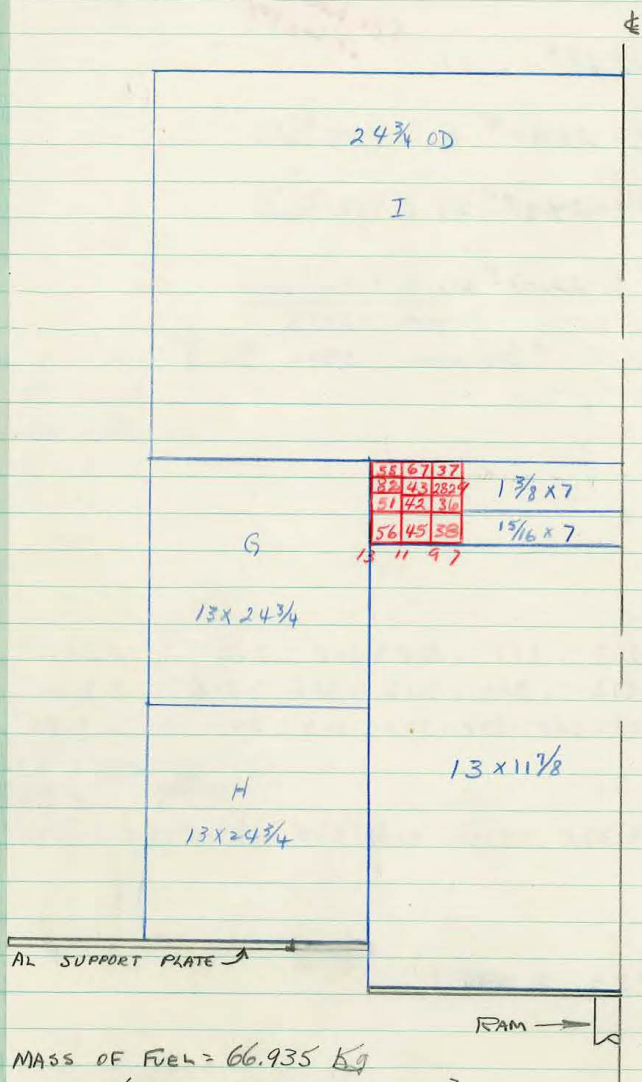
11-9 = 3.168 - .168 - .168 - .168 - .170 - .170 - .170 = 3.1688"

wt. avg = 3.1666"

 $+8.43\% = 3.1666"$ O_{react} → $3.1666 - .0075 = \underline{3.1591}"$

13"-7" "INFINITE" POLYETHYLENE REFLECTOR + POLY CORE

Eq 199



MASS OF FUEL = 66.935 Kg

$$\text{VOLUME} = 3573.53412 \text{ cm}^3$$
$$\rho = 18.73075 \text{ gm/cc}$$

MASS OF POLY =

VOLUME:

$\rho = 0.916 \text{ gm/cc}$

AVG. O.D. FUEL = 12.99619"

OD²: 168.90095

ID : 7.00291"

ID: 49.04074

DD Poly

(2) =

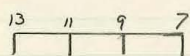
13-7 "INFINITE" Poly Ref + Core

Nom. Ht. Critical: $2\frac{5}{16}"$

reactivity = $+40.0\%$
27.3

Not agree with 198 Poly from 11/24/01 correct
See bottom x hot max

$\frac{1}{8}"$ SEPARATION OF G & I: -12.68%



$$\frac{1}{32}" (13-11) = 23.69\% \text{ or } 0.7580\%/mil$$



$$\frac{1}{32}" (11-9) = 24.38\% \text{ or } 0.7801\%/mil$$



$$\frac{1}{32}" (9-7) = 22.17\% \text{ or } 0.7094\%/mil$$

TOT = 2.2475

* Core value = .0922 $\%/mil$

FUEL HEIGHT $13-11 = 2.317 - .317 - .317 - .317 - .317 - .316 = 2.3168"$

$11-9 = 2.316 - .316 - .316 - .316 - .316 - .316 = 2.3160"$

$9-7 = 2.323 - .323 - .325 - .327 - .327 - .323 - .322 = 2.3246"$
- 8 mils
= 2.3166"
wt avg. $2.3164"$

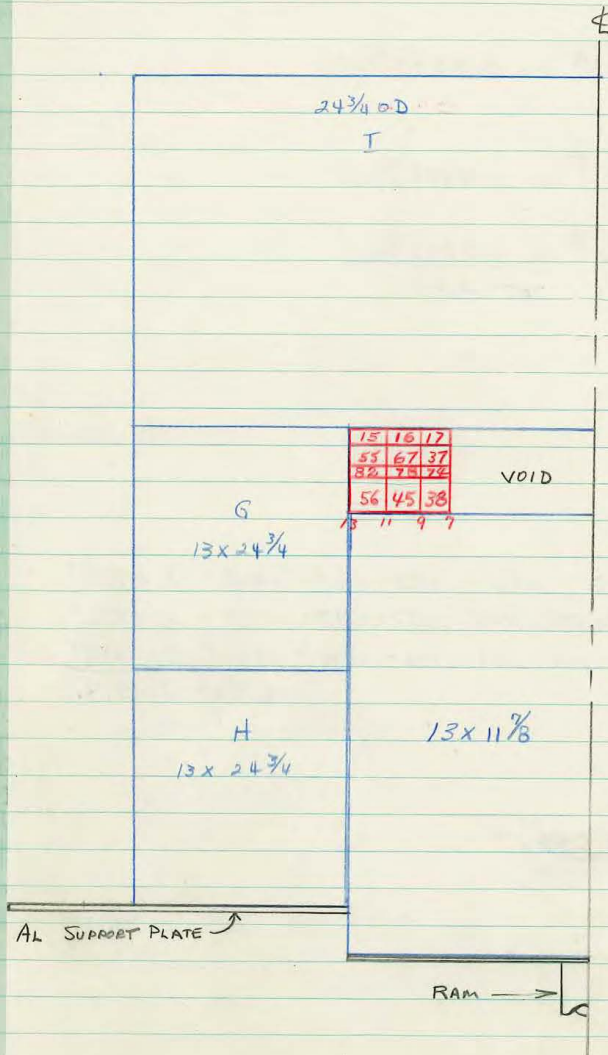
Nt of Poly Core = $2.315 - .314 - .315 - .315 - .313 - .315 - .315 - .315 = 2.3146"$

$+ 40.0\% = 2.3164"$

O_{react} = $2.3164 - .0177 = 2.2987"$

13"-7" "INFINITE" POLYETHYLENE REFLECTOR & No CORE

196



MASS OF FUEL = 60.548 kg

VOLUME = 3236.55265 cm³

$\rho = 18.70755 \text{ gm/cc}$

MASS OF POLY =

VOLUME =

$\rho = 0.916 \text{ gm/cc}$

AVG O.D. FUEL = 12.99650" OD² = 168.90901

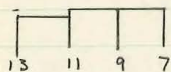
ID = 7.00268" ID² = 49.03752

AVG O.D. POLY = () :

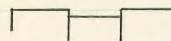
13-7 "INFINITE" POLY REF & No Core

Nom. Ht. Critical = $2\frac{3}{32}"$

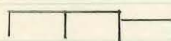
reactivity = $+27.92\%$



$$\frac{1}{32}"(13-11) = 23.11\% \text{ or } 0.7395\%/mil$$



$$\frac{1}{32}"(11-9) = 27.9\% \text{ or } 0.8928\%/mil$$



$$\frac{1}{32}"(9-7) = 26.21\% \text{ or } 0.8387\%/mil$$

$$TOT = 2.4710$$

FUEL HEIGHT

$$13-11 = 2.097, .097, .096, .097, .098, .096 = 2.0968"$$

$$11-9 = 2.097, .097, .098, .098, .097, .097, .097 = 2.0972"$$

$$9-7 = 2.100, .100, .100, .101, .101, .100, .100 = 2.1002"$$

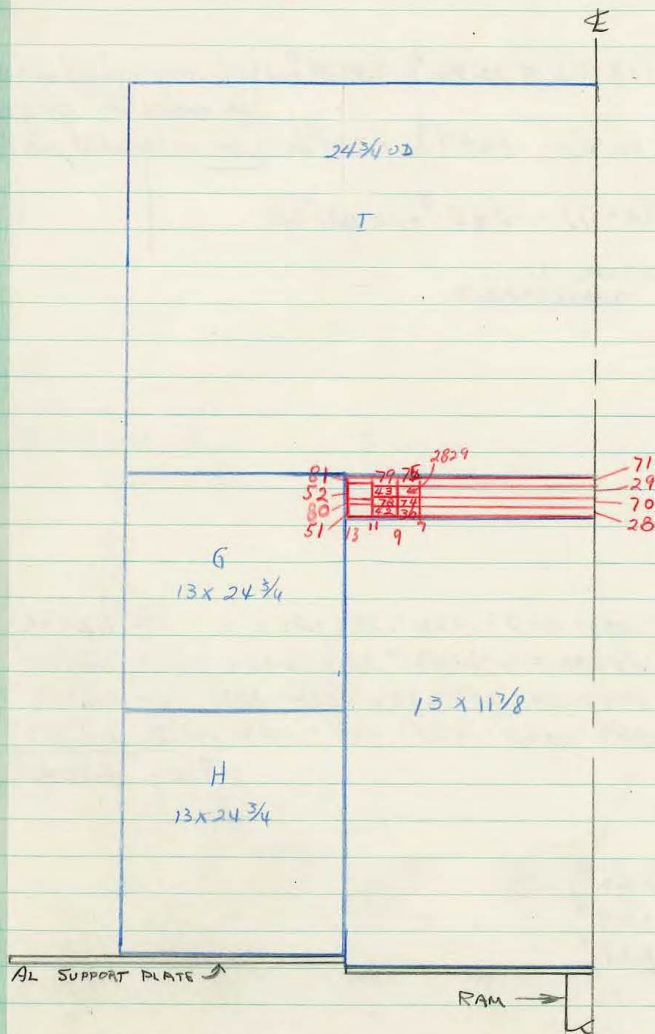
w. avg = 2.0978"

$$+27.92\% = 2.0978"$$

$$O_{react} \rightarrow 2.0978 - .0112 = 2.0866"$$

13" DIA. SOLID "INFINITE" POLYETHYLENE REFLECTOR

Pg 204



MASS OF FUEL = 50.971 Kg
 VOLUME = 2726.21470 cm³
 $\rho = 18.69661 \text{ gm/cc}$

MASS OF POLY =
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$

AVG OD FUEL = 12.99577" OD² = 168.89003

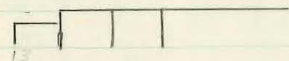
OD POLY = () :

13" dia SOLID "INFINITE" Ref

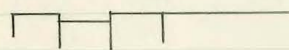
Dom HT. Critical 1 1/4"

Reactivity = 44.2%

13 11 9 7 ->



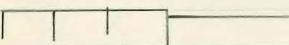
$$\frac{1}{32}" (13-11) = 15.42\% \text{ or } 0.4934\%/\text{mil} \quad \left\{ \begin{array}{l} \text{If mass diff. need} \\ \text{consideration they may} \\ \text{be calculated via Pg 305} \end{array} \right.$$



$$\frac{1}{32}" (11-9) = 21.97\% \text{ or } 0.7030\%/\text{mil}$$



$$\frac{1}{32}" (9-7) = 24.0\% \text{ or } 0.7680\%/\text{mil}$$



7" DIA.
NOT MEASUREABLE

FUEL HEIGHT

$$\begin{aligned} 13-11 &= 1.257-.256-.257-.256-.256-.255 &= 1.2561" \\ 11-9 &= 1.252-.252-.252-.252-.252-.252 &= 1.2520" \\ 9-7 &= 1.255-.254-.254-.256-.256-.255 &= 1.2551" \\ 7" DIA &= 1.254-.254-.253-.253-.254-.254 &= 1.2535" \\ & & \text{wt. avg. } 1.2541" \end{aligned}$$

7" dia = 0

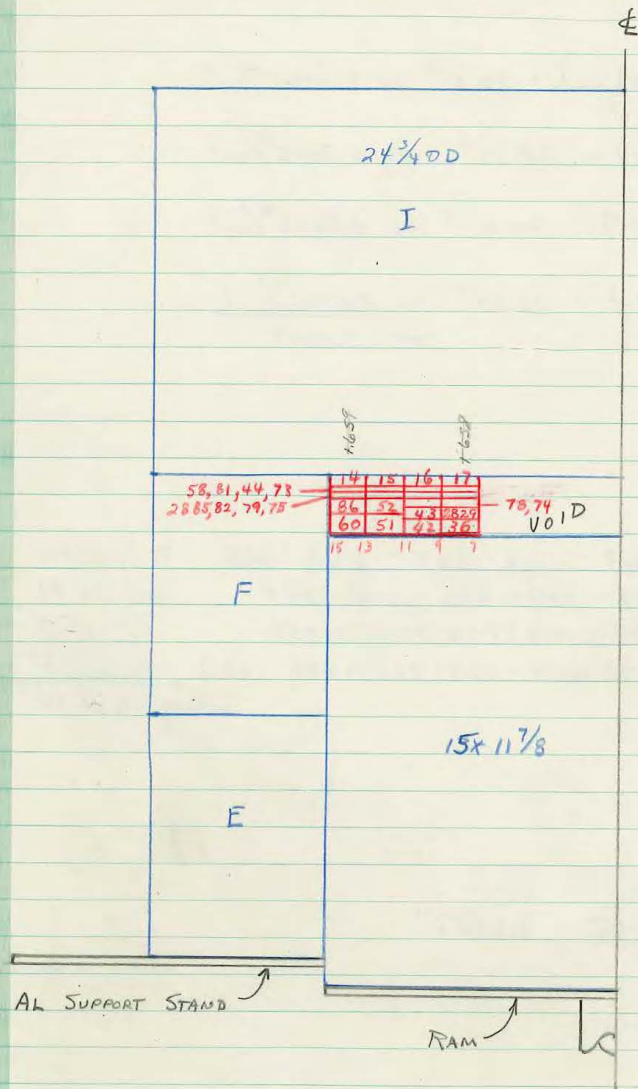
$$\begin{aligned} 9-7 \text{ down } 1.6 \text{ mils} &= -1.22\% \\ 11-9 \text{ up } 1.5 \text{ mils} &= +1.05\% \\ 13-11 \text{ down } 2.6 \text{ mils} &= -1.28\% \end{aligned}$$

+ 42.75% = 1.2535"

(~~best~~ 1.240" @ 0)

15" 7" "INFINITE" POLYETHYLENE REFLECTED & NO CORE

Page 1



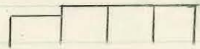
MASS OF FUEL = 70363 gm
 VOLUME = 3762,72642 cm³
 $\rho = 18.70000 \text{ gm/cc}$
 MASS OF POLY =
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$
 Avg. D.D. FUEL = 14.99608"
 (2) = 224,88241
 Avg. I.D. = 7.00263"
 (2) = 49.03682

15-7 Poly & No Core

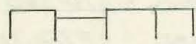
nom. ht. critical = $1\frac{21}{32}$ "

Reactivity: +30.01%

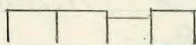
15 13 11 9 7



$$\frac{1}{32}" (15-13)_{\text{fuel}} = 20.5\% \text{ or } 0.6560\%/mil$$



$$\frac{1}{32}" (13-11) = 23.94\% \text{ or } 0.7660\%/mil$$



$$\frac{1}{32}" (11-9) = 30.01\% \text{ or } 0.9603\%/mil$$



$$\frac{1}{32}" (9-7) = 21.24\% \text{ or } 0.6796\%/mil$$

$$TOT = 3.0619$$

fuel height

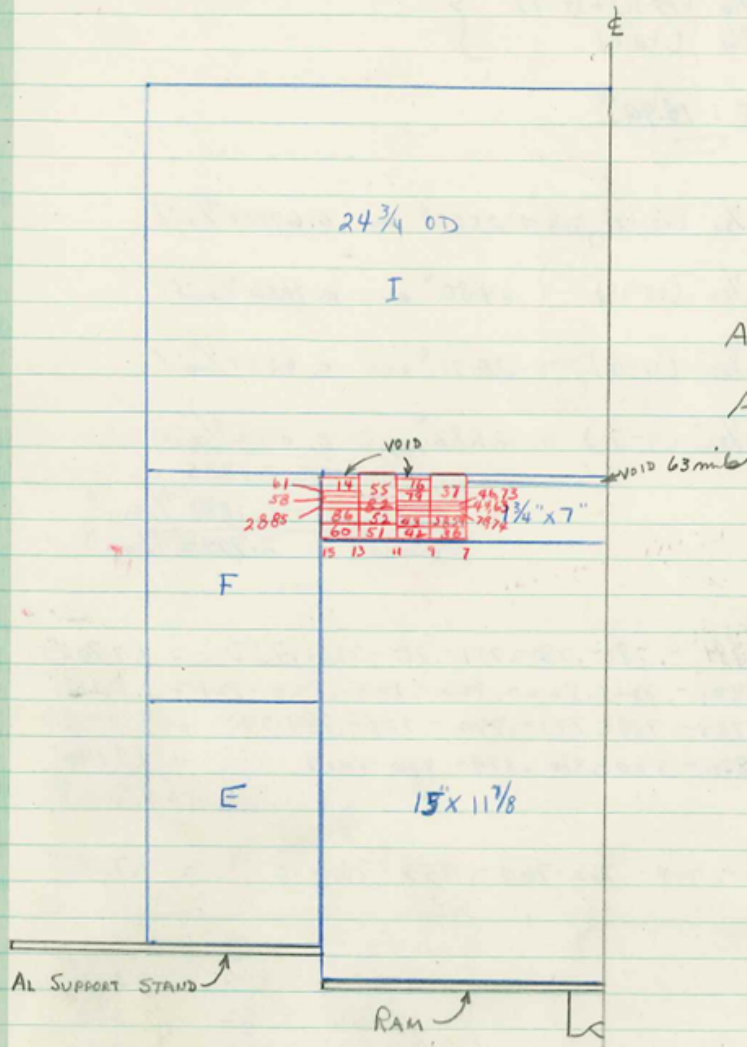
$$\begin{aligned}
 15-13 &= 1.664 - .663 - .664 - .665 - .666 - .667 = 1.6640" \\
 13-11 &= 1.664 - .664 - .664 - .665 - .664 - .664 = 1.6641" \\
 11-9 &= 1.657 - .658 - .659 - .657 - .657 - .658 = 1.6577" \\
 9-7 &= 1.662 - .662 - .663 - .663 - .665 - .666 - .666 = 1.6638" \\
 &\quad \text{avg} = 1.6625"
 \end{aligned}$$

$$30.01\% = 1.6625"$$

$$O \text{ reactivity ht} = 1.6625 - .0098 = 1.6527"$$

15"-7" INFINITE POLYETHYLENE REFLECTED + CORE

Pg 220

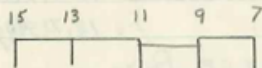


MASS OF FUEL = 76330 gm
 VOLUME = 4076.28029 cm³
 $\rho = 18.72540 \text{ gm/cc}$
 MASS OF POLY =
 VOLUME =
 $\rho = 0.916 \text{ gm/cc}$
 AVG. D.D. FUEL = 14.99589"
 $(^2) = 224.87671$
 AVG. I.D. FUEL = 7.00243"
 $(^2) = 49.03402$

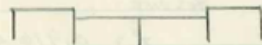
15-7 Poly + Core

$$\left. \begin{array}{l} \text{Nom. Net. Critical } 1\frac{35}{32}'' (15-13) + (11-9) \\ 1\frac{13}{16}'' (13-11) + (9-7) \\ 1\frac{3}{4}'' (\text{core}) \end{array} \right\} \text{ Reactivity} = +24.34\%$$

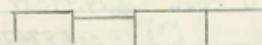
$\frac{3}{16}''$ gap between I & F : 16.90%



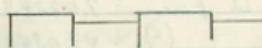
$\frac{1}{32}'' (15-13)_{\text{fuel}} = 21.22\%$ or 0.67904% mil



$\frac{1}{32}'' (13-11) = 24.80\%$ or 0.7936% mil



$\frac{1}{32}'' (11-9) = 20.71\%$ or 0.6627% mil



$\frac{1}{32}'' (9-7) = 21.82\%$ or 0.6982% mil

TOT = 2.8535

* Core = -0.1080% mil

Grand T = 2.7255% mil

fuel height 15-13 = 1.781 - .780 - .780 - .781 - .780 - .780 - .780 = 1.7802"

13-11 = 1.821 - .821 - .822 - .822 - .823 - .823 - .821 = 1.8218" ✓

11-9 = 1.789 - .789 - .790 - .790 - .789 - .789 - .790 = 1.7894"

9-7 = 1.820 - .820 - .820 - .819 - .820 - .819 = 1.8196"

wt. ht = 1.8008"

ht of Poly Core = 1.758 - .758 - .760 - .760 - .757 - .760 = 1.7588"

13-11 - 0

9-7 up 2.2 = +1.536%

11-9 up 32.4 = +21.471%

15-13 up 1.6 = +28.248%

Core up 63 = -16.80%

+68.79% = 1.8218"

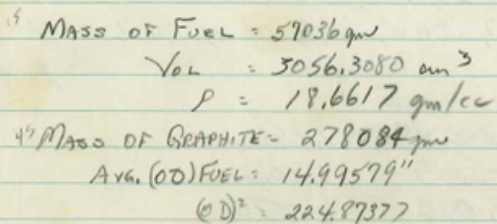
Reactiv. = 1.8218 - .0252 = 1.7966"

Void over the core is considered

$$\left. \begin{array}{l} 15-13 - 0 \\ 13-11 \text{ down} - 41.6 - 33.01\% \\ 11-9 \text{ down} - 9.2 - 6.09\% \\ 9-7 \text{ down} - 35.4 - 27.5\% \\ -42.26\% = 1.7802\% \\ 0 \rightarrow 1.7802 + .0149 = 1.7951\% \end{array} \right\}$$

* (Core vs No Core derivation)

Q 4-152



$$\text{Ref. Avg.} \left(\frac{\text{Rad} + \text{Top} + \text{Bottom}}{3} \right) = 7.0187''$$

mass of C = 278084 kg
Vol = 162507 m³
 $\rho = 1.711 \text{ g/cc}$

15" DIA. Solid & 7" ref

(15" dia)

Nom. Ht. Critical = $15 - 13 \frac{1}{2} \text{ dia} = 1 \frac{1}{2}''$
 $13 - 9 = 1 \frac{1}{2}''$

also Top Ref $\frac{1}{16}''$ extra

Reactivity = +17.15¢

Value of depth = -5.06¢
 Support = 23.03¢
 Value of 15-13 fuel = 24.98¢
 $\frac{1}{32}'' \rightarrow 13-11 = 30.41¢$
 $\rightarrow 11-9 = 36.93¢$
 $\rightarrow 9-7 = 38.27¢$
 7 dia = -

ϕ_{fuel}
~~0.7993 7806~~
~~0.9728 9903~~
~~1.1819 1154~~
~~1.2246 1196~~

OK

Make increment Calculations

$15 \frac{1}{16}'' \times \frac{1}{8}'' = 15.79¢$
 $.8'' 25 \times 21 = 7.65¢$
 $19-17 (\frac{7}{8}'') = 13.62¢$
 $15-17 \text{ ext} = 14.5 \text{ for } \frac{7}{8}''$

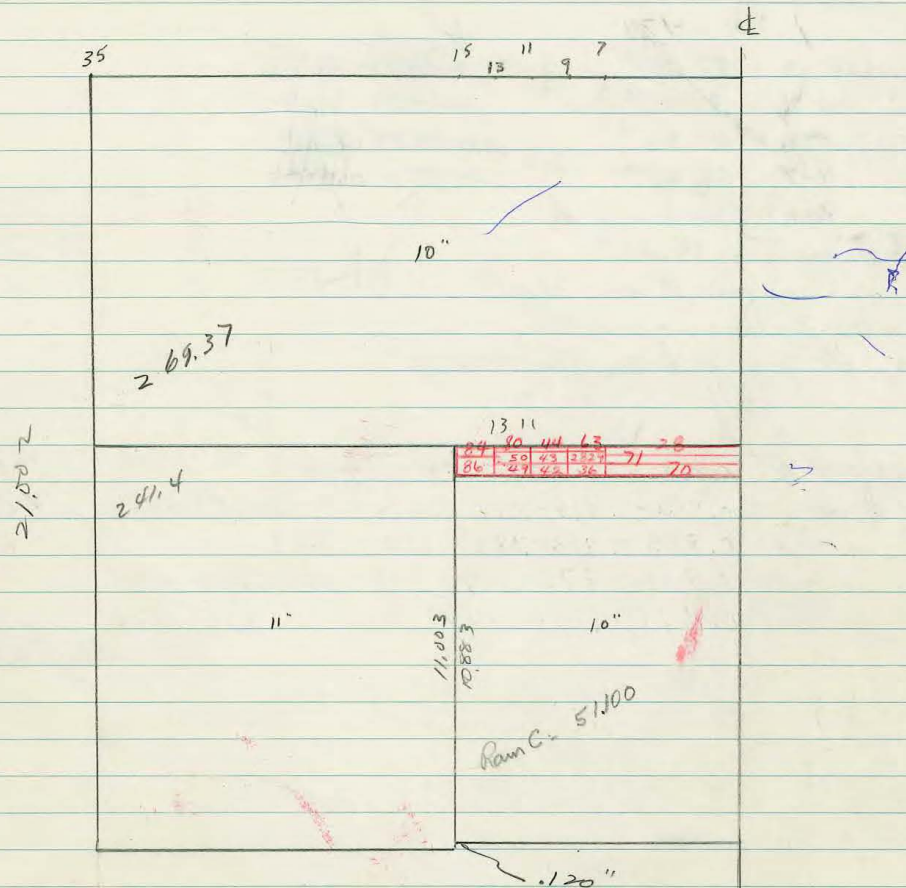
.126
 .00946
 .0156
 .0167

Ht. of fuel 15-13 = 1.065 - .065 - .065 - .065 - .065 = 1.0650
 13-11 = 1.038 - .039 - .038 - .038 - .038 = 1.0381
 11-9 = 1.042 - .042 - .042 - .042 - .043 = 1.0422
 9-7 = 1.068 - .068 - .067 - .068 - .069 - .069 - .068 = 1.0681
 7 dia = 1.067 - .067 - .067 - .066 - .066 - .067 - .067 - .067 = 1.0667
 using = 1.0560

Ht of graphite
 A = 7.050 - .057 - .058 - 0.48 = 7.0532
 B = 1.008 - .003 - .005 - .009 = 1.0062
 C = 6.020 - .012 - 5.996 - .000 = 6.0070
 D = Look Up = 6.0221
 dia up \rightarrow E = 8.990 - .987 - .984 - .987 = 8.9870
 " F = 8.918 - .914 - .917 - .917 = add (8 miles) To Avg \rightarrow = 9.0045
 " G = 9.000 - .000 - 8.996 - 8.994 = 8.9975
 " H = Look Up = 9.0003
 " I = Look Up = 9.0063

15" DIA. SOLID CYL.; 10" GRAPHITE REF.

P4-103



MASS OF FUEL = 4740.2 gm

Vol = 2541.3707 cm³

$\rho = 18.6521 \text{ gm/cc}$

AVG OD = 14.99478"

LOD = 224.84342

CMMS = 561.870 Kg

CVOL = 328584

$\rho = 1.710 \text{ gm/cc}$

AVG REF = 10.0068"

15" DIA. Cyl. #10" graphite ref.

Dem. HT Critical = $\frac{1}{8}$ " *
 reactivity = 9.56¢

$\frac{1}{32}$ " fuel 15-13 = 27.64¢

13-11 = 35.57¢

11-9 = 43.56¢

9-7 = 35.47¢

7 dia. = Could not do.

all supports = 14.25¢

{ 32 mil gap over 15" dia = 32.27¢

created by lowering ram same.

ADDED $\frac{1}{8}$ " graphite on top of fuel = +13.32¢

$\frac{1}{32}$ mil
~~0.8844 9.637~~
~~41382 1.1117~~
~~413939 1.301~~
~~41350 1.1006~~

OK

Ht. of 15-13: 0.878, .878, .878, .877, .877, .877 = 0.8775

13-11: 0.880, .879, .879, .878, .878, .881, .880 = 0.8792

11-9: 0.883, .883, .882, .882, .883 = 0.8826

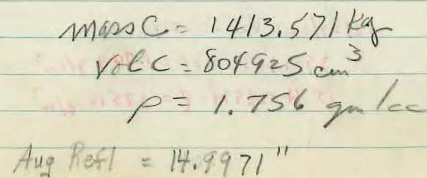
9-7: 0.878, .878, .879, .878, .879, .879, .878 = 0.8784

7 dia: 0.874, .874, .874, .874, .875, .875 = 0.8743

avg = 0.8782

* $\frac{1}{8}$ " protruding out on 35-15 ring at bottom

Pg 4-132

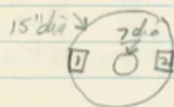
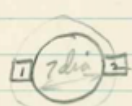


15 dia Solid & 15" Conf.

nom. Critical At. = $15 - 7 = \frac{1}{16}''^{.6975}$
 $7 \text{ dia} = \frac{1}{16}''^{.750}$ } reactivity = ∞

all supports = 2.80*

$2(2\frac{1}{2} \times 2\frac{1}{2}) @ \text{at } 700 = 17.50^*$



$2(2\frac{1}{2} \times 2\frac{1}{2}) @ \text{outer edge of } 1500 = 12.48^*$

$2(2\frac{1}{2} \times 2\frac{1}{2}) @ \text{outer edge of } 1300 = 16.11^*$

$\frac{1}{2}'' (45 - 15) \text{ Cen top} = 9.97^*$

$.0199^*$

15-13	= 0.685 - .685 - .685 - .685 - .685	0.6850
13-11	= 0.689 - .689 - .689 - .689 - .689 - .689	.6890
11-9	= 0.692 - .692 - .692 - .692 - .691 - .692	.6918
9-7	= 0.688 - .688 - .687 - .688 - .688 - .688	.6878
7 dia	= 0.750 - .749 - .749 - .750 - .749 - .750	.7495
		<u>wt avg = .7015</u>

A = Same as 4-177 = 5.0052"

$\rho \text{ of C of ram under fuel} = \frac{7107.1 \text{ gm}}{42.893, 226 \text{ cm}^3} = 1.6569 \text{ gm/cc}$
 $\rho \text{ of } 2-8'' (45 \times 15) \text{ paces} = \frac{65890.0 \text{ gm}}{370450.08 \text{ cm}^3} = 1.7786 \text{ gm/cc}$
 $\rho \text{ of } 45'' \text{ TOP} = \frac{653,600}{357450.269 \text{ cm}^3} = 1.8253 \text{ gm/cc}$

45" dia assumed
 to be 45.000 also
 wt of Pig is est.

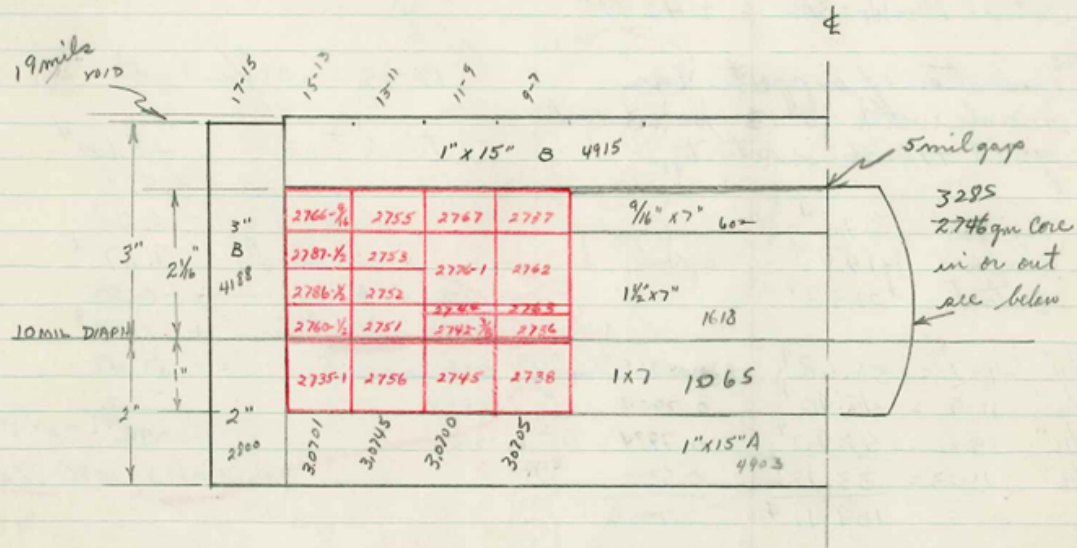
12/24/02 V.I. to T.P.

$390938.35 \rightarrow \rho = 1.749 \text{ g/cm}^3$

15 H = 14974 $\rho = 1.7516 \text{ g/cm}^3$

wt of polymers = 1.79506 gm/cc

15"-7" 1" GRAPHITE REFLECTOR WITHOUT G.CORE B 274
 15"-7" 1" GRAPHITE REFLECTOR WITH G.CORE B 276



WITHOUT CORE	WITH CORE
MASS TOP GRAPHITE = 9103 gm TOTAL = 16,806 Kg	11323 gm TOTAL = 20,091 Kg
BOTTOM = 7703 gm	8768 gm
MASS TOP FUEL = 87564 gm TOTAL = 129,884 Kg	SAME
BOTTOM = 42320 gm	SAME
AVG O.D. ALL FUEL WTD = 14.99479"	SAME
AVG I.D. ALL FUEL WTD = 7.00320"	SAME
AVG Ht ALL FUEL WTD = 3.07135"	SAME
FUEL VOLUME = 6949.28412 cm ³	SAME
FUEL ρ = 18.6902 gm/cc	SAME
Vol of graphite 19 mil gap (not incl.) = 9950.37988 cm ³ ρ = 1.68898 gm/cc	Vol of graphite 19 or 5 mil gap (not incl.) = 11885.60511 cm ³ ρ = 1.69036 gm/cc
ρ of Refl = 0.9958"	ρ of core only = 1.69947

15"-7" 1" Crp w/wd Core C7

WITHOUT Core

Critical Nom Ht = $3\frac{1}{16}" = +43.49\%$

NOTES:

* Evaluation of supports was made with 15-13 $\frac{1}{16}"$ removed gms +10.36% reactivity.

ring = 3.48%
dia = -14.9%
S. stand = 21.48%

$\frac{1}{16}"$	9-7 =	36.68%	0.5868% mil ✓
$\frac{1}{16}"$	11-9 =	49.40%	0.7904% ✓
$\frac{1}{16}"$	13-11 =	44.90%	0.7984% ✓
$\frac{1}{16}"$	15-13 =	33.13%	0.5300% ✓
		169.11%	2.7056%

Ht all FUEL

15-13 = $3.070 - .070 - .067 - .072 - .070 - .072 = 3.0701"$
13-11 = $3.075 - .073 - .075 - .075 - .075 - .074 = 3.0745"$ ✓
11-9 = $3.070 - .070 - .070 - .069 - .070 - .071 = 3.0700"$
9-7 = $3.072 - .070 - .070 - .069 - .070 - .072 = 3.0705"$
wt avg = $3.0713"$

Core Ht only = $3.066 - .065 - .066 - .066 - .066 = 3.0658"$

1 x 15 disc = $0.998" = \text{Vol} = 3066.42718 \text{ cm}^2$

1 x 15" = $0.9995" = \text{Vol} = 3071.44267 \text{ cm}^2$

17" ring = $5.043 - .043 - .046 - .045 =$

$.046 - .041 - .049 = 5.0447 \rightarrow$

Vol = 4165.51894 cm^3 w/o $\frac{1}{16}$ void
 4180.54708 cm^3 with $\frac{1}{16}$ void

TOP CTR = 3.0713"

EVEN FUEL HT. = $3.0713"$

SKY HOOK REACT. = $+33.43\%$

mil (19 mil carbon void
(17-15 ring not considered)

o React Ht = $3.059"$

With Core

17-15 = .02% mil act.

Critical Ht = $+8.66\%$
ring = 3.51%
dia = -12.48%
S. stand = 19.17%

17-15 \uparrow 19 = $+0.38\%$
React. without core = $+43.49\%$

all support = -23.47%

15-7 =

$+20.92\% = 3.0713"$

$0 = 3.0713 - .0075 = 3.0638"$

17-15 \uparrow 19 = $+0.38\%$

React with core = $+8.66\%$

all support = -10.20%

15-7 =

Core (-0.0061) \uparrow 5 = -0.03%

$-1.19\% = 3.0713"$

$0 = 3.0713 + .0004 = 3.0717"$

15-7 = 2.54% mil from curve
Core = $\frac{.0061}{2.49394\% \text{ mil}}$

EVEN FUEL HT. = $3.0713"$

SKY HOOK REACT. = -1.54%

(19 mil carbon void 17-15
5 mil void over core
not considered)

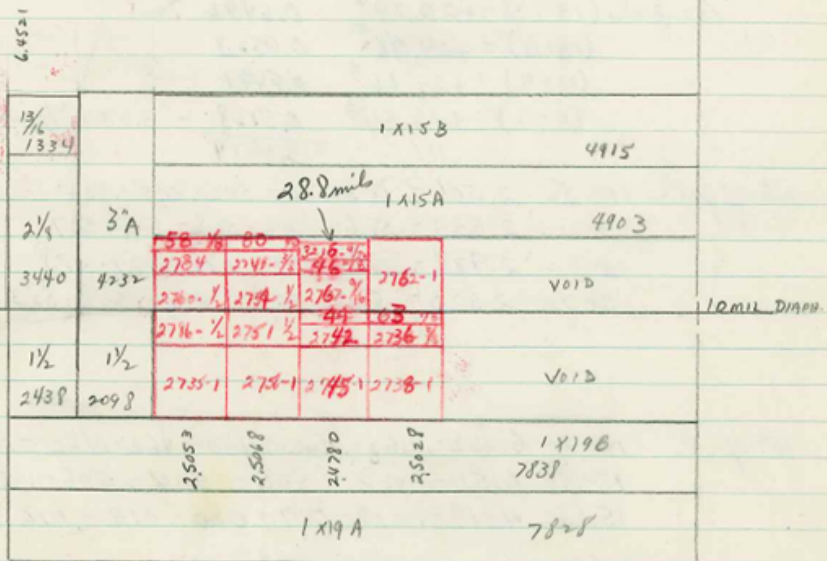
o React Ht = $3.0708"$

15"-7"

2" GRAPHITE REFLECTOR & NO CORE

28103

19-17 17-15 15-13 13-11 11-9 9-7



MASS OF FUEL = 105699 gm
 VOLUME = 5653.82352 cm³
 $\rho = 18.69513 \text{ gm/cc}$

MASS OF GRAPHITE = 39026 gm
 VOLUME = 22977.67966 cm³ ✓
 $\rho = 1.69843 \text{ gm/cc}$ ✓

AVG. O.D. ALL FUEL (WT'D) - 14.99440"
 ID = 7.00357"
 19-17 Center OD = 18.99648"
 OD² = 224.83203
 ID² = 49.04999
 360.86625

Avg Refl = 2.0019"

15-7 2" ref # No Cor

nom. Ht Critical $(15-13) + (13-11) + (9-7) = 2\frac{1}{2}"$
 $11-9 = 2\frac{1}{32}" \rightarrow + 2.27\frac{1}{32}"$

Rings = + 2.80"
Diaphragm = - 18.56"
S. Stand = + 13.89"

$\frac{1}{32}"$ fuel $(15-13) = + 20.29\frac{1}{32}"$ 0.6492 $\frac{1}{32}"$ /mil ✓
 $(13-11) = + 29.76\frac{1}{32}"$ 0.9523 ✓
 $(11-9) = + 29.66\frac{1}{32}"$ 0.9491 ✓
 $(9-7) = + 16.54\frac{1}{32}"$ 0.5168 ✓

3.080 $\frac{1}{32}"$ /mil
3.0674

Ht of fuel 15-13 = 2.506 - .503 - .506 - .506 - .505 - .506 = 2.5053"
13-11 = 2.505 - .506 - .507 - .508 - .508 - .507 = 2.5068"
11-9 = 2.978 - .478 - .479 - .476 - .479 - .478 = 2.4780"
9-7 = 2.503 - .503 - .503 - .502 - .503 - .503 = 2.5028"

w/avg = 2.4990"

Ht of C 19-17 = 6.462 - .462 - .462 - .460 - .462 - .462 - .460 = 6.4614"
17-15 = 6.511 - .507 - .505 - .504 - .506 - .508 - .509 = 6.5071"
15 dia = 4.019 - .019 - .017 - .020 - .018 - .016 - .018 = 4.0181"

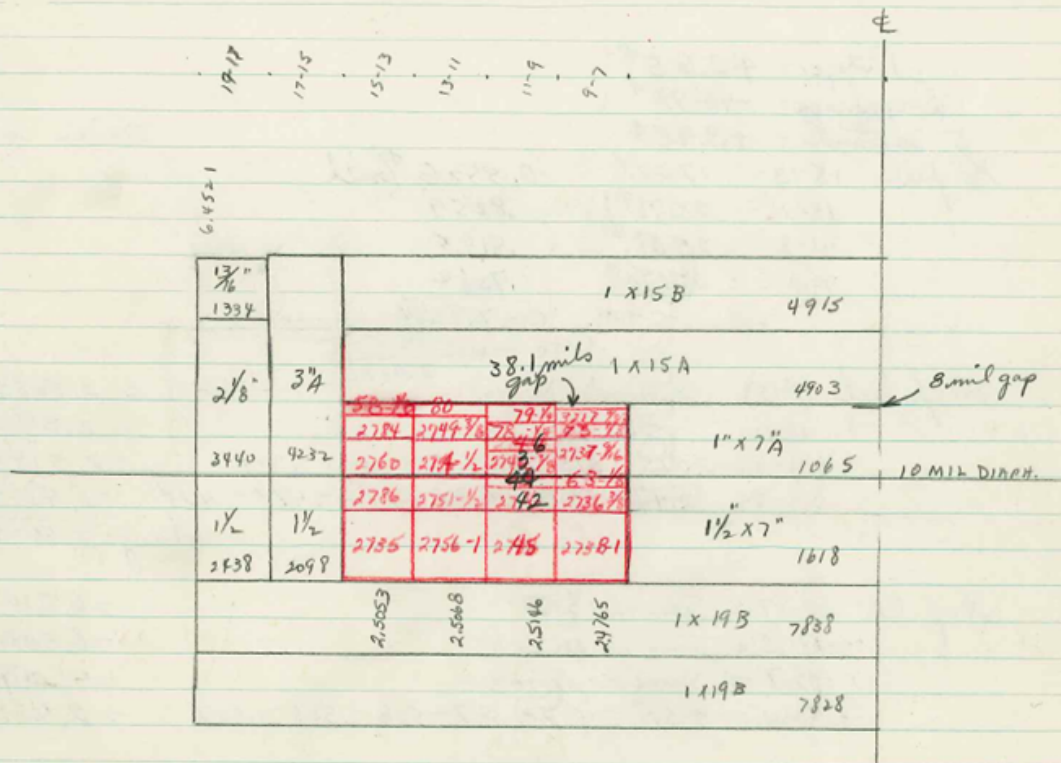
Even Fuel Ht = 2.4990"
Sky Hook React = + 4.14"

o React = 2.498" ✓

Reactivity $\rightarrow = + 2.27$
19-17 mil = 0
15-7 = 0
all support = + 1.87

+ 4.14 = 2.4990"
 $0 = 2.4990 - .0013 = \underline{2.4977}"$

2 Pg 109



MASS OF FUEL = 105792 gm
VOLUME = 5664.05719 cm³
 $\rho = 18.67777 \text{ gm/cc}$

MASS OF GRAPHITE: 41709 gm
VOLUME = 24559.66978 cm³
 $\rho = 1.69827 \text{ gm/cc}$

Avg. CD. ALL FUEL (w't'd) = 14.99440" OD² = 224,83203
 ID = 7.00263" ID² = 49,03682
 19-17 Carbon OD = 18.99648" ——— : 360,96625

Aug Repl = 2.0019"

15-7 2" ref. + core

Nom. Net Critical 15"-9" = 2 1/2" & 9"-7" = 2 15/32" \rightarrow reactivity = -5.43%

Rings = +2.65%
 Diaphragm = -15.73%
 5. Stand = +9.95%
 1/32" fuel 15-13: 17.27% 0.5526 %mil ✓
 13-11: 25.81% .8259 ✓
 11-9: 25.61% .8195 ✓
 9-7: 22.70% .7264 ✓
 Avg 2.9244
 Core = .0007

Raise 1001"

1st. of fuel 15-13: Same as No core = 2.5053"
 13-11: Same = 2.5068"
 11-9: 2.515, .515, .516, .513, .515, .514 = 2.5146"
 9-7: 2.478, .476, .474, .476, .477, .478 = 2.4765"
 wt avg = 2.5025"

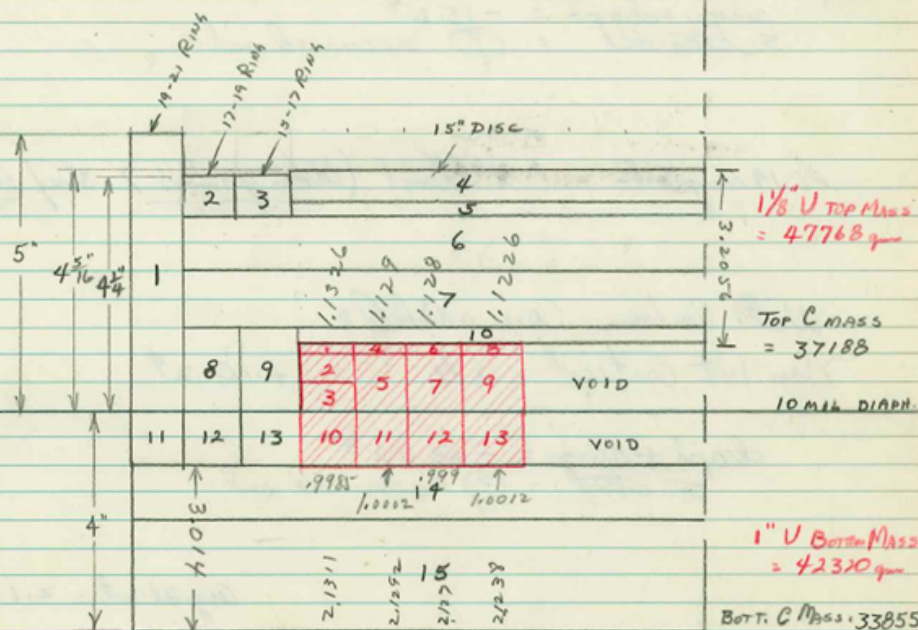
1st of C 19-17: Same as 103 = 6.4614" (100)
 17-15: Same as 103 = 6.5071" ✓
 15-7: Same as pg 103 = 4.9181"
 Core: 2.508, .507, .507, .506, .505, .507 = 2.5066"

0 React 14+ = 2.5035" ✓

React \rightarrow = -5.43%
 all support = +3.13
 19-17 ml = 0
 15-7 = 0
 Core (-) ml = 0
 -2.304 = 2.5025"
 ① = 2.5025" + .0007 = 2.5032"

15-7- 3" C VOID

From Fig 40



Pos.	#	Mass	Pos.	Size	Mass
1	2758 (1/8")	1685	1	1" x 5" (19-21) RING	8827
2	2848 (1/2")	6748	2	1" x 3/4" (17-19) RING	1255
3	2787 (1/2")	6788	3	1" x 3/8" (15-17) RING	1060
4	2781 (1/8)	1449	4	3/8" x 15" Disc	2763
5	2757 (1")	11575	5	1/4" x 15" Disc	1224
6	2744 (1/8")	1223	6	1" x 19" Disc A	7828
7	2776 (1")	9644	7	1" x 19" Disc B	7838
8	2763 (1/8")	953	8	1" x 1 1/2" (17-19) RING	2452
9	2762 (1")	7703	9	1" x 1 1/2" (15-17) RING	2100
10	2735 (1")	13409	10	3/8" x 15" Disc	1841
11	2756 (1")	11567	11	1" x 1" (19-21) RING	1828
12	2745 (1")	9634	12	1" x 1" (17-19) RING	1644
13	2738 (1")	7710	13	1" x 1" (15-17) RING	1454
			14	1" x 21" Disc	9666
			15	2" x 21" Disc	19263

22489201
Avg Fuel OD = 14.99640"
ID = 7.00375"
49.05251

Fuel vol. = 4816.68180 cm³
 $\rho = 18.70333 \text{ gm/cc}$

graphite vol. = 41813.76277 cm³
 $\rho = 1.69903 \text{ gm/cc}$

Avg Refl = 3.0101"

15" 7" 3" C ref WO core

$$\text{Nom. Wt Critical} = 2\frac{1}{8}" = +22.05\frac{1}{2}$$

$$\begin{aligned} \text{rings} + \text{diag} &= -15.2\frac{1}{2} \\ \text{S. stand} &= (?) \text{ assumed mil} \end{aligned}$$

$$21-19 \text{ ring center} = 0.0176\frac{1}{2} \text{ mil (taken from 15.7 3" ref Q 111)}$$

With Carbon Core added:

$$\text{Nom. Wt Critical} = 2\frac{1}{8}" = +10.2\frac{1}{2}$$

$$\begin{aligned} \text{diag} + \text{rings} &= -13.02\frac{1}{2} \\ \text{S. stand} &= (?) \text{ assumed mil} \end{aligned}$$

$$\text{Avg. Wt. wt.} = 2.1283"$$

$$\begin{aligned} \text{React} &= +22.05\frac{1}{2} \\ \text{all support} &= +4.40 \\ 19-17 \text{ assum mil} &= +26.45\frac{1}{2} = 2.1283" \\ O &= 2.1283 - .0086 = \underline{2.1197"} \end{aligned}$$

Rings 2.75
Stand 10.8
diag 1.795

$$\text{EVEN FUEL NT.} = 2.1283"$$

(7)
1

15-7 3"ref + No Core

'''

Nom. HT. Critical $(9-7 \& 13-11) - 2\frac{5}{8}"$ } reactivity + 1.39¢
 $(11-9 \& 15-13) = 2\frac{1}{8}"$

Rings = + 3.59¢
 Diaphragm = - 20.38¢
 S. Stand = + 11.73¢

Lower .0019"

all $\frac{1}{32}"$ fuel 15-13 = 25.08¢
 13-11 = 33.88¢ \$ 35.64¢ avg 34.76
 11-9 = 23.94¢ \$ 26.03¢ avg 24.98
 9-7 = 23.70¢
 Nom. $\frac{1}{4}"$ C on 19-17 ring = 4.4¢

0.8025¢/mil
 1.1123
 0.7660
 0.7584
 3.4392¢/mil

HT all fuel 15-13 = 2.130 - .130 - .129 - .130 - .130 - .129 = 2.1296"
 13-11 = 2.161 - .161 - .161 - .163 - .163 - .164 = 2.1621"
 11-9 = 2.137 - .136 - .136 - .136 - .136 - .134 = 2.1358"
 9-7 = 2.165 - .165 - .163 - .164 - .165 - .165 = 2.1645"
 w avg = 2.1462"

HT Carbon 21-19 = 8.165 - .160 - .155 - .150 - .155 - .162 = 8.1578" (11)
 19-17 = 8.020 - .017 - .014 - .014 - .020 - .022 - .023 = 8.0185" (12)
 17-15 = 8.204 - .208 - .201 - .192 - .198 - .199 - .204 = 8.2008" (13)
 15-7 = Same as 12 = 6.0168"

OK

Correct flat fuel HT = 2.1443" ✓

Reactivity = → = + 1.39¢
 all support = + 5.06
 21-15 ↑↓ NIL = 0
 15-7 = 0
 + 6.45¢ = 2.1462"
 0 = 2.1462 - .0019 = 2.1444"

15-7

3" GRAPHITE REFLECTOR + GRAPHITE CORE

19² 117

[illegible]

MASS OF FUEL = 91182 gm
VOLUME = 4878.46714 cm³
 $\rho = 18.690707 \text{ gm/cc}$

MASS OF GRAPHITE: 7055/gm
VOLUME = 41360.76837 cm³
 $\rho = 1.70574 \text{ gm/cc}$

AVG. O.D. ALL FUEL (WTD) = 14.99480" O.D.: 224.84402
I.D. = 7.00335" I.D.: 49.04691
21-19 O.D. carbon = 20.99959" 440.98278

Aug. Repl = 2.999"

15-7 3" ref + Core

Nom. Ht. Critical: $15-9 = 2\frac{5}{32}" + 9-7 = 2\frac{1}{8}"$

Reactivity = +15.69¢

Rings = +2.92¢
Diaphragm = -16.10¢
5. Stand = +9.58¢

Lower .0055"

1/32" fuel	15-13 = 24.38¢	0.7801 ¢/mil ✓
	13-11 = 33.78¢	1.0809 ✓
	11-9 = 29.90¢	0.9568 ✓
	9-7 = 21.45¢	0.6864 ✓
	<u>3.5042</u>	
	Core(-) <u>.0100</u>	
	<u>3.4942</u>	

Ht. of fuel	15-13 = 2.160 - .160 - .161 - .160 - .164 - .161	= 2.1610"
	13-11 = same as 11	= 2.1621"
	11-9 = 2.162 - .163 - .163 - .160 - .163 - .163	= 2.1623"
	9-7 = 2.132 - .132 - .131 - .131 - .130 - .130	= 2.1310"
	avg	= 2.1561"

Ht. of Carbon	21-19 = Same as Pg 111	= 8.1578" ✓
	19-17 =	= 8.0185" (-138)
	17-15 =	= 8.2008" (+54)
	15-17 =	= 6.0168"
	Core = 2.137 - .135 - .135 - .138 - .139 - .137 - .137	= 2.1368"

correct flat fuel Ht = 2.1506" ✓

[core gap not considered] OK

React	= +15.69¢
all support	= +3.60
21-15 mil	= 0
15-7	= 0
Core	↑ 19.3 = -0.19
	+ 19.10¢ = 2.1561"
	0 = 2.1561 - .0054 = <u>2.1507"</u>

11. 1871

Year	1871	1872	1873	1874	1875	1876	1877	1878
75-21								
21-19								
19-12								
17-15								
15-13								
13-11								
11-9								
9-7								

	1 1/8"	1 1/2"	1 3/4"		1/8 x 15	625
		111	1170		3/8 x 15	1841
1.2"	1 1/8"		3/8		1 1/2 x 15	7485
4895	1 1/8"	1 1/2"	1233			
	2"	2438				
	3546		1 1/2"		1 x 15 C	4915
4 1/2"			2098			
	4"				1 x 15 B	4915
18455	3"	3"B		28.8mil gap 32.5mil	1 x 15 A	4913
	6513	4188				
5305						
	1"	1"	1"			
1828	1644	1456				
3"						
12350						

MASS OF FUEL : 72382 gm
VOLUME = 3879.89390 cm³
 ρ : 18.65566 gm/cc

MASS OF GRAPHITE: 151179 gm
VOLUME = 88025.00261 cm³
 $\rho = 1.71745 \text{ gm/cc}$

Avg. Repl. = 4.998"

Avb. O.D. ALL FUEL (W'T b): 14.99612"
I.D. = 7.00250"
25-21 OD Carbon = 24.99799"

$OD^2 = 224.88361$
 $ID^2 = 49.03500$
 ————— 624.89950

15-7

5" ref # No Core

1.702

Dem. Nt. Critical $(13-11) \div (9-7) = 1.6875 (1\frac{1}{16}) \rightarrow \text{reactivity} = +3.28\%$
 $(15-13) \div (11-9) = 1.71875 (1\frac{23}{32})$

Rings = +3.63%

Diaphragm = -13.92%

S. Stand = +5.46%

 $\frac{1}{32}$ " fuel 15-13 = +27.51%

13-11 = +36.76%

11-9 = +37.16%

9-7 = +28.86%

600 mils carbon 25-21 = +5.39%

Nt of fuel

15-13 = 1.728 - .728 - .727 - .728 - .729 - .728 = 1.7280"

13-11 = 1.700 - .698 - .699 - .700 - .699 - .700 = 1.6993"

11-9 = 1.728 - .728 - .728 - .729 - .728 - .728 = 1.7281"

9-7 = 1.696 - .696 - .695 - .697 - .695 - .695 = 1.6956"

wt val Avg = 1.7134"

Lower 0.0019"

0.88034/mil
1.1763
1.1891
0.9235
0.08984/mil

= 4.16924/mil

Wt of Carbon 25-21 = 5.5115 + [5.6900] = 11.2015" (-529)

21-19 = 5.4986 + [6.140 - .142 - .141 - .150 - .146 - .148 - .150] = 11.6438" (-79)

19-17 = 5.5053 + [6.205 - .195 - .194 - .190 - .199 - .201 - .200] = 11.7030" (-18)

17-15 = 5.5052 + [6.226 - .223 - .224 - .224 - .224 - .225] = 11.7295" (+9)

15 dia. = 5.0031 + [5.016 - .016 - .016 - .016 - .017 - .017 - .016] = 10.0193"

Raise 0.0010"

Corrected flat fuel = 1.7125"

React. = +3.28%

all support = +4.73

25-21 \uparrow 519 = +4.66

15-7

+ 12.67% = 1.7134"

0 = 1.7134 - .0030 = 1.7104"

NOTE: FUEL SAME AS NO CORE CONF.
GRAPHITE SAME AS NO CORE CONF. EXCEPT CORE IS ADDED.

GRAPHITE
5" REFLECTOR + GRAPHITE CORE

Pg 164

[illegible]

MASS OF FUEL = 72382 gm
VOLUME = 3879.89390 cm³
 $\rho = 18.65566 \text{ gm/cc}$

Mass of GRAPHITE: 152.987 gm
VOLUME: 89098.38333 cm³
f = 1.71705 gm/cc

$$\text{Avg Refl} = 4.998''$$

Av. OD. ALL FUEL (w't'd) = 14,99612"
ID: 7.00250"
25-21 OD Carbon = 24.99799"

$OD^2 = 224.88361$
 $2D^2 = 49.03500$
 $\quad \quad \quad 624.89950$

15-7 5" ref + core

Dem. Ht. Critical (13-11) + (9-7) = $1\frac{1}{16}$ reactivity = $+1.70^4$
 (15-13) + (11-9) = $1\frac{3}{32}$

Rings = $+3.58^4$
 Diaphragm = -15.22^4
 S. Stem = $+5.67^4$

Lower 0.0017"

$\frac{1}{32}$ " fuel 15-13 = 31.30^4 1.0016 $\frac{4}{\text{mil}}$ → TOTAL = 45353
 13-11 = 38.69^4 1.2380
 11-9 = 41.49^4 1.3276
 9-7 = 30.25^4 0.9680
 wt vol Avg = $4.5353^4/\text{mil}$
 Core = $+0.079$
 4.5432
 ≈ 600 mils carbon on 25-21 = 5.35^4 or $.00898^4/\text{mil}$ ← this data from No core run.

Measurements same as 15-7 (5") & No Core

FUEL 15-13 = } as pg 162
 13-11 :
 11-9 :
 9-7 : }

= 1.7280"
 = 1.6993"
 = 1.7281"
 = 1.6956"

wt vol Avg = 1.7077"

Carbon 25-21 : }
 21-19 : }
 19-17 : }
 17-15 : }
 15 dia : }

= 11.2015" (-506)
 = 11.6438" (-64)
 = 11.7030" -
 = 11.7295" (+22)
 = 10.0193"
 = 1.7008"

Core hly = 1.700 - .700 - .700 - .701 - .702 - .703 - .700

Raise 0.0010"

NOTE: B1672 "clean" changed to comparable configuration but put all fuel on top of diaphragm : reactivity = $+8.26^4$
 diaphragm = $+0.58^4$

corrected flat fuel height = 1.7070"
 React = $+1.70^4$; all support = $+5.97^4$; 25-21 + 519 = $+4.66^4$;
 15-7 = 0; Core + 6.9 = $+0.05$ = $+12.38^4 = 1.7077"$
 0 = $1.7077 - 0.027 = 1.7050"$

15"-7"		7" GRAPHITE # No CORE				<u>Also + CORE</u>		Pg 282
29	25	21	19	17	15	13	11	
1 1/2	1.2	3/4	2 1/8	1 1/6	1	1 x 13	3682	
7427	4895	1364	3440	13/16	1262			
				1170				
		3		1	1 1/2	1 1/2 x 13	5509	
		5525		1456	1890			
			3 3/8			1/2 x 15	2467	
			3863	38		1 x 15 D	4781	
				4188		1 x 15 C	4915	
9	7					1 x 15 B	4915	
	28700	5						
		8827	4			1 x 15 A	4903	
43550			6513	3A				
				4232				
						2885 82 74 75	3/8 x 7 404	IN OR OUT
						66 55 67 37	1/16 x 7 602	
						58 50 78 74	1/2 x 7 536	
						60 51 42 36		
						2 x 25	27650	
							15 mil DIAP.	
						1/2 x 25	6868	
		1 1/2	1 1/2	1 1/2		1 1/2 x 15	7485	
5	4 1/2	2677	2438	2098				
						1 x 21	9666	
24550	18455							
						2 x 21	19263	

No Core 61071
 MASS OF FUEL = 62699 gm
 Vol. = 3268.67272 cm³
 ρ = 18.68323 gm/cc
 No Core
 MASS OF GRAPHITE = 281364 gm
 Vol. = 163150.5025 cm³
 ρ = 1.7245 gm/cc

Avg Refl = 6.997"
 + Core Same
 + Core graphite mass = 282906 gm
 Vol. = 164062.92686 cm³
 ρ = 1.72437 gm/cc
 Avg. OD. fuel = 14.99585 (224.87551)
 Avg. ID = 7.00248 (49.03472)

15-7 7" ref. & No CORE

SEE + Core Below

nom. ht. Critical = $1\frac{7}{16}$ "

reactivity = $+17.55\%$

Fuel value ($\frac{1}{32}$ ") = 15-13 = $+42.61\%$
 13-11 = $+65.86\%$
 11-9 = $+47.40\%$
 9-7 = $+40.98\%$

✓ 1.3635 $\frac{\%}{\text{mil}}$
 ✓ 2.1075
 ✓ 1.5168
 ✓ 1.3113
 6.2991

REACTIVITY = $+17.55\%$
 29-25 \downarrow 95 mils = -0.10
 25-21 \uparrow 264 mils = $+1.05$
 21-19 \downarrow 349 mils = -3.62
 19-17 \downarrow 64 mils = -0.89
 17-15 \downarrow 41 mils = -0.84
 ALL SUPPORT = -2.67%

ring & ring support = $+4.32\%$
 support stand }
 diaphragm } = -1.65

$\frac{1}{8}$ " x 13" dia carbon top = $+17.24\%$
 (773 mils) 21-19 ($\frac{3}{4}$ ") = 8.97%

1.4443" = $+10.28\%$
 -1.6 mils = 1.4427 " ∞

15-7 7" ref + core 1st: $1\frac{7}{16}$ " \rightarrow reactivity $+18.41\%$

diaphragm = -2.68%
 ring & ring support & support stand = $+5.74\%$

Fuel value ($\frac{1}{32}$ ") 15-13 = 28.00%
 13-11 = 49.01%
 11-9 = 34.55%
 9-7 = 39.0%

✓ 0.8960 $\frac{\%}{\text{mil}}$
 ✓ 1.5683
 ✓ 1.1056
 ✓ 1.2480
 4.8179

+ Core
 React = $+18.41\%$
 ALL SUPR = -3.06
 ALL Carbon = -4.60
 Core = $\frac{NIL}{1.4443} = +10.75\%$
 -2.2 mils = 1.4421 " ∞

1st. of fuel 15-13 = 1.444 - 445 - 444 - 445 - 445 - 445
 13-11 = 1.445 - 445 - 445 - 445 - 445 - 445
 11-9 = 1.443 - 444 - 445 - 445 - 445 - 446
 9-7 = 1.443 - 443 - 443 - 442 - 442 - 443 - 443

1.4446"
 1.4450"
 = 1.4446"
 = 1.4427"

wt avg = 1.4443"

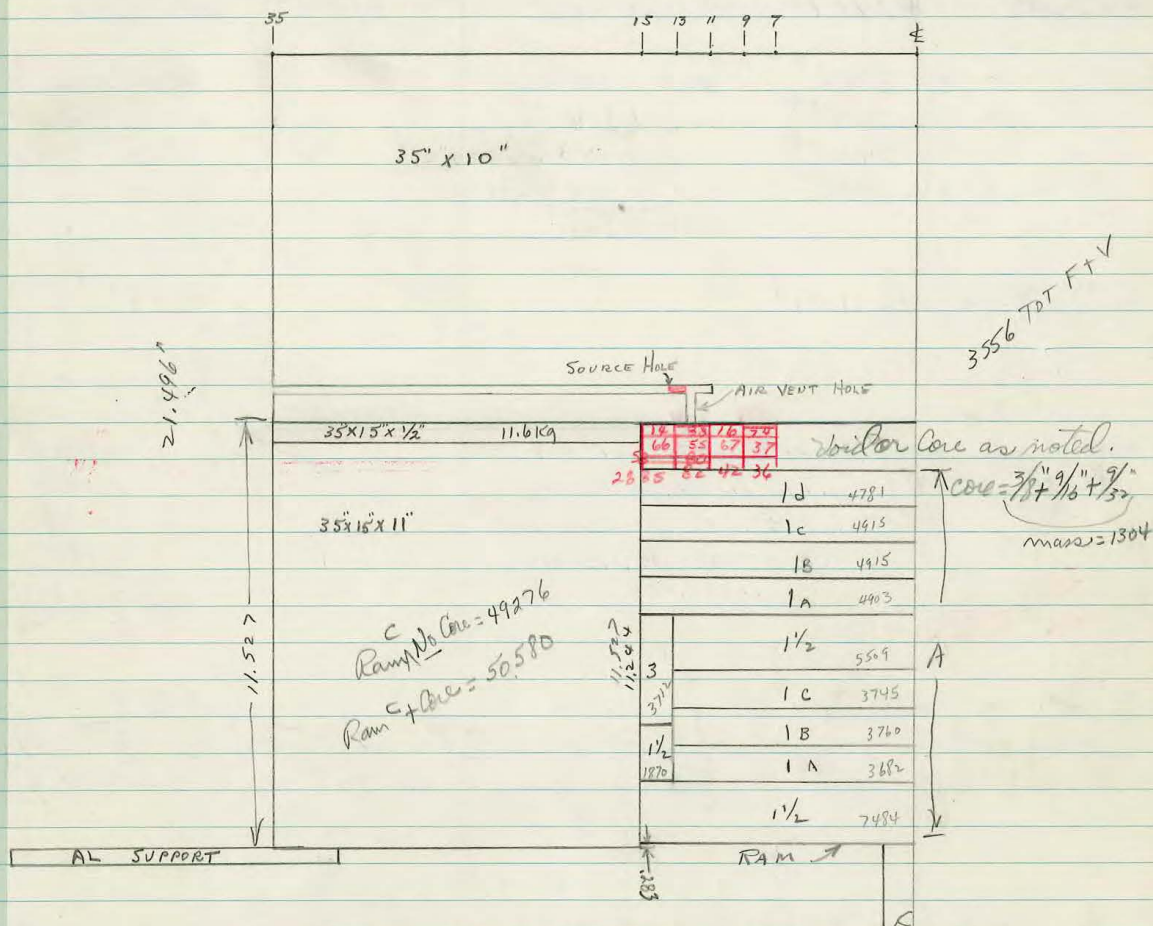
Part measured carbon heights in the drawing
 Core = 1.447 - 447 - 446 - 445 - 445 - 445 - 447 = 1.4460"

29-25 = 15.522 - .538 - .550 - .550 = 15.5400"
 25-21 = 15.179 - .175 - .186 - .180 = 15.1800"
 21-19 = 15.794 - .795 - .796 - .790 = 15.7937"
 19-17 = 15.515 - .506 - .505 - .502 = 15.5085"
 17-15 = 15.491 - .486 - .490 - .477 = 15.4860"
 15-13 = 14.049 - .029 - .050 - .036 = 14.0410"

13" dia = 14.005 - .026 - .027 - .015 = 14.0182"

15"-7" 10" GRAPHITE REFLECTOR. \$ No CORE \$ + Core as noted

Pg 52



MASS OF FUEL: 51146 gm
Vol. : 2745.4359 cm³
 $\rho = 18.6367 \text{ gm/cc}$
MASS OF GRAPHITE = 49427 gm
RAM GRAPHITE + CORE = 50580 gm

Avg. WID OD = 14.99716" OD² = 224.91480
ID = 7.00216" ID² = 49.03024

Avg. Refl. = 10.012"

TOT. No Core C = $49.276 + 241.4 + 11.6 + 269.37 = 571.646 \text{ Kg}$; Vol = 335358 cm^3 ; $\rho = 1.704 \text{ g/cm}^3$
Total with Core = $571.646 + 1304 = 572.950 \text{ Kg}$; Vol = 336169 cm^3 ; $\rho = 1.704 \text{ g/cm}^3$

15-7 10" Cref. + Void core + \pm Core as noted

clean Critical Mem. HT. = $(15-13) \div (11-9) = 1\frac{1}{2}"$; $(13-11) \div (9-7) = 1\frac{3}{4}"$
 Reactivity : +24.07¢ with no core + 31.29¢ with core

$\frac{1}{32}"$ Value	15-13 = 37.06¢	or \checkmark 1.186¢/mil	36.16¢	or 1.157¢
	13-11 = 56.68¢	\checkmark 1.814¢/mil	49.39¢	or 1.580¢
	11-9 = 54.47¢	\checkmark 1.743¢/mil	47.26¢	1.512¢
	9-7 = 34.48¢	\checkmark 1.103¢/mil	32.09¢	1.026¢
		TOTAL 5.846		

all Support value = 11.01¢

8.84¢

HT of fuel 15-13 = 1.228¹²²⁸ - 228 - 228 - 227 - 227
 13-11 = 1.196 - 196 - 196 - 196 - 196
 11-9 = 1.228 - 228 - 228 - 228 - 228
 9-7 = 1.193 - 193 - 194 - 193 - 194
 194 - 194 = 1.1935

Same
 Same
 1.2276"
 1.1960
 1.2278
 1.1935
 uTavg = 1.2128

clean critical ^{with Core} compared to above but with the ^{graphite} $\frac{1}{2}" \times (35" \times 15")$
 disc removed = The $\frac{1}{2}"$ price 22.39¢ or 0.04478¢/mil

A 10.017 - .020 - .016 - .012 = 10.0162

A = Same = 10.0162
 Core = 1.223 - .222 - .221 - .222 = 1.220

HT = 1.213"
 or 1.211"/mil

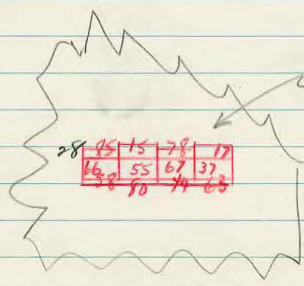
1.213"
 1.209"/mil

15" x 7" & 15" GRAPHITE REFLECTOR

NO CORE
+ CORE

Eq 4-177

45 25 15 13 9 7



FUEL FOR NO CORE.
GRAPHITE IS SAME

281.3 cm³ TOT V+P

30.110"

683.6

2202 cm³

Carbon
No Core

mass =
1413.571 kg
Vol =
804872 cm³
ρ = 1.756 gm/cc

330.1

328.8

13-11			
28	85	15	17
16	55	67	37
38	50	44	46

1	1/2
2	1/2

B
↑
A
↓

Carbon
+ Core

mass = 1414.601
Vol = 805483 cm³
ρ = 1.756 gm/cc

10
R_{am C} (No Core) = 71071
R_{am C} (+ Core) = 72101

VOL FUEL = 2152.2276 cm ³	Core	No Core	Vol = 2166.5832
MASS OF FUEL = 40133 gm			40406 gm
Av _h OD _{FUEL} = 14.99625" (2) = 224.88751		Same	
Av _h ID _{FUEL} = 7.00220" (2) = 49.03080			7.00164" (2) = 49.02296
MASS OF GRAPHITE =			
FUEL ρ = 18.6471 gm/cc			18.6496 gm/cc
			Aug. Refl = 14.997"

15-7 # 15" C. ref. + Core

No Core

Mom. Ht. Critical: (15-11 # 9-7) @ $\frac{15}{16}$ "; (15-13 # 11-9) @ $\frac{31}{32}$ "; (13-11 # 9-7) @ $\frac{15}{16}$ "
(11-9) @ $\frac{31}{32}$ "

reactivity = -5.54%

+24.90%

$\frac{1}{32}$ " fuel value: 15-13 = 39.88%

13-11 = 48.44%

11-9 = 47.14%

9-7 = 27.68%

$\frac{1}{16}$ "

1.2761

1.5500

1.6084

1.8858

$\frac{1}{8}$ "

39.89%

44.51%

45.63%

36.93%

$\frac{1}{4}$ "

1.2764

1.4243

1.4601

1.1817

all supports = 2.22%

2.47%

Ht. of fuel: 15-13 = 0.951 - .948 - .948 - .951

13-11 = 0.942 - .942 - .942 - .942

11-9 = 0.971 - .971 - .971 - .972 - .972 - .972

9-7 = 0.941 - .941 - .941 - .941 - .941 - .941

for ship
inches →

as chosen

avg = 0.9509

Same only on 15-13

0.972 - .972 - .972 - .971 - .971 - .972

0.940 - .940 - .940 - .939 - .939 - .940

0.941 - .941 - .941 - .941 - .941 - .940

.971 - .971 - .971 - .972 - .972 - .971

avg = .9572

A = $\frac{5.005}{5.005 - .005 - .006 - .005} = 5.0052$

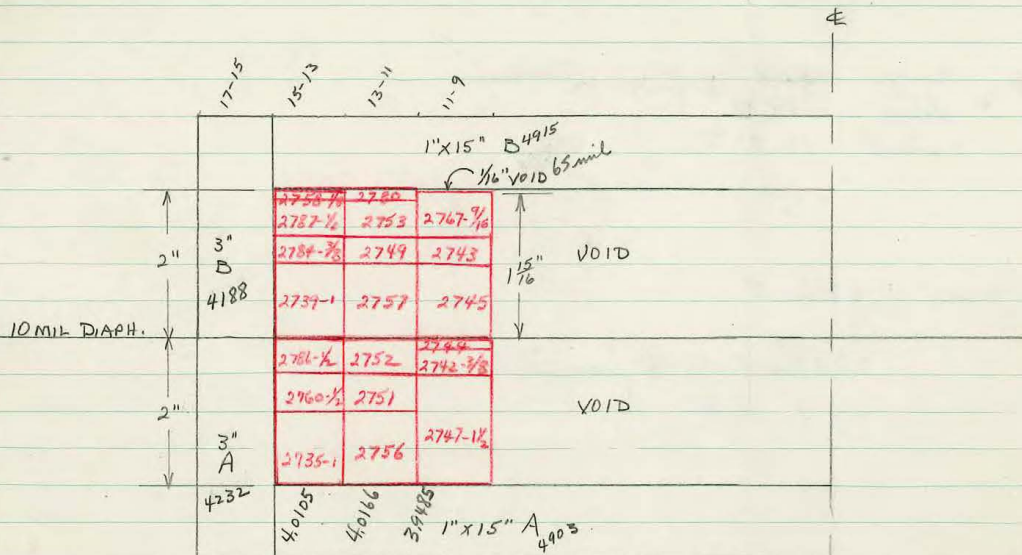
B = 0.970 - .971 - .970 - .969 = 0.9700

$\frac{4.150}{1} = 4.150$

$\frac{0.957}{0.957} = 1$

15"-9" 1" GRAPHITE REFLECTOR #VOID CORE

Pg 263



MASS OF TOP GRAPHITE = 9103 gm TOTAL = 18.238 Kg

BOTTOM = 9135 gm

MASS OF TOP FUEL = 68795 gm TOTAL = 138.140 Kg

BOTTOM = 69345 gm

AVG. O.D. ALL FUEL (wt'd) = 14.99475" AVG I.D. (wt'd) = 9.00175"

AVG. Ht ALL FUEL (wt'd) = 224.84252" 8103150

FUEL VOLUME = 7394.96904 cm³

FUEL ρ = 18.68026 gm/cc

graphite volume = 10768.40825 cm³

ρ = 1.69365 gm/cc

Avg Refl = 0.999"

15"-9" 1" Conf. WO Core

Non. Ht Critical 4" on 15-11 $\pm 3\frac{15}{16}$ on 11-9 = +20.95"

rings: 5.19"
diaph: -19.38"
5. stand: 16.32"

11-9 fuel \triangleq .63"/mil

1.83"/mil 15-9 from Curve
1.87 used

Ht ALL FUEL = 15-13 = 4.009 - .009 - .011 - .013 - .012 - .009 = 4.0105"
13-11 = 4.015 - .017 - .017 - .017 - .018 - .016 = 4.0166"
11-9 = 3.946 - .946 - .948 - .951 - .952 - .948 = 3.9485"
wtavg = 3.9953"

1X15B = 0.998

1X15A = 0.9995

(17-15) 3+3 = 6.035 - .035 - .035 - .037 - .034 - .035 = 6.0351 (+40 mils)

CARBON TOP 17-15 = 3.009

15-9 = 0.998

EVEN FUEL HT. = 4.0133" or 3.9953"
SKY HOLE REACTIVITY = +59.77% + 18.92%

0 React fuel Ht = 3.9898"

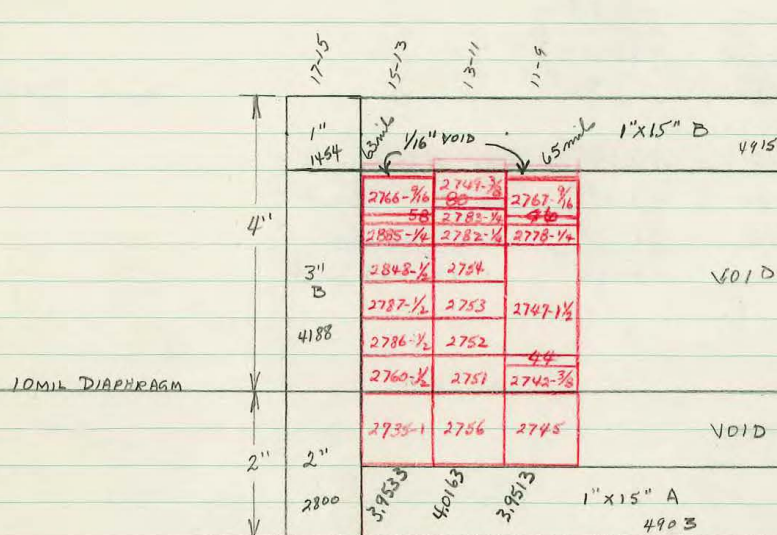
REACT. = +20.95"
ALL SUPPORT = -2.13"
+18.82 = 3.9953"
0 = 3.9953 - .0102 = 3.9851"

15" - 9"

1" GRAPHITE REFLECTOR

WITHOUT CORE

Run 10e

2-279
Pg 280

MASS OF TOP GRAPHITE = 10557 gm TOTAL = 18.260 Kg
 BOTTOM = 7703 gm

MASS OF TOP FUEL = 102891 gm TOTAL = 137.501 Kg
 BOTTOM = 34610

AVG. O.D. ALL FUEL (WT'D) = 14.99515" (2) 224.85452

AVG. I.D. ALL FUEL (WT'D) = 9.00169" (2) 81.03042

~~AVG HE. ALL FUEL (WT'D) =~~

FUEL VOLUME = 7355.77849 cm³

FUEL ρ = 18.6929 gm/cc

graphite vol. = 10741.91021 cm³
 ρ = 1.69988 gm/cc

Avg. Refl = 0.999"

15"-9" 1" Cnf WD Core(C)

$$3\frac{15}{16}m(15-13) + 4" \text{ on } 13-11 = +0.67\frac{1}{4}$$

$$\begin{aligned} \text{ring} &= 5.58\frac{1}{4} \\ \text{shape} &= -10.52\frac{1}{4} \\ \text{stand} &= 17.36\frac{1}{4} \end{aligned}$$

Raise .0064"

$\frac{1}{16}$	Ring	$= 39.44\frac{1}{4}$	or	$0.6318\frac{1}{4}/\text{mil} \checkmark$
$\frac{1}{16}$	11-9	$= 43.28\frac{1}{4}$	or	$0.6524\frac{1}{4}/\text{mil} \checkmark$
$\frac{1}{16}$	13-11	$= 31.78\frac{1}{4}$	or	$0.5084\frac{1}{4}/\text{mil} \checkmark$
		<u>114.55</u>		<u>1.8328\frac{1}{4}/\text{mil}</u>

Ht. all FUEL

15-13:	3.955 - .952 - .952 - .955 - .952 - .954	= 3.9533"
13-11:	4.015 - .015 - .015 - .017 - .018 - .017 - .017	= 4.0163 ✓
11-9:	3.952 - .951 - .951 - .948 - .952 - .954	= 3.9513
	wt avg	3.9737"

1X15B = 0.998
1X15A = 0.9995

(17-15) ~~2737 $\frac{3}{4}$ = 5.797 - .798 - .798 - .802 - .798 - .791~~ = ~~5.7958~~ 60093 (+27)

Corrected 17-15
15" 2000 = 0.998

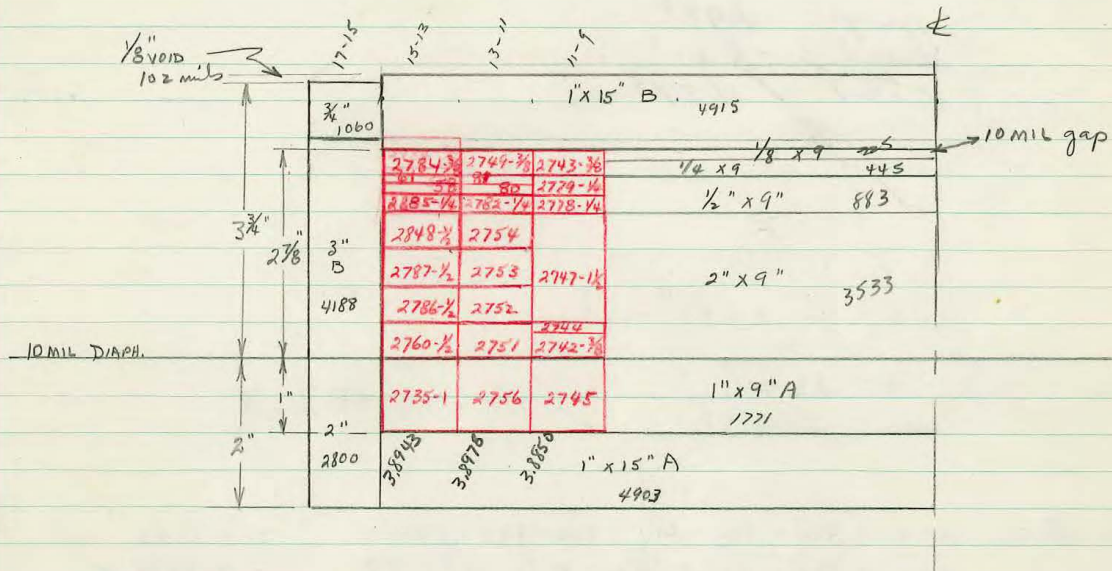
Even Fuel HT. = 4.0163"
SKY Hook Reactivity = +61.33%

React -	+0.67 $\frac{1}{4}$
all support	-12.42
15-9	<u>0</u>
	-11.75 $\frac{1}{4}$ = 3.9837
	0 = 3.9737 + .0064 = <u>3.9801"</u>

corrected flat fuel Ht = 3.9673"

15"-9" 1" GRAPHITE REFLECTOR + GRAPHITE CORE

Run 11c Pg 282



MASS OF TOP GRAPHITE = 15249 gm TOTAL = 24.723 Kg
 BOTTOM = 9474 gm

MASS OF TOP FUEL = 99970 gm TOTAL = 134.580 Kg
 BOTTOM = 34610 gm

AVG. O.D. ALL FUEL (wtd) = 14.99487" OD² = 224.84597
 AVG. I.D. ALL FUEL (wtd) = 9.00215" ID² = 81.03870
 AVG. Ht. ALL FUEL (wtd) =

FUEL VOLUME = 7205.20898 cm³
 FUEL ρ = 18.6781 gm/cc

graphite vol = 14620.87038 cm³
 ρ = 1.69093 gm/cc

Avg. Refl = 0.999"

15"-9" 1" Cinf + Core(C)

Dom. Ht $3\frac{7}{8}"$ Critical +21.0"

ring = 4.94"
diaph = -8.21"
stand = 11.57"

Lower .0069"

17-15 = $\approx .0245$ "/mil

15-9 = 1.64"/mil
Core $\approx .0343$ > TOT = 1.6743"/mil

Ht. all Fuel 15-13 = 3.894 - .895 - .897 - .894 - .892 - .894 = 3.8943"

13-11 = 3.898 - .898 - .898 - .898 - .898 - .897 = 3.8978 ✓

11-9 = 3.884 - .884 - .884 - .886 - .887 - .885 = 3.8850

Carbon
Ht Core Only 13.889 - .888 - .889 - .887 - .887 - .885 - .887 = 3.8874

1x15B = 0.998

1x15A = 0.9995

(17-15) 2+3+3/4 = 5.797 - .798 - .798 - .802 - .799 - .781 = 5.7958 (-97)

DRIFT TOP 17-15

15" DIA = 0.998

9" DIA =

Bottom Ht 17-15 = 3.894

EVEN FUEL HT. = 3.8928"

SKYHOOK REACTIVITY = +12.70% (NOT considered: 1/8" void 17-15 carbon)
10 mil gap over core).

0 React Fuel Ht = 3.8859" ✓

reactiv = +21.00

all support = -8.30

15-9 = 0

Core \uparrow 5.4 + 0.18

17-15 \uparrow 102 = +2.49

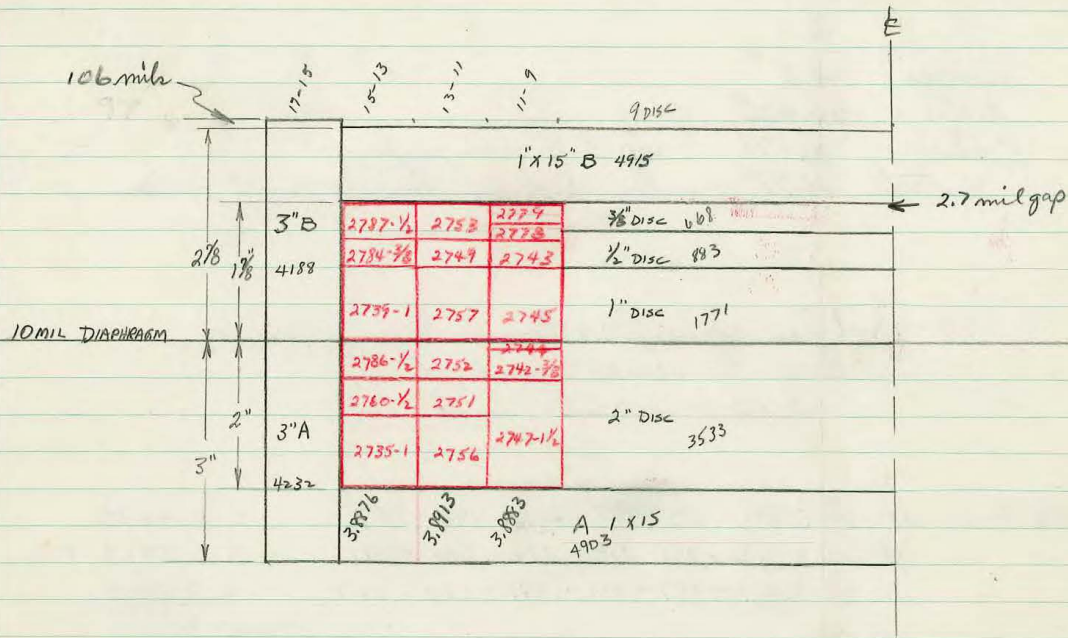
+14.79 = 3.8928"

0 = 3.8928 - .0088 = 3.8840"

15" 9"

1" GRAPHITE REFLECTOR + GRAPHITE 9" DIA. CORE

Bq 266



MASS OF TOP GRAPHITE = 12425 gm
BOTTOM = 12668 gm

TOTAL = 25.093 Kg

MASS OF TOP FUEL = 65088 gm
BOTTOM = 69345 gm

TOTAL = 134.433 Kg

AVG. OD ALL FUEL (WTD) = 14.99469"
AVG. ID. ALL FUEL (WTD) = 9.00186"
~~AVG. HT ALL FUEL (WTD)~~

OD² = 224.84072
ID² = 81.03348

FUEL VOLUME = 7198.07352 cm³
FUEL ρ = 18.67624 gm/cc

graphite vol. = 14823.98294 cm³
 ρ = 1.692729 gm/cc

Avg. Refl = 0.999"

15-9" 1" C. ref. + C Core

$$\text{Nom. Ht Critical} = 378'' = +21.73''$$

$$\begin{aligned} \text{rings} &= 4.8'' \\ \text{diaph} &= -14.42'' \\ \text{S. stand} &= 10.87'' \\ \text{S. stand} &= 16.87'' \end{aligned} \quad \left(\begin{array}{l} \text{cup } \approx 1/2'' \text{ from surface} \\ \text{when dropped down against carbon} \end{array} \right) 13.87$$

$$\begin{aligned} 15-9 \text{ fuel from curve} &= 1.64''/\text{mil} \\ \text{Core} &= 1.0439''/\text{mil} \\ 17-15 &= .0245''/\text{mil} \end{aligned} \quad > 1.6839''/\text{mil}$$

$$\begin{aligned} \text{Ht. all FUEL } 15-13 &= 3.885 - .885 - .888 - .891 - .890 - .887 &= 3.8876'' \\ 13-11 &= 3.892 - .891 - .890 - .892 - .892 - .891 &= 3.8913'' \\ 11-9 &= 3.887 - .887 - .886 - .891 - .892 - .887 &= 3.8883'' \end{aligned}$$

$$\begin{aligned} \text{Ht. of Core only} &= 3.888 - .888 - .889 - .889 - .891 - .887 &= 3.8886'' \\ 1 \times 15 \text{ B} &= 0.998 \\ 1 \times 15 \text{ A} &= 0.9995 \end{aligned}$$

$$(17-15) 3+3 = 6.035 - .035 - .035 - .037 - .034 - .035 = 6.0351$$

CALCULATED
17-15 = 5.000''
15-11 = 0.998''
1-15 = 0.9995''

$$\text{EVEN FUEL HT.} = 3.8890''$$

$$\text{SKY HOOK REACTIV.} = +14.48''$$

$$\text{O React Ht} = 3.8810'' \quad \checkmark$$

$$17-15 \downarrow 106.0 = -2.59''$$

$$\text{React.} = +21.73''$$

$$\text{all support} = -7.25$$

$$15-9 \rightarrow = 0$$

$$\text{Core (mil)} = 0$$

$$+14.89'' = 3.8890''$$

$$0 = 3.8890 - 0.070 = 3.8820''$$

15"-9" 2" GRAPHITE ~~≠~~ No CORE

3-96
~ Pg 96

16-17 12-15 15-13 13-11 11-9

7/0/2

1 1/2"	1 1/16"	1" x 15" B			4915
1334	960				
	1"	1" x 15" A			4903
	1456				
2 3/8"	1 1/2"	2766 3/4	2755	2767	
3863	2100	58	80	2778 1/4	
		2760 1/2	2753	2742 3/8	
		2734 1	2752 1/2	2776	
	2"		2751		
		2735 1	2756	2745	
4"	2770				
6513		3164 6	3200 1	3198	1" x 17" B 6268
					1" x 17" A 6261

10 MIL DIAPH.

MASS OF FUEL = 110.555 Kg
VOLUME = 5913.68103 cm³
ρ = 18.69478 gm/cc

MASS OF GRAPHITE = 41343 gm
VOLUME = 24249.85413 cm³
ρ = 1.70487 gm/cc

AVG. O.D. ALL FUEL (w't'D) = 14.99501" OD² = 224,85032
I.D. = 9.00188" ID² = 81.03384
19-17 OD Carbon = 18.99977" — 360.99126

Avg Refl = 2.000"

15-9 2" ref + NO core

Nom. Ht. Critical = $3\frac{3}{16}$ " reactivity = +24.89¢
recheck after all below = +24.26¢

Rings = +4.22¢

Diaphragm = -18.40¢

Support stand = +13.33¢

115

remove $\frac{1}{32}$ " fuel 15-9 = $\approx 62.59¢$

$\frac{1}{32}$ " 11-9 = 21.47¢

$\frac{1}{32}$ " 13-11 = 28.35¢

$\frac{1}{32}$ " 15-13 = 20.50¢

0.6870¢/mil ✓

0.9072 ✓

0.6560 ✓ total → 2.2502¢/mil

Ht of fuel = 15-13 = 3.192" - .193" - .191" - .196" - .192" - .192" = 3.1926"

13-11 = 3.200" - .200" - .199" - .200" - .200" - .202" = 3.2001"

11-9 = 3.192" - .192" - .191" - .192" - .192" - .192" = 3.1918"

wt avg = 3.1948"

Ht of 19-17 ring = 7.200" - .206" - .212" - .214" - .208" - .208" - .207" - .210" = 7.2081"

17-15 ring = 7.206" - .214" - .217" - .208" - .209" - .209" - .207" = 7.1100"

15 dia = Same as 91 = 4.0147"

Even Fuel Ht = 3.1948

SKY Hook React = +25.64

0 React Ht = 3.1834" ✓

React = +24.58¢

all support = +0.85

15-9 → = 0

+25.43¢ = 3.1948"

0 = 3.1948" - 0.113" = 3.1835"

15"-9"

2" GRAPHITE + GRAPHITE CORE

~Pg 100

7.525		19.17	17.15	15.13	13.11	11.09		
3/4	3/4						1x15 B	4915
1255	1060							
	7/8						1x15 A	4903
	1233							
2 3/8		58	80	96			1/4 x 9	445
3863	1 1/2	3214-32	3215	3216			3/8 x 9	668
	2100	2885-4	2782	2778-1			1/2 x 9"	883
		2760	2753	2742-2				10 MIL DIAPH
		2734-1	2752-1/2	2776				
	2"		2751				2" x 9"	3533
4"	2770	2735	2756	2745				
6513		3.693	3.690	3.683			1" x 17" B	6268
							1" x 17" A	6261

MASS OF FUEL = 109568 gm

VOLUME = 5863.68688 cm³ $\rho = 18.68585 \text{ gm/cc}$

MASS OF GRAPHITE = 46670 gm

VOLUME = 27424.84131 cm³ $\rho = 1.70174 \text{ gm/cc}$

Avg. O.D. ALL FUEL (W/T'D) = 14.99525"

OD² = 224.85752

I.D. = 9.00212"

ID² = 81.03816

19-17 OD Carbon = 18.99877"

— 360.95326

Avg. Refl = 2.000"

15-9 2" ref + core

Nom. Ht. critical = Fuel = $3\frac{5}{32}$ " C. Core = $3\frac{1}{8}$ " \rightarrow reactivity = +27.93%

Rings = +4.14¢
Diaphragm = -13.98¢
S. Stand = +13.18¢

remove $\frac{1}{32}$ " fuel	15-13 ring = +20.96¢	0.6707 ¢/mil
$\frac{1}{32}$ "	13-11 = +22.77¢	0.7286
$\frac{1}{32}$ "	11-9 = +22.54¢	0.7212
		2.1205 ¢/mil
	Core \rightarrow	.0183
		<u>2.1388</u>

Ht of fuel 15-13 = 3.168 - .168 - .169 - .171 - .171 - .169 = 3.1693"
13-11 = 3.168 - .169 - .169 - .170 - .170 - .168 = 3.1690"
11-9 = 3.164 - .165 - .164 - .164 - .164 - .165 = 3.1643"
wt avg = 3.1678"

Ht of C 19-17 = 7.155 - .155 - .155 - .163 - .163 - .167 - .165 - .158 = 7.1601"
17-15 = 7.156 - .160 - .158 - .154 - .153 - .160 - .154 = 7.1564"
15-9 = Same as Pg 91 = 4.0147"
Core = 3.133 - .133 - .136 - .133 - .131 - .133 - .131 = 3.1328"

Even Fuel Ht = 3.1678"
Sky Hook React = +24.59%

O React Ht = 3.1562" ✓

React. = +27.93¢
all support = -3.34
15-9 \rightarrow = 0
Core \uparrow 3.5 = +0.06
+24.65 = 3.1678"
O = 3.1678 - .0115 = 3.1563"

15"-9"

3" GRAPHITE REFLECTOR # No CORE

Pg = 123

	21-19	19-17	17-15	15-13	13-11	11-9	
86488							
1 1/8	13 1/16"	13 1/16"					1 x 15 C 4915
1947	1334	1170					
	1"	3/4"					1 x 15 B 4915
	1444	1060					
3"							1 x 15 A 4903
5325	2 3/8"	2 1/8"					
	3863	3776					VOID
							10 MIL GRAPH.
2"	1 1/2	1 1/2					VOID
3546	2438	2091					
1 1/2"							1 x 19 B 7838
2677							1 x 19 A 7828
							1 x 21 9666

MASS OF FUEL = 94316 gm

VOLUME = 5048.53923 cm³ $\rho = 18.68183 \text{ gm/cc}$

MASS OF GRAPHITE = 70993 gm

VOLUME = 41645.11420 cm³ $\rho = 1.70471 \text{ gm/cc}$

Avg. O.D. ALL FUEL (W.T'D) = 14.99515"

O.D. = 224.85452

I.D. = 9.00160"

I.D. = 81.02880

21-19 OD Carbon = 20.99948"

— 440.97816

Avg. Refl = 3.001"

15-9 3" ref #No Core

123

Dem. Ht. Critical = $2\frac{23}{32}$ "

reactivity = + 25.38⁺

Rings = + 4.14⁺
Diaphragm = - 19.62⁺
S. Stand = + 8.33⁺

$\frac{1}{32}$ " fuel 15-13 = 22.22⁺ 0.7110⁺/mil ✓
13-11 = 31.01⁺ 0.9923 ✓
11-9 = 23.96⁺ 0.7667 ✓
total 2.4700⁺/mil

Ht. of fuel 15-13 = 2.726 - .724 - .726 - .726 - .727 - .726 = 2.7258"
13-11 = 2.730 - .727 - .729 - .730 - .730 - .731 = 2.7295"
11-9 = 2.728 - .727 - .727 - .727 - .726 - .726 = 2.7268"
wt avg = 2.7261"

Ht of Carbon 21-19 = 8.670 - .668 - .685 - .670 - .678 - .680 - .672 = 8.6747"⁽⁻⁵⁰⁾
19-17 = 8.715 - .715 - .717 - .712 - .710 - .713 - .715 = 8.7138"
17-15 = 8.760 - .758 - .754 - .750 - .750 - .757 - .760 = 8.755"⁽⁺³⁰⁾
15-13 = 6.014 - .016 - .016 - .015 - .016 - .019 - .022 = 6.0169"
0-12

Corrected flat fuel Ht = 2.7158" ✓

React = + 25.38
all support = + 7.15
15-9 = 0
21-15 mil = 0
+ 32.53 = 2.7261"
0 = 2.7261 - .0131 = 2.7130"

15"-9" 3" GRAPHITE + GRAPHITE CORE

2/3/24

	21-19	19-17	17-15	15-13	13-11	11-9	
86488							£
1 1/8	13/16	1 1/8					1 x 15C 4915
1999	1334	1170					
	1	3/4					1 x 15B 4915
	1644	1060					
3"		2 1/16					1 x 15A 4903
5325	238	3776	28854	81-80	78		1/4 x 9 445
	3863		66 9/16	55	67		3/8 x 9 668
			84 3/8	49	43		9/16 x 9 998
			60 1/2	51	42 3/8		10 mil DIAPH.
2"	1 1/2	1 1/2	35-1	56	45		1 1/2 x 9 2675
3546	2138	2098					
			27008	2686P	26986		1 x 19B 7838
1 1/2							1 x 19A 7828
2677							1 x 21 9666

MASS OF FUEL = 93279 gm
 VOLUME = 4995.48490 cm³
 $\rho = 18.67266 \text{ gm/cc}$

MASS OF GRAPHITE = 75779 gm
 VOLUME = 44459.96809 cm³
 $\rho = 1.70443 \text{ gm/cc}$

AVG. O.D. ALL FUEL (WTD) = 14.99481" OD² = 224.84432
 ID = 9.00163" ID² = 81.02934
 21-19 OD Carbon = 20.99948" ——— 440.97816
 Avg Refl = 3.001"

15-9 3" up + Core

Norm. Ht. Critical = $2\frac{1}{16}"$

reactivity = $+7.11\%$

Rings = $+4.07\%$
Diaphragm = -17.10%
S. Stand = $+8.18\%$

Lower .004"

$\frac{1}{32}"$ fuel 15-13 = 31.08% - 0.9945% mil ✓
13-11 = 28.91% 0.9251 ✓
11-9 = 24.68% 0.7898 ✓
core $\frac{2.7094}{0.190}$
 $\frac{2.7274}{2.7094}$ wt Vol Avg = 2.7094% mil

Ht. of fuel 15-13 = $2.700 - .700 - .701 - .700 - .702 - .702$ = $2.7008"$
13-11 = $2.697 - .698 - .696 - .695 - .697 - .698$ = $2.6968"$
11-9 = $2.699 - .699 - .699 - .698 - .699 - .698$ = $2.6986"$
wt Vol Avg = 2.6988

Ht. of Carbon = 21-19 = Same as 123 = $8.6747"$ (-23)
19-17 = Same as 123 = $8.7138"$ (-10)
17-15 = Same as 123 = $8.7555"$ (+57)
15-9 = Same as 123 = $6.0168"$
Core = $2.700 - .698 - .699 - .702 - .698 - .697 - .700$ = $2.6991"$

Lower .0003

Corrected flat fuel height = $2.6947"$ ✓

React = $+7.11\%$
all support = $+4.85$
15-9 = 0
21-15 mil = 0
Core ↓ mil = 0
 $+11.96\% = 2.6988"$
 $0 = 2.6988 - .0043 = \underline{2.6945}"$

15"-9" - 3" Cmp. + VOID Core

FROM #46

BOORUM & PEASE "NGEAR"®

Top 1 1/8" U MASS = 58632 gm

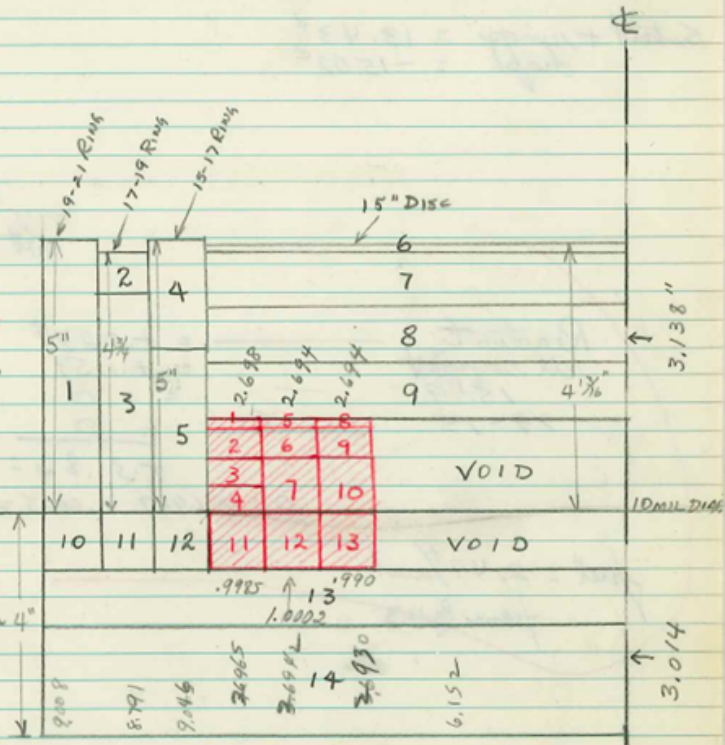
Top C MASS = 38807 gm

Total U 93.242

Total C 72.662

Bottom 1" U MASS = 34610 gm

Bottom C MASS = 33855 gm



Pos	Size	Mass
1	2758 (1/8")	1685
2	2766 (9/16")	7605
3	2787 (1/2")	6788
4	2848 (1/2")	6748
5	2780 (1/8")	1440
6	2755 (9/16")	6514
7	2757 (1")	11575
8	2744 (1/8")	1223
9	2767 (9/16")	5410
10	2776 (1")	9644
11	2735 (1")	13409
12	2756 (1")	11567
13	2745 (1")	9634

Pos	Size	Mass
1	1" x 5" (19-21)	8827
2	1" x 3/4" (17-19)	1255
3	1" x 4" (17-19)	6513
4	1" x 2" (15-17)	2800
5	1" x 3" (15-17) B	4188
6	1/8" x 15" Disc	625
7	1" x 15" Disc B	4915
8	1" x 15" Disc D	4781
9	1" x 15" Disc A	4903
10	1" x 1" (19-21)	1828
11	1" x 1" (17-19)	1644
12	1" x 1" (15-17)	1454
13	1" x 21" Disc	9666
14	2" x 21" Disc	19263

Av. O.D. FUEL (wTD) = 14.995094"

Av. I.D. FUEL (wTD) = 9.00144"

Fuel vol = 4989.79152 cm³

ρ = 18.686552 gm/cc

graphite vol = 42676.06307 cm³

ρ = 1.70264 gm/cc

OD² = 224.85284

ID² = 81.02592

Avg Refl = 3.005"

15'-9" 3" Cref. wd Core

Dem. Ht. Critical: $2\frac{1}{16}" = +2.27\frac{1}{4}$

Stand + rings = $13.43\frac{1}{4}$
dia ph = $-15.02\frac{1}{4}$

wt ht = $3.6947"$

Reactivity
all support = $+2.27\frac{1}{4}$
15'-9" = $+1.59$
19-15 m'l = 0
 $+3.86 = 3.6947"$

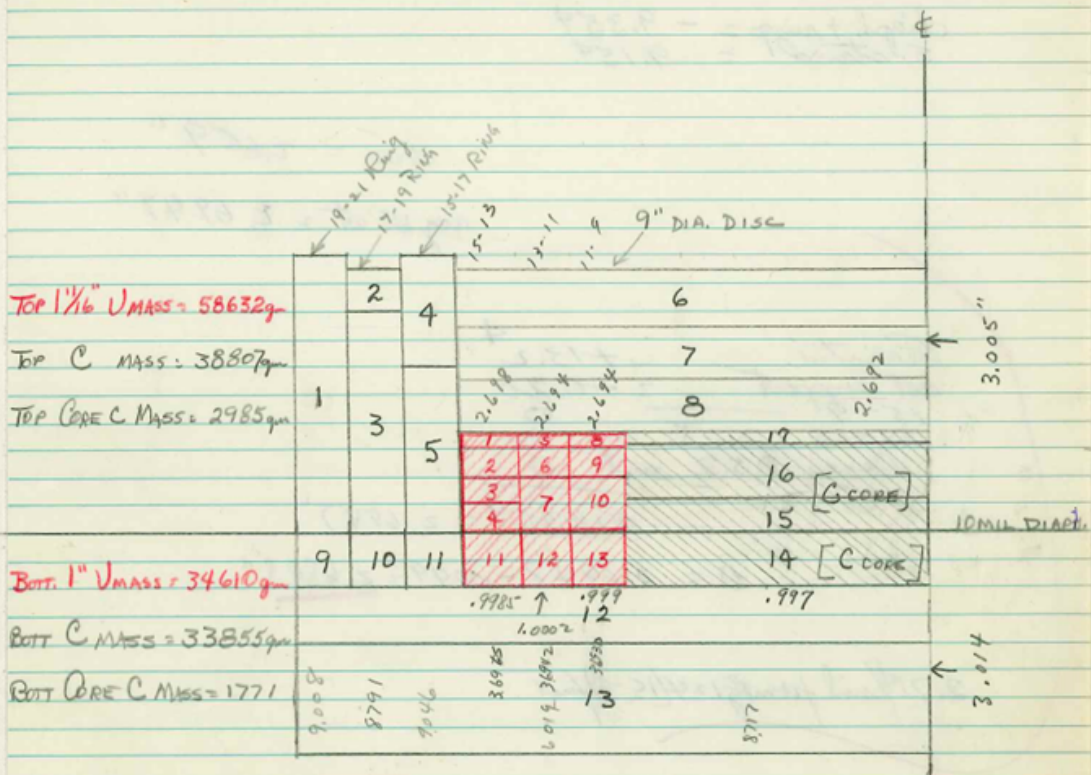
$0 = 3.6947 - .0015 = \underline{3.6932}"$ but has
extra $\frac{1}{8}" \times 15"$ Carbon
on top.

fuel = $2.47\frac{1}{4}$ m'l
from Pg 123

EVEN FUEL HT. = $3.6947"$ ✓
SKY HOOK REACTIVITY: $+3.86\frac{1}{4}$

(Carbon 21-15 ring ^{ht.} error not considered)
also contains $\frac{1}{8}" \times 15"$ dia extra carbon ^{net} ".

15"-9" 3" C C center. ≈ 46



PS	W	MASS
1	2758 (1/8)	1685
2	2766 (1/8)	7605
3	2787 (1/8)	6788
4	2848 (1/8)	6748
5	2780 (1/8)	1440
6	2755 (1/8)	6514
7	2757 (1")	11575
8	2744 (1/8)	1223
9	2767 (1/8)	5410
10	2776 (1")	9644
11	2735 (1")	13409
12	2756 (1")	11567
13	2745 (1")	9634

PS	SIZE	MASS
1	1" x 5" (19-21)	8827
2	1" x 3/4" (17-19)	1255
3	1" x 4" (17-19)	6513
4	1" x 2" (15-17)	2800
5	1" x 3" (15-17) D	4188
6	1" x 15" Disc B	4915
7	1" x 15" Disc D	4781
8	1" x 15" Disc A	4803
9	1" x 1" (19-21)	1828
10	1" x 1" (17-19)	1644
11	1" x 1" (15-17)	1454
12	1" x 21" Disc	9666
13	2" x 21" Disc	19263

AVG. OD FUEL (W.T.D) = 14.995094"

AVG. I.D. FUEL (W.T.D) = 9.00144"

FUEL VOLUME = 4989.79152 cm³

$\rho = 18.686552 \text{ gm/cc}$

GRAPHITE VOL = 45104.95629 cm³

$\rho = 1.71639 \text{ gm/cc}$

14	1" x 9" Disc A	1771
15	1/8" x 9" Disc	998
16	1" x 9" Disc B	1762
17	1/8" x 9" Disc	225

Avg Refl = 3.006"

15"-9" 3" C ref. + C Core

$$\text{Nom. Ht Critical} = 2\frac{1}{16} = +13.24$$

$$\begin{aligned} \text{diag. + ring} &= -9.354 \\ \text{5. stand} &= 9.154 \end{aligned}$$

$$\text{core} = 2.659''$$

$$\text{avg Ht wt} = 2.6947''$$

$$\begin{aligned} \text{Reactiv.} &= +13.24 \\ \text{all support} &= +0.20 \\ \hline 15-9 &= 0 \\ 21-15 \text{ mil} &= 0 \\ \text{Core } \uparrow 5.7 \text{ mil} &= 0 \end{aligned}$$

$$+13.404 = 2.6947''$$

$$0 = 2.6947 - .0049 = \underline{2.6898''}$$

$$2.714 \text{ mil from } 124(15-9) \text{ fuel}$$

$$\begin{aligned} \text{EVEN FUEL HT.} &= 3.6947'' \\ \text{SKY Hook React.} &= +13.404 \end{aligned}$$

(Carbon 21-15 ring Ht error not considered)

15-9 5"ref & No Core

Nom. Ht. Critical = $2\frac{1}{8}"$ reactivity = -13.39%

Rings: + 5.25¢
Diaphragm: + 0.49¢
S. Stand: + 6.07¢

Raise 0.0086"

$\frac{1}{32}"$ fuel 15-13 = 29.34¢ 0.9389¢/mil ✓
13-11 = 31.96¢ 1.0227 ✓
11-9 = 28.41¢ 0.9091 ✓
 $\frac{1}{8}"$ graphite 15" dia top = -21.13¢ 2.8707 ✓
wt vol Avg = 2.8707¢/mil

Ht. of fuel 15-13 = 2.136 - .138 - .137 - .136 - .139 - .137 = 2.1371"
13-11 = 2.143 - .144 - .145 - .144 - .144 - .143 = 2.1438"
11-9 = 2.130 - .130 - .130 - .129 - .129 - .130 = 2.1296"
wt vol Avg = 2.1372"

Ht. of Carbon 25-21: 7.0000 + 5.0092 = 12.0092"
21-19 = [7.128 - .133 - .123 - .119 - .119 - .121 - .123 - .130] + 5.0007 = 12.1252" (-32)
19-17 = [7.125 - .125 - .127 - .127 - .130 - .126 - .125 - .125] + 5.0007 = 12.1269" (-36)
17-15 = [7.132 - .134 - .129 - .137 - .132 - .133 - .133] + 5.0007 = 12.1213" (-16)
15 dia = 10.0147"
Raise .0068"

Corrected flat fuel height = 2.1526" ✓

Reactivity = -13.39%
all support = -10.83
15-9 = $\frac{0}{-24.22\%} = 2.1372"$
① = $2.1372 + .0084 = \underline{2.1456}"$

NOTE: FUEL SAME AS No Core run
GRAPHITE SAME AS No Core run but + core.

15"-9" 5" REFLECTOR + CORE (GRAPHITE)

B_g 171

5765.11

7"	1828	1"	1"	3/4"	1/2 x 15	2467
		1 1/8"	1 1/8"	1/16"	1 1/2 x 15	7485
		1997	2 1/8"	960	1 x 15 C	4915
	28700	5"	3440	2 1/16"	1 x 15 B	4915
			8827	3976	1 x 15 A	4903
			4"			
	4232	6513	3A	2885	1/4 x 9	445
				58	3/8 x 9	668
				85-3/8	1/2 x 9	883
				84-3/8	1 x 9	1771
3"	12350			86-1/2		
				52		
				45-1		
				60-1/2		
				51		
					1 x 21	9666
					2 x 21	19263
					2 x 25	27650

MASS OF FUEL = 73831

VOLUME: 3954.29916 cm³

ρ = 18.66163 gm/cc

MASS OF GRAPHITE = 160358 gm

VOLUME: 93351.21881 cm³

ρ = 1.71779 gm/cc

Avg Refl = 4.996"

AVG. O.D. ALL FUEL (w'tb) = 14.99529"

I.D. = 9.00179"

25-21 OD Carbon = 24.99750"

OD² = 224.85872

ID² = 81.03222

— 624.87500

15-9 5" ref + Core

Norm. HT. Critical = $2\frac{1}{8}"$

reactivity = $+17.07\%$

Rings = $+5.29\%$
 Diaphragm = 0.0%
 S. Stand = $+4.97\%$

Lower $0.0079"$

$\frac{1}{32}"$ fuel 15-13 = 26.93%	0.8617 ✓	
13-11 = 40.74%	1.3036 ✓	
11-9 = 39.69%	1.2700	wt Vol Avg = 3.435% / mil
	<u>3.4353</u>	
	+002	
core	<u>3.4373</u>	

Wt. of fuel 15-13 = Same as No Core	= $2.1371"$
13-11 = Same	= $2.1438"$
11-9 = Same	= $2.1296"$
	wt vol Avg = $2.13725"$

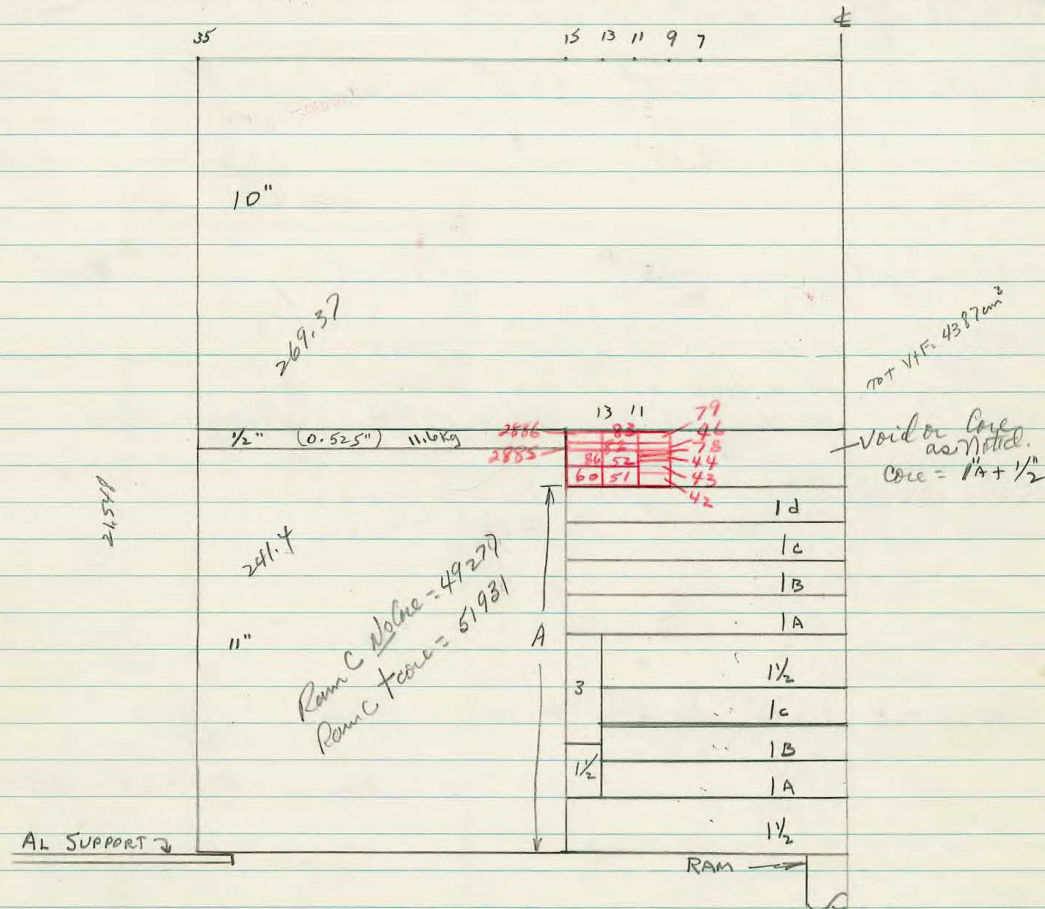
Wt of Carbon 25-21 = $7.0000 + 5.0092$	(-103)	= $12.0092"$ ⁽⁻¹²⁸⁾
21-19 = Same	(+10)	= $12.1252"$
19-17 = Same — 168	(+14)	= $12.1269"$
17-15 = Same as 19-168	(+4)	= $12.1213"$
15 dia = $10.0147"$		= $10.0147"$
Core = $2.130 - .131 - .130 - .130 - .130 - .130 - .133 - .128 = 2.1302"$		
		Raise $0.0003"$

corrected flat fuel height = $2.1296"$ ✓

Reactivity	= $+17.07\%$
all support	= -10.26
15-9	= 0
Core ↑ 7.0	= $+0.01$
	<u>+6.82%</u>
	= 2.1372
	<u>0 = $2.1372 - .0019 = 2.1353"$</u>

15-9 10" GRAPHITE REFLECTOR WITH OR WITHOUT CORE AS NOTED

Pg 62



MASS OF FUEL = 52.233 gm
 VOL = 2796.9770 cm³
 $\rho = 18.6748 \text{ gm/cc}$

MASS RAM GRAPHITE = 49277 gm
 RAM C + CORE = 51931 gm

Avg Refl = 9.997"

Avg. wid OD = 14.99548"
 (OD)² = 224.86442
 ID = 9.00227"
 (ID)² = 81.04086

Mass of C = 571640 Kg
 C Vol = 335346 cm³
 $\rho = 1.704 \text{ gm/cc}$

Core - No Core
 Same except Carbon

+Core

574.301 Kg
 336986 cm³
 1.704

15-9 10" C ref ~~at~~ No Core

or Core as NOTED

clean Critical Nom. 1/4" - 1 1/2"

reactivity = +20.11% No Core

with Core = +34.97%

1/32" Value 15-13 = 35.28%
13-11 = 61.08%
11-9 = 56.58%

33.3% Use 34.3% $\times 1.09$ ~~factor~~
1.954 ✓
1.810 ✓
total 4.861

41.92% $\times 1.341$
56.74% $\times 1.815$
51.40% $\times 1.644$
9.800

All Support Value = 7.25%

11.43%

Ht. of fuel 15-13 = 1.507 - .508 - .506 - .507
13-11 = 1.512 - .512 - .512 - .512
11-9 = 1.516 - .515 - .516 - .516
.515 - .516 - .516 1.516

1.5071
1.5120
1.5156

Same
int avg = 1.5110"

15" dia ^{carbon} 10" dia on top of 10" ref = +9.42% (Page 61)
15" dia (3/8") on top = +18.16%

A Same as (15-7) Pg 52 = 10.0162

Same -

= 10.0162

Core = 1.497 - .499 - .499 - .499 = 1.4985

1.4985

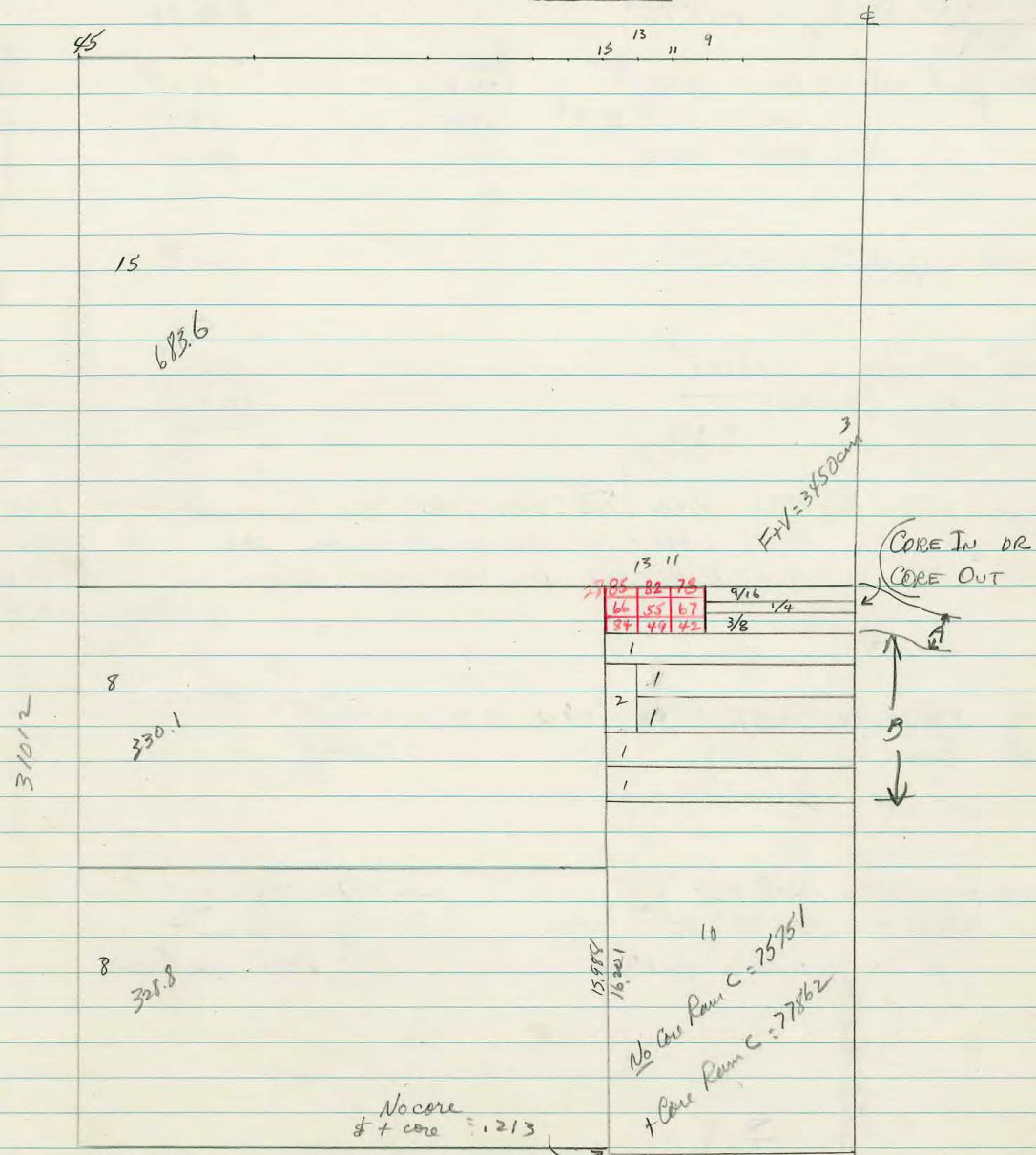
1.511" $\times 1.09$
1.509"

1.511" $\times 1.09$
1.506"

15"-9" \$ 15" GRAPHITE REFLECTOR

No Core
\$
+ Core

Eq 4-179



fuel mass = 41285 gm

$V_f = 2205.7297 \text{ cm}^3$

$\rho = 18.7171 \text{ gm/cc}$

OD = 14.99571" (2) = 224.87131

ID = 9.00136" (2) = 81.02448

$\pi \cdot 14.998''$

15-9 & 15" C. ref

No Core

Dom At critical = $1\frac{3}{16}$ "
reactivity = +11.70%

$\frac{1}{32}$ " fuel value: 15-13 = 48.00%
13-11 = 56% $\pm 3\%$
11-9 = 41.3%

$\frac{1}{16}$ "
1.5360
1.7920
1.3216
4.6

all supports = +2.57%

$\frac{1}{2}$ " x 25" dia. C. = 12.67%

1" x 17" Carbon = —

1" x 15" = 13.36

+ Core

$1\frac{3}{16}$ "

+16.36

48.71%

54.1%

40.66%

$\frac{1}{16}$ "
1.5587

1.7312

1.3011

SAME

14.27%

14.4%

fuel measured: 15-13 = 1.192, 192, 192, 192, 192 Same 1.1920

13-11 = 1.191, 191, 192, 191, 192, 192, 192 1.1915

11-9 = 1.190, 191, 191, 191, 190, 190 1.1905

wt avg = 1.1914

A: 1.193, 192, 192, 191, 190, 193 = 1.1918"

B: Same as 4-189 = 5.0091

Mass of C = 1418.251 Kg

Vol C = 804808 cm³

$\rho = 1.762$ gm/cc

= 1420.362 Kg

= 806053 cm³

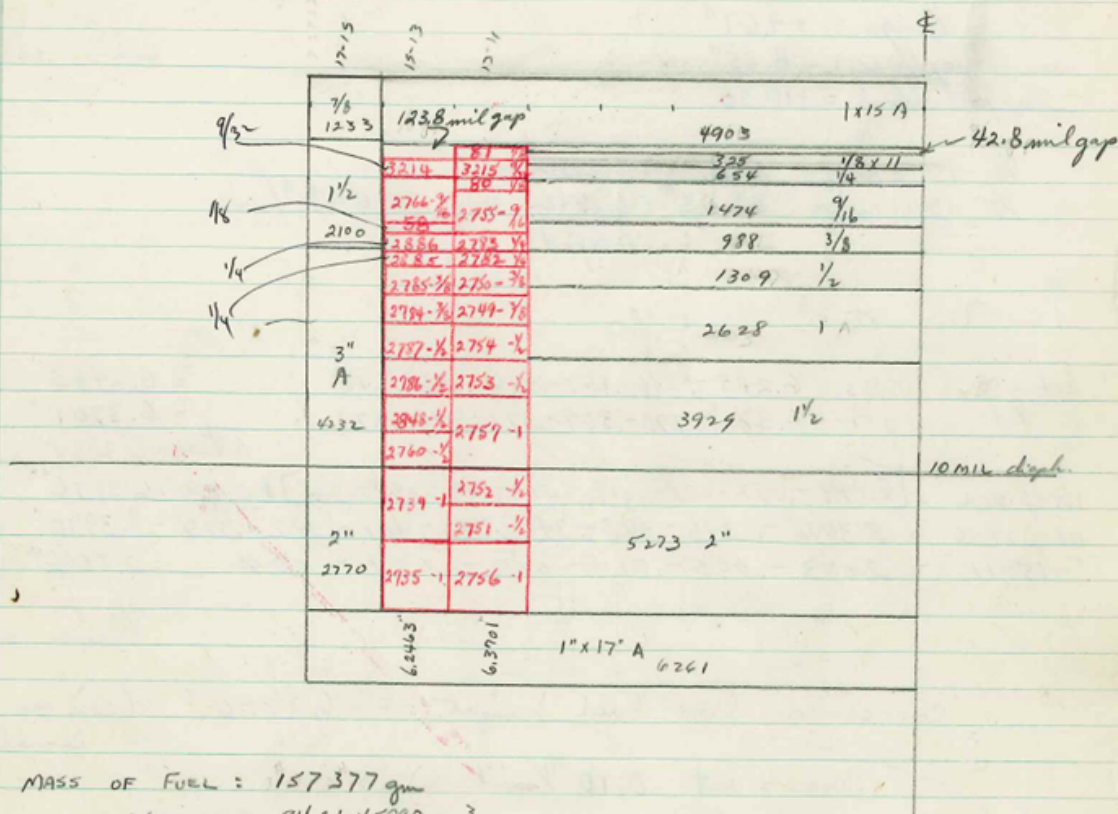
= 1.762 gm/cc

$\rho = 1.762$
1.1918
1.1914

$\rho = 1.762$
1.1918
1.1914

15"-11" 1" GRAPHITE REFLECTOR + G. CORE

Fig 89



MASS OF FUEL: 157.377 gm
 VOLUME: 8421.45990 cm³
 ρ : 18.68761 gm/cc

MASS OF GRAPHITE: 38079 gm ✓
 VOLUME: 22706.6314 cm³ ✓
 ρ : 1.6770 gm/cc ✓

AVG. O.D. ALL FUEL (w.t.d) = 14.99545" OD² = 224.86352
 I.D. = 11.00272" ID² = 121.05984
 17-15 OD avg Carbon = 16.99941" (r) = 288.97994

Avg Refl = 0.996"

15-11

1" ref. + Core

Nom. Ht. Critical $\rightarrow 13 \times 11 = 6 \frac{1}{32}$; $15-13 = 6 \frac{1}{32}$; C. CORE = $6 \frac{5}{16}$ " = $+7.22^{\circ}$

Rings = $+9.67^{\circ}$
 Diaphragm = -8.35°
 Support Stand = $+10.38^{\circ}$

Lower .0088"

$\frac{1}{8}$ " 15-13 ring = 30.4° $\checkmark 0.2432^{\circ}/\text{mil}$
 $\frac{1}{8}$ " 13-11 ring = 33.03° $\checkmark 0.2642^{\circ}$ Avg $0.507^{\circ}/\text{mil}$
 $\frac{0.5074}{10}$

Ht of fuel 15-13 = $6.245 - .246 - .247 - .246 - .248$ = 6.2463 "
 13-11 = $6.370 - .370 - .369 - .371 - .370 - .371$ = 6.3701 "

Avg = 6.3034 "

Ht of core = $[6.098 - .097 - .098 - .098 - .097 - .098 - .097 - .098] + 0.250 = 6.3476$ "
 Ht of 17-15 = $8.396 - .396 - .398 - .398 - .396 - .401 - .397 - .394 = 8.3970$ " (+94)
 15-11 = $2.003 - .005 - .010 - .009 - .009 - .004 = 2.0066$ "

1 XISA

Lower .004"

Corrected flat fuel height = 6.2906 " (core gap not considered)

Core = est. $0.10^{\circ}/\text{mil}$ Cell support = -11.70° 13-11 $\rightarrow 0$ 15-13 up 123.8 mils = $+30.10^{\circ}$ Core up 22.5 mils = $+2.2^{\circ}$

Support =

 6.3701 " = $+20.60^{\circ}$ $0^{\circ} \rightarrow 6.3701 - .0339 = 6.3362$ " all considered

31 233.1942
 9526.5628

2

15"-11"

2" GRAPHITE REFLECTOR & NO CORE

Q91

		19-17	17-15	15-13	13-11	ø
		23456				
3/4	1255	13/16	1170	1x15 B		4915
1/16	1111			1x15A		4905
1 1/2	2100					
2452				276-7/16	2755	
				2785-7/16	2750	
				2714-7/16	2749	
	3			2848-7/16	2754	
278	4232			2787-7/16	2753	
3863				278-1/2	2759-1	
				2760-1/2		
				2739-1	2752-1/2	
					2751-1/2	
	2"			2735-1	2756-1	
4"	2770					
6513				5.3296"	5.3296"	1x17 B 6268
						1"x17" A 6261

10 MIL DIAPH.

MASS OF FUEL = 133146 gm
 VOLUME = 7119.05134 cm³
 P = 18.70277 gm/cc

MASS OF GRAPHITE = 47813 gm
 VOLUME = 27982.70022 cm³
 P = 1.70866 gm/cc

AVG. O.D. ALL FUEL (w/IT'D) = 14.99512 OD² = 224,85362
 I.D. = 11.00281 ID² = 121.06182
 19-17 OD Carbon = 18.99724 = 360,89512

Aug. Refl = 1.997"

15-11

2" ref # no core

91

Nom. Ht. CRITICAL = $5\frac{5}{16}$ " $\rightarrow 19.68\frac{1}{2}$

Rings = $+8.01\frac{1}{2}$
 Diaphragm = $-13.72\frac{1}{2}$
 Support Stand = $9.88\frac{1}{2}$

remove $\frac{1}{16}$ " 13-11 ring = $33.92\frac{1}{2}$ removed from "clean" i.e. $\checkmark 0.5427\frac{1}{2}$ mil
 remove $\frac{1}{32}$ " from 15-11 = $31.57\frac{1}{2}$ $\checkmark 0.4675\frac{1}{2}$ mil 15-13
 \uparrow 1.0102" $\checkmark 1.0102$
 $X_{16} = 29.22$

Ht of fuel 15-13 : $5.330 - .328 - .328 - .331 - .331 - .330 = 5.3296$ "
 13-11 : $5.330 - .328 - .329 - .330 - .327 - .329 = 5.3288$ "
 avg = 5.3292 "

Ht of 19-17 ring = $9.362 - .362 - .352 - .358 - .358 - .362 - .362 = 9.3594$ " (+30)
 17-15 ring = $9.327 - .327 - .331 - .337 - .335 - .335 - .331 - .327 = 9.3312$ " -
 15 dia = $4.016 - .014 - .016 - .013 - .014 - .014 - .016 = 4.01471$ "

Even Fuel Ht = 5.3292 "Sky Hook React = $+15.51\frac{1}{2}$

0 React Fuel Ht = 5.3149 " \checkmark (ignoring reflector diff) nil?

Pg 91

MASS OF FUEL = 121412 gm
VOLUME = 6494.73868 cm³
 $\rho = 18.6939 \text{ gm/cc}$

MASS OF GRAPHITE = 58820 gm
VOLUME = 34545.41657 cm³
 $\rho = 1.70268 \text{ gm/cc}$

Avs. O.D. ALL FUEL (w/ty) = 14.99537" OD² = 224.86112
I.D. = 11.00277" ID² = 121.06094
19-17 OD Carbon = 18.99681" (2) = 360.87879

Aug. Refl = 1.997"

15-11 2" ref + C Core

Dem. Wt. Critical = $4\frac{27}{32}$ " - 11.72⁴

Rings = +7.47⁴
 Diaphragm = -12.83⁴
 Support Stand = +9.60⁴

$\frac{1}{32}$ " fuel from 15-13 ring = 15.70⁴ 0.502⁴/mil (p. 94)

Wt of fuel 15-13 = 4.856 - .858 - .861 - .861 - .864 - .861 = 4.8601"
 13-11 = 4.864 - .861 - .862 - .864 - .864 - .864 = 4.8631"
 wt avg = 4.8614"

Wt of 19-17 ring = 8.900 - .902 - .901 - .898 - .895 - .896 - 900 = 8.8988"
 17-15 ring = 8.907 - .905 - .906 - .911 - .905 - .906 - .905 - 908 = 8.9066"
 15-11 ring = same as 19-17
 Core only = $[4.592 - .590 - .590 - .582 - .584 - .590 - .590] + 0.250 = 4.8382$ "

Even Fuel 14+ = 4.8614"
 Sky Hook React = - 15.96⁴

Core $\frac{1}{4}$ mil = + 0.1076 (Core vs No Core relationship)
 1.2⁴/mil of 15-11 fuel from curve = 15.3 mil

is "O reactivity = 4.8614 + 15.3 = 4.8747"

So all
 4.8614" fuel = -11.72⁴
 249 mil Core = + 2.67⁴
 $\therefore 4.8614 \rightarrow -13.35^4$

1.2⁴ (15-11 fuel) + (0.1076 core) = 1.3076 mil RT
 $\therefore 7.3$ miles to be added

flat "O reactivity $\rightarrow 4.8614 + 0.0102 = 4.8716$ "

15"-11"

3" GRAPHITE REFLECTOR & NO CORE

= 129

21-19	19-17	17-15	15-13	13-11	
10.2846					
3/4 1364	3/4 1255	1 1/16 1170			1 x 15 C 4915
5	1 1644	2 2770			1 x 15 B 4915
	4	3A			1 x 15 A 4903
			66-9/16 55		
			2885-1/4 82		
			87-1/2 53		
			86-1/2 52		
8827	6513	4232	39-1 57		
			60-1/2 51		
2	1 1/2 2438	1 1/2 2098	35-1 56		
3546			43323	43306	1 x 19 B 7838
1 1/2					1 x 19 A 7828
2677					1 x 21 9666

MASS OF FUEL = 108123 gm

VOLUME = 5786.21059 cm³ $\rho = 18.68632 \text{ gm/cc}$

MASS OF GRAPHITE = 78599 gm

VOLUME = 46073.92605 cm³ $\rho = 1.70593 \text{ gm/cc}$

Avg. O.D. ALL FUEL (w/rod) = 14.99498

I.D. = 11.00279

21-19 OD Carbon = 20.99926

OD = 224.84942

ID = 121.06138

— 440.96892

Avg Refl = 2.997"

15-11 3" w/ & No Core

Nom. Ht. Critical: $4\frac{5}{16}"$ reactivity = $+27.22\%$

Rings = $+7.38\%$
Diaphragms = -15.62%
Support Stand = $+6.85\%$

Lower .0220"

$\frac{1}{8}"$ fuel 15-13 = 22.79% ✓ $0.7292\%/mil$
13-11 = 23.64% ✓ 0.7564% wt vol Avg = $1.484\%/mil$
 $\frac{1.4856}{1.4856}$

Ht. of fuel 15-13 = $4.330 - .329 - .332 - .333 - .335 - .335 = 4.3313"$
13-11 = $4.329 - .329 - .334 - .329 - .334 - .329 = 4.3306"$
wt vol Avg = $4.3315"$

Ht. of Carbon: 21-19 = $10.288 - .298 - .294 - .296 - .298 - .290 - .288 = 10.2931"$
19-17 = $10.300 - .303 - .298 - .298 - .292 - .285 - .290 - .297 = 10.2953"$
17-15 = $10.330 - .333 - .328 - .325 - .324 - .326 - .331 = 10.3281"$
15 dia = same as 12 5 = $6.0168"$
Raise .0004"

Corrected flat fuel height = $4.3099"$

all supports $+1.39\%$
reactivity -27.22%
15-13 - 0 -
13-11 $\times 0.7 mils = 0.5\%$

$4.3315" = +29.11\%$

"O" react: $4.3315 - .0195 = \underline{4.3120}"$

15"-11"

3" GRAPHITE REFLECTOR + GRAPHITE CORE

Fig 131

	21-19	19-17	17-15	15-13	13-11		
	3/4"	13/16"	3/4"				
	1364	1334	1060			1 x 15 C	4915
		3/4"	13/16"			1 x 15 B	4915
		1255	1170			1 x 15 A	4903
			1"				
			1456				
5"	4"	3"	3"				
				66 7/16	55	7/16 x 11	1474
				57 1/2	53		
				86 1/2	52	2 x 11	5273
				35-1	57		
				60 1/2	51		
				35-1	56	1 1/2 x 11	3929
2	1 1/2	1 1/2					
	2438	2098					
	3546			42753	40753	1 x 19 B	7828
						1 x 19 A	7928
1 1/2						1 x 21	9666
2677							

10 MIL DIAPH.

4 mil gap

MASS OF FUEL = 101794 gm

VOLUME = 5442.85522 cm³ $\rho = 18.70231 \text{ gm/cc}$

MASS OF GRAPHITE = 88711 gm

VOLUME = 52057.55651 cm³ $\rho = 1.704094 \text{ gm/cc}$

Avg. O.D. ALL FUEL (w/ID) = 14.99496"

I.D. = 11.00277"

21-19 O.D. Carbon = 20.99926"

OD² = 224.84882ID² = 121.06094

440.96892

Avg Refl = 2.997"

15-11 3" ref. + Core

nom. ht. Critical = $4\frac{1}{16}"$

reactivity: $+17.96\%$

Rings: $+6.61\%$
diaphragm: -12.7%
S. Stand = 5.61%

Lower .0119"

(77 1/4 miles)

3/4" reflector 21-19 ring removed = 5.96% or $.0077\%$ /mil

1/32" fuel 15-13 = 22.27% ✓ 0.7126% /mil
13-11 = 26.71% ✓ 0.8547% wt. vol Avg = 1.556% /mil
 $\frac{1.8673}{0.959}$
+ Core = 1.6632

Nt. of fuel 15-13 = $4.075, .074, .075, .074, .076, .078$ = $4.0753"$
13-11 = $4.075, .074, .072, .073, .074, .075$ = $4.0738"$
wt vol Avg = $4.0744"$

Nt. of carbon: 21-19: Same as Pg 129 = $10.2931"$ (+218)
19-17 = $10.120, .123, .120, .116, .109, .112, .112, .120$ = $10.1165"$ (+40)
17-15 = $10.095, .093, .093, .092, .092, .089, .090$ = $10.0920"$ (+2)
15-11 = Same as 123 = $6.0168"$ (-58)
Core = $4.076, .072, .072, .071, .071, .070, .068, .074$ = $4.0717"$

Raise .0010"

Corrected flat fuel height = $4.0633"$ ✓

React $+17.96$
all Support $+0.48\%$
15-13 = 0 = 0
13-11 up 1.5 $\rightarrow +1.28\%$
Core = $+0.95\%$ /mil
 $\frac{0}{+19.72}$

$+19.72\%$ = $4.0753"$

0 = $4.0753 - .0118 = \underline{4.0635}"$

15-11 5"ref 4 No Core

New. Ht. Critical = $3\frac{1}{4}"$

reactivity = $+32.81\%$

Rings = $+6.56\%$
Diaphragm = nil
S. Stand = $+4.40\%$

Lower 9.0278"

$\frac{1}{32}"$ FUEL 15-13 = 25.56% ✓ $0.8179\%/mil$
 $\frac{1}{32}"$ FUEL 13-11 = 23.61% ✓ 0.7555
1.5734

wt vol Avg = $1.573\%/mil$

Ht of fuel 15-13 = $3.259 - .260 - .260 - .264 - .262 - .263 = 3.2617"$
13-11 = $3.264 - .263 - .263 - .263 - .264 - .264 = 3.2635"$
wt vol Avg = $3.2625"$

Ht. of carbon = $25-21 = [8.200 - .196 - .190 - .195 - .184 - .180 - .184] + 5.0092 = 13.1990"$ (+63)
 $21-19 = [8.295 - .299 - .301 - .309 - .307 - .305 - .303] + 5.0007 = 13.3034"$ (+10)
 $19-17 = [8.196 - .196 - .198 - .199 - .196 - .196 - .194] + 5.0007 = 13.1971"$ (-10)
 $17-15 = [8.275 - .273 - .271 - .271 - .278 - .277 - .277] + 5.0007 = 13.2752"$ (+63)
15 dia: 10.0147
 $= 10.0147"$
Revised .0011"

Corrected flat fuel height = $3.2358"$

All Support -10.96%
Reactivity $+32.81\%$
15-13 up 1.8 mils = $+1.47\%$
13-11 0
 $+23.32\%$

$3.2635" = +23.32\%$
"O" react = $3.2635 - .0148 = \underline{3.2487}"$

4 Pg 175

1000 D1145

624.88600

15-11 5" ref + Core

New. HT. Critical = $3\frac{1}{8}$ "

reactivity = +15.14¢

Rings + Support Stand = +11.31¢

diaphragm = -1.52¢

→ recheck @ slower period: +0.14¢

avg = -0.6¢

Lower 0.0023"

$\frac{1}{32}$ " fuel 15-13 = 32.64¢

✓ 1.0444¢/mil

13-11 = 39.49¢

✓ 1.263¢

wt val Avg = 2.308¢/mil

2.308¢

+ core = 5387¢

Ht. of fuel 15-13 = 3.140 - .139 - .1375 - .141 - .138 - .138

= 3.1389"

13-11 = 3.139 - .142 - .143 - .142 - .142 - .141

= 3.1415"

wt val Avg = 3.1401"

Ht of Carbon 25-21: Same as pg. 174

13.1990" (+81)

21-19: [8.125 - .135 - .127 - .127 - .131 - .124 - .122] + 5.0007 = 13.1279" (+10)

19-17: [8.164 - .169 - .175 - .172 - .169 - .166 - .162] + 5.0007 = 13.1688" (+50)

17-15: [8.150 - .153 - .153 - .162 - .158 - .158 - .154] + 5.0007 = 13.1561" (+35)

15 diaz 10.0147 = 10.0147"

Core 3.137 - .142 - .142 - .144 - .141 - .141 = 3.1411"

Lower .0007"

Corrected flat fuel height = 3.1371" ✓

Reactivity: +15.14¢

All Support = -11.31¢

15-13 up 2.6 mil = +2.71¢

13-11 0

Core = 7.0796¢/mil

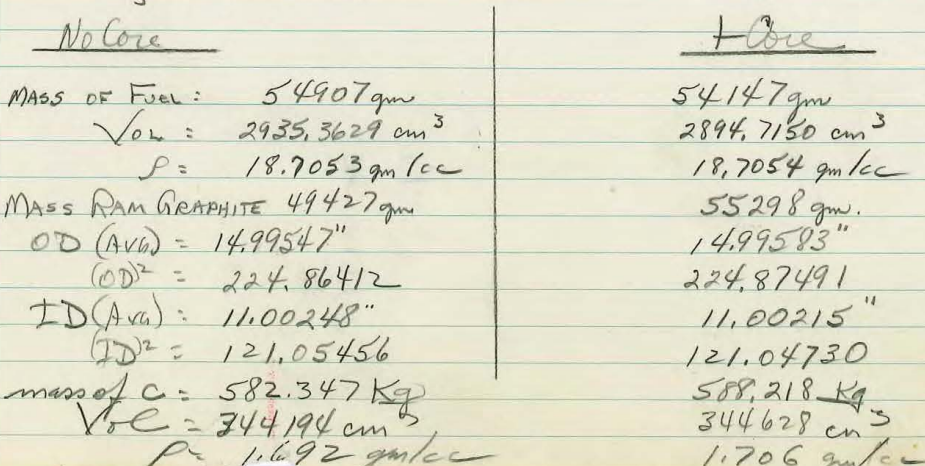
0

+6.54¢

+6.54¢ = 3.1415"

0 = 3.1415 - .0027 = 3.1388"

71



15-11

10°C ref. # No Core

+ Core

Clear Critical Nom. Ht. = $2\frac{3}{16}$ "
 reactivity = +14.83¢

$2\frac{5}{32}$ "
 +19.41¢

$\frac{1}{32}$ " value 15-13 = $\frac{40.05¢}{48.5¢}$ $\frac{1.281¢/\text{mil}}{1.271¢/\text{mil}}$
 13-11 = $\frac{54.3¢}{39.73}$ $\frac{1.271¢/\text{mil}}{2.552}$

✓ 41.93 or $\frac{1.341¢/\text{mil}}{1.310¢/\text{mil}}$
 ✓ 40.96 or $\frac{1.310¢/\text{mil}}{2.651}$
 6.85¢

all Support Value = 7.74¢

Ht of fuel 15-13 = $2.197 - \frac{.197 \cdot .197 \cdot .197}{.197 \cdot .197 \cdot .197} = 2.1970$
 13-11 = $2.197 - \frac{.197 \cdot .197 \cdot .197}{.197 \cdot .197 \cdot .197}$

2.1662 "
 $2.166 - \frac{.166 \cdot .166 \cdot .166}{.166 \cdot .166 \cdot .166} = 2.1662$ "

Use $\frac{1}{2}$ graphite ring (35-15) 952 as
 being 0.04478¢/mil

$\frac{1}{2}$ " (15" dia) on top = 22.30¢

A = Same as (15-7) Pg 52 = 10.0162

A Same = 10.0162

Core = $2.165 - \frac{.163 \cdot .166 \cdot .163}{.163 \cdot .166 \cdot .163} = 2.1642$

2.197 " wtd
 2.194 "

2.166 " wtd
 2.161 "

Pg 4-185
£



15-11

No Core

Nam 14: 15-13 @ 1 1/16"
13-11 @ 1 2 3/32"

Reactivity = + 5.70⁺

Supports = + 2.08⁺

fuel 15-13 = —
13-11 = —

45" x 15" x 1/2" = 10.67⁺

15" x 1/2" C = 7.76⁺

45" x 1/2" C = 18.43⁺

14.17 15-13 = 1.696 - .696 - .696 - .696 = 1.6960
13-11 = 1.725 - .725 - .725 - .725 = 1.7250
- .725 - .725
avg = 1.7093

Mass of C = 1457.751 kg
Vol = 828052 cm³
ρ = 1.760 gm/cc

1.709 wtd
1.708

Core

fuel = 1 1/16" ~~fuel = 1 5 1/32"~~

- 5.31⁺

3.14⁺

33.85⁺ including 1/32" add. C Core
36.16 " " " " "

18.25⁺

Sam = 1.6960
1.695 - .695 - .695 - .695 - .695 - .695 = 1.6950
avg 1.6955

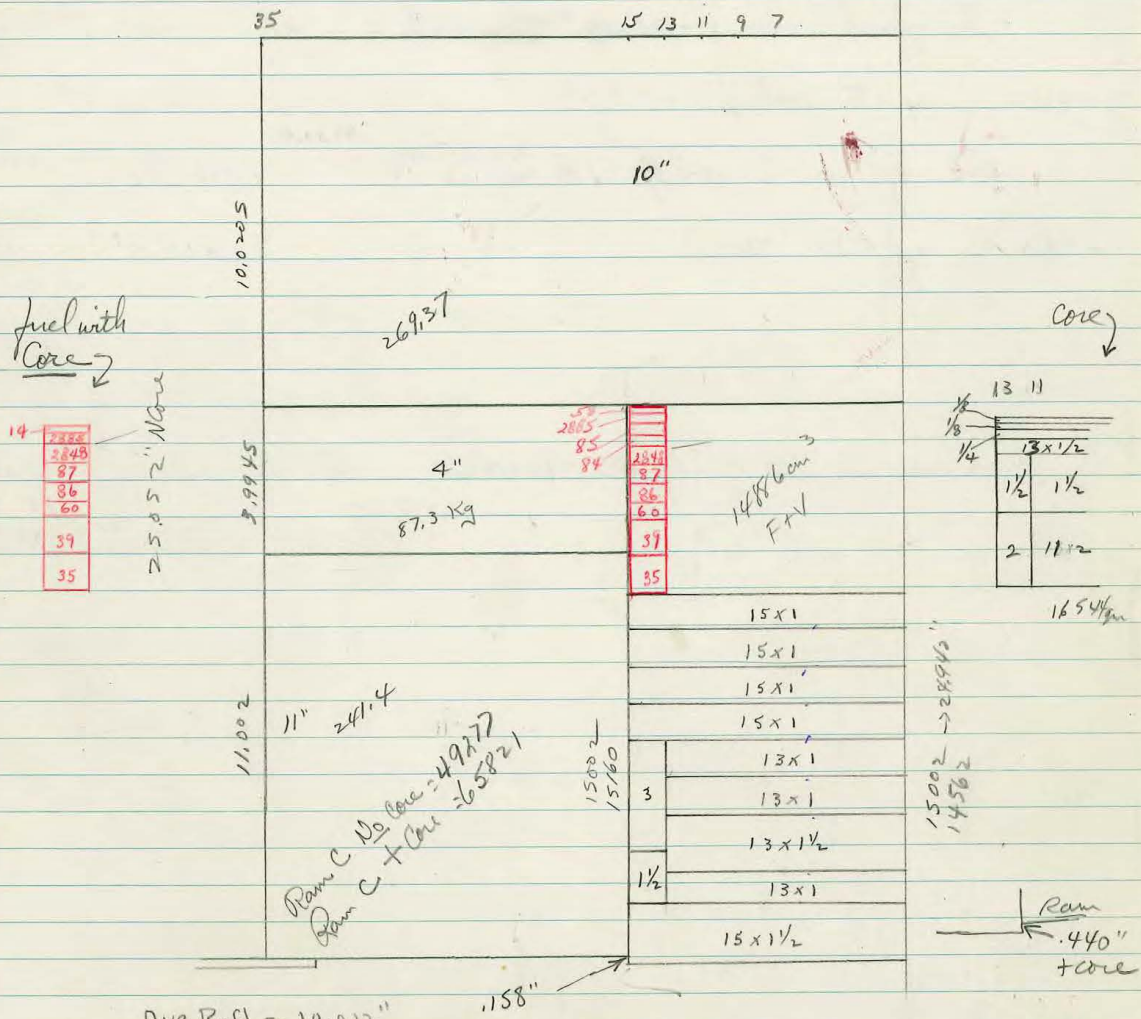
A = 1.689 - .689 - .689 - .689 - .689 = 1.6890
B = Same as 4-189 = 5.0091

= 1462.178 kg
= 820701 cm³
= 1.760 gm/cc

1.696 wtd
1.700

15-13 Ring Only #10" GRAPHITE REFLECTOR { \pm Core
 { \neq No Core

4-
Pg 82



Aug. Refl = 10.012"
No CORE
 MASS OF FUEL = 69048 gm
 Vol = 3693.6704 cm³
 $\rho = 18.6936 \text{ gm/cc}$

MASS RAM GRAPHITE 49277 gm
 FUEL OD(Avg) = 14.99506"
 (OD)² = 224.85182
 ID(Avg) = 13.00218"
 (ID)² = 169.05668

TOT.
 mass C = 647347 Kg
 Vol = 380093
 $\rho = 1.703 \text{ gm/cc}$

CORE
 61078 gm
 3264.7910 cm³
 18.7080 gm/cc
 65821 gm
 14.99528"
 224.85842
 13.00226
 169.05876

mass C =
 663.891 Kg
 Vol C =
 389.981 cm³
 $\rho = 1.702$

15-13 Ring Only & 10" ref(c)

No CORE

Clean Critical Nom. Wt. = ^{5.128} 5 1/8"
 reactivity = -5.92¢

+ 1/32" fuel value = +20.24¢ ✓ 0.6476¢

All Supports value = +7.23¢

Wt. of fuel 15-13 = 5.144 ^{144 144 143} 5.143

+ 0.525" C ref TOP (35-15)

+ CORE

4 1/32"
 +15.47¢

+ 1/32" = +35.17¢ 1.1254¢

+6.04¢

4.546 - .506 - .546 - .546 = 4.546

+15.38¢

A = Same as 15-7 Pg 52 = 10.0162

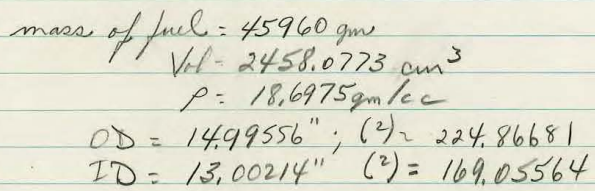
A = Same = 10.0162

Core = 4.505 - .505 = 4.505

5.144
 5.164

4.546
 4.538

4-190



Mass of C = 1511.725 kg
V = 858655 cm³
ρ = 1.760 gm/cc

Arg. Ref 1 = 15.000"

15-13 #15" C. Ref. + Core

$$\text{Nom. } \cancel{15} \frac{13}{32} = 3 \frac{13}{32}$$

$$\text{reactivity} = -8.67^\circ$$

$$\frac{1}{32} \text{ fuel value} = 4454^\circ \quad 1.4252 \frac{\text{ft}}{\text{min}}$$

$$\text{all supports} = 2^\circ$$

$$\text{Carton value} = -$$

$$45" \times 15" \times 12" \text{ C} = 11,034$$

$$\text{fuel measured } 15-13 = 3.422, 422, 422, 422, 422, 422 = 3.422"$$

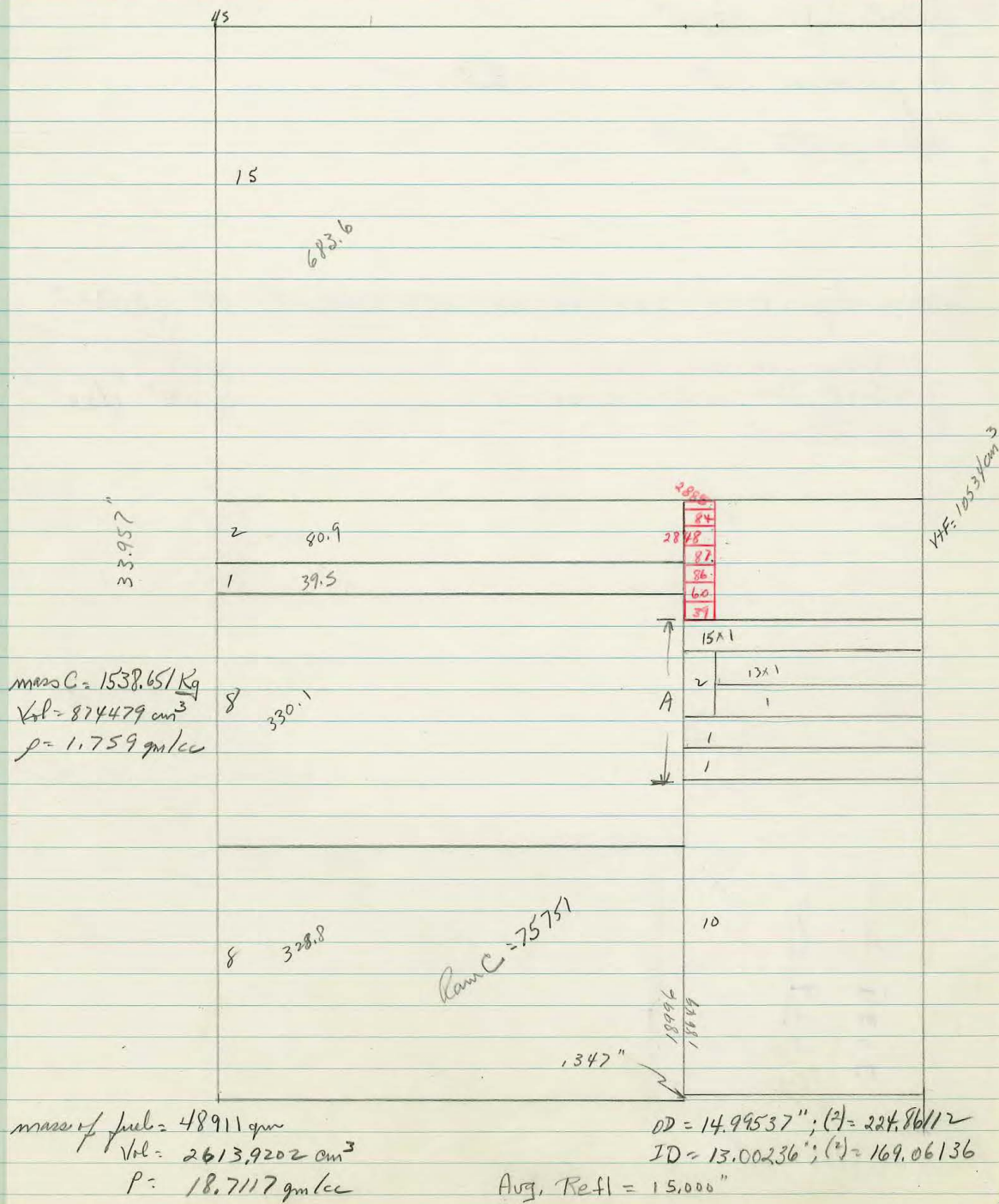
$$A = 3.412, 415, 415, 415, 413 = 3.4140"$$

$$B = \text{Same as } A = 4.189 = 5.0091$$

~~15-13~~
~~15-13~~
~~15-13~~
3.422
3.422
3.422
3.422
3.422
3.422

Q 4-189

4



15-13 + 15" GRAPHITE Ref.

$$\text{Nom. Ht} = 3\frac{5}{8}"$$

$$\text{reactivity} = +12.62^\circ$$

$$\frac{1}{32}" \text{ fuel value} = 32^\circ \quad 1.0240 \text{ mil} \quad \checkmark$$

$$\text{all supports} = 2.01^\circ$$

$$\text{measured fuel 15-13} = 3.640 - .640 - .640 - .639 - .639 - .640 - .640 = 3.6397$$

$$A = 5.022 - .020 - .021 - .019 - .016$$

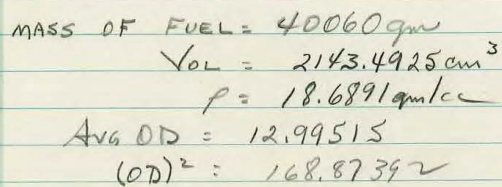
$$\rightarrow 5.008 - .010 - .008 - .012 - .007 - .010$$

A with calipers

$$\frac{2.019}{5.0091"} \text{ Use}$$

3.639 as is
3.629

Pg 4-109




Avg Refl = 11.013"

13" DIA. cyl. # 11" graphite reflector

Nom. Wt. Critical = 7" dia $\times \frac{15}{16}$ " # (13-7) = 1"
 reactivity = 15.02%

$\frac{1}{32}$ " fuel	13-11 = 42.09	d/mult	4.3468	1.313
	11-9 = 48.54		4.5532	1.517
	9-7 = 52.17		4.6694	1.630
7 dia = Not measurable		OK		
all Supports = 9.45%				

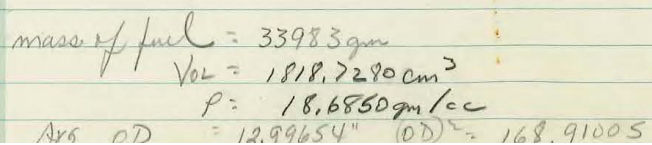
$\frac{1}{32}$ " (2 1/2 x 2 1/2) IN center = 20.98% (Pc #1)
 7" dia \rightarrow  $\frac{1}{32}$ " x 2 1/2 x 2 1/2 = 12.56% (Pc #2)

Wt of fuel 13-11 = 1.006 - .006 - .006 - .006 - .006 - .006 = 1.0060
 11-9 = 1.005 - .005 - .005 - .005 - .006 - .005 = 1.0051
 9-7 = 1.005 - .005 - .005 - .005 - .004 - .005 - .006 - .005 = 1.0050
 7 dia = 0.940 - .940 - .939 - .940 - .939 - .939 - .939 = 0.9394
 avg = 0.9862

A = Lock up = 0.9995"
 B = Lock up = 1.0000

937

By 4-137



Mass of C = 1510.550 Kg
Vol C = 858171 cm³
 $\rho = 1.760$
Avg R = 1.5991"

13" dia Solid # 16" C. ref.

Nom. Ht. Critical: $13-7 = \frac{27}{32}'' \xrightarrow{.84375}$ reactivity + 13.29"
 $7'' = \frac{13}{16}'' \xrightarrow{.8125}$
 Top ref = $\frac{5}{32}''$ Too much

all supports = 40"

$\frac{1}{32}''$ 9-7 = 40.57"
 11-9 = 42.34"
 13-11 = 36.08"

d/mil

~~1.2982~~ 1.267
~~1.3548~~ 1.323
~~1.1545~~ 1.123

10 3/4" / mil

45" OD graphite $\frac{1}{2}'' = 15.68''$

1 ($2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{32}$) @ edge of 7" dia = 13.64"
 1 ($2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{32}$) @ center of 7" dia = 13.75"

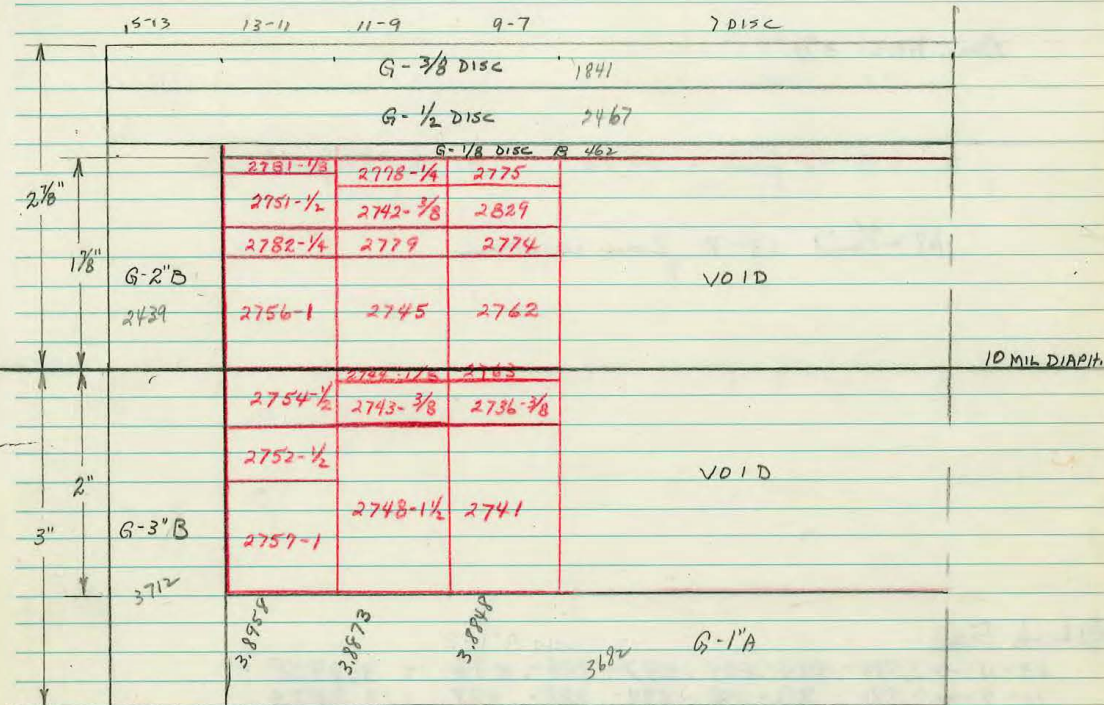
Stiffen = 13-11 = 0.845 - .845 - .845 - .845 - .845 - .845 = 0.8450
 11-9 = 0.845 - .845 - .845 - .845 - .845 - .845 = 0.8450
 9-7 = 0.850 - .850 - .850 all way = 0.8500
 7 dia = 0.813 - .813 - .813 - .813 - .812 - .813 - .813 = 0.8128
 avg = 0.8366

A = 6.007 - .009 - .008 - .009 = 6.0082"
 B = Lock Up = 2.0043
 C = 1.155 - .159 - .159 - .160 - .158 = 1.1582

13-7

1" GRAPHITE REFLECTOR (NO CORE)

Run 67 1-25-63 Pg 100 Bk 1



MASS OF TOP FUEL = 54276 gm
 BOTTOM = 57934

TOTAL = 112.210 Kg

MASS OF TOP GRAPHITE = 7209 gm
 BOTTOM = 7394

TOTAL = 14.603 Kg

(WEIGHTED)
 AVG. O.D. OF ALL FUEL = 12.99599"
 AVG. I.D. OF ALL FUEL = 7.00307"

AVG. WTD HT FUEL (ALL) = 3.8877"

FUEL VOL = 5986.82333 cm³
 FUEL ρ = 18.74283 gm/cc

VOL of all C. stacked = 866863524 cm³
 ρ = 1.68457 gm/cc

Avg Refl = 1.001"

13-7 1" Crp. & Void Core

P.100 BK 1

Critical = -14.37°
 Rings = 5.85°
 Graph = -18.31°
 fuel sup. = 12.06°

Raise .0085"

Nom. Ht. = $3\frac{7}{8}"$

$\frac{1}{16}"$ (13-11) fuel = 30.46° or $0.487^{\circ}/\text{mil}$

$18^{\circ}/\text{mil}$ 13-7 from curve

ALL Ht. FUEL

13-11 $\rightarrow 3.894, .894, .895, .897, .899, .896 = 3.8958^{\circ}$ ✓

11-9 $\rightarrow 3.886, .886, .888, .888, .888, .888 = 3.8873^{\circ}$

9-7 $\rightarrow 3.885, .884, .885, .884, .884, .887 = 3.8848^{\circ}$

wt. avg. 3.8900°

(1x13) + high fuel + (Vp x 13B) = 5.0208

(15-13 3B) + (15-13 2B) = $5.018, .020, .018, .021, .018, .018 = 5.0188$

all Carbon stacked @ 15-13 = $5.906, .907, .905, .909, .908, .908, .905 = 5.9068$

EVEN FUEL Ht. = 3.8900°

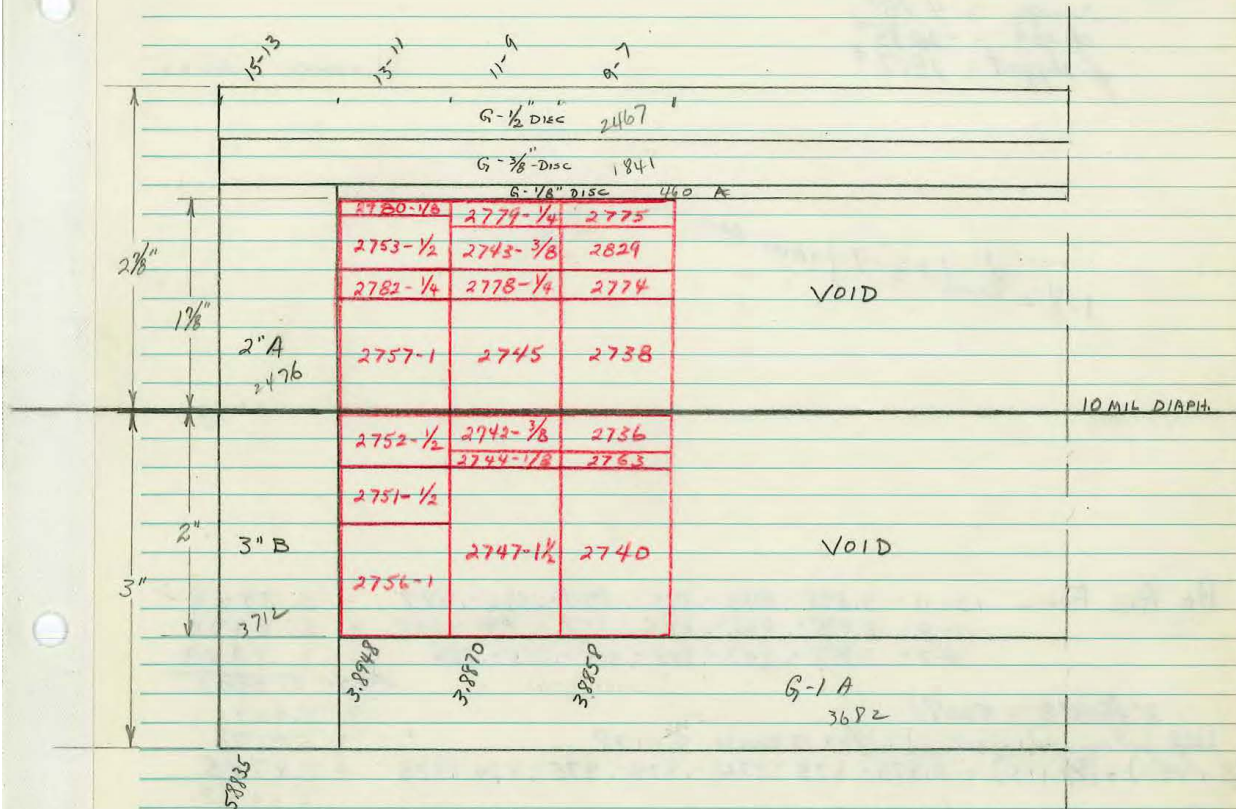
SKY Hook REACT. = -13.97°

13-7 — = 0
 React. = -14.37°
 all support = $+0.40$
 $-13.97 = 3.8900$

$0 = 3.8900 + .0076 = 3.8976$

13-7

1" GRAPHITE REFLECTOR (No CORE)

280263
RUN #70 Pg 252 BK #2

57835
MASS OF TOP FUEL = 54246 gm
BOTTOM = 57892

TOTAL = 112.138 Kg

MASS OF TOP GRAPHITE = 7244
BOTTOM = 7314

TOTAL = 14.638 Kg

AVG O.D. (WTD) ALL FUEL = 12.99616"

168.900174

AVG I.D. (WTD) ALL FUEL = 7.00307"

49.042989

3.889797
AVG Ht (WTD) ALL FUEL = 3.870064

FUEL Vol = 6000.4790 cm³FUEL ρ = 18.6881 gm/cc

Vol of graphite = 8582.05072 cm³
 ρ = 1.70565 gm/cc

Avg Refl = 0.999"

13"-7" 1" C ref WO Core (c)

Rem Ht Critical $3\frac{7}{8}" = + 5.94\frac{1}{2}"$

swing = $4.45\frac{1}{2}"$
 drop = $-20.85\frac{1}{2}"$
 f. support = $18.7\frac{1}{2}"$

Lower .0022"

1.82 9/16" 13-7 from curve

Ht ALL FUEL 13-11: $3.895-.893-.895-.894-.895-.897 = 3.8948"$
 11-9: $3.885-.886-.885-.887-.891-.888 = 3.8870$
 9-7: $3.887-.887-.885-.885-.885-.886 = 3.8858$
 w avg = $3.8898"$

$2"A+3"B = 5.009"$
 High fueling + (1x13 dia) + (1/4 x 13 dia) = 5.0178
 (1/2 x 15") + (3/4 x 15) = $0.875-.875-.874-.874-.875-.874-.875 = 0.8745$
 5.8923

EVEN FUEL HT = $3.8898"$
 SKY NOOK REACT. = $+ 3.64\frac{1}{2}"$

0 Reactivity HT = $3.8876"$

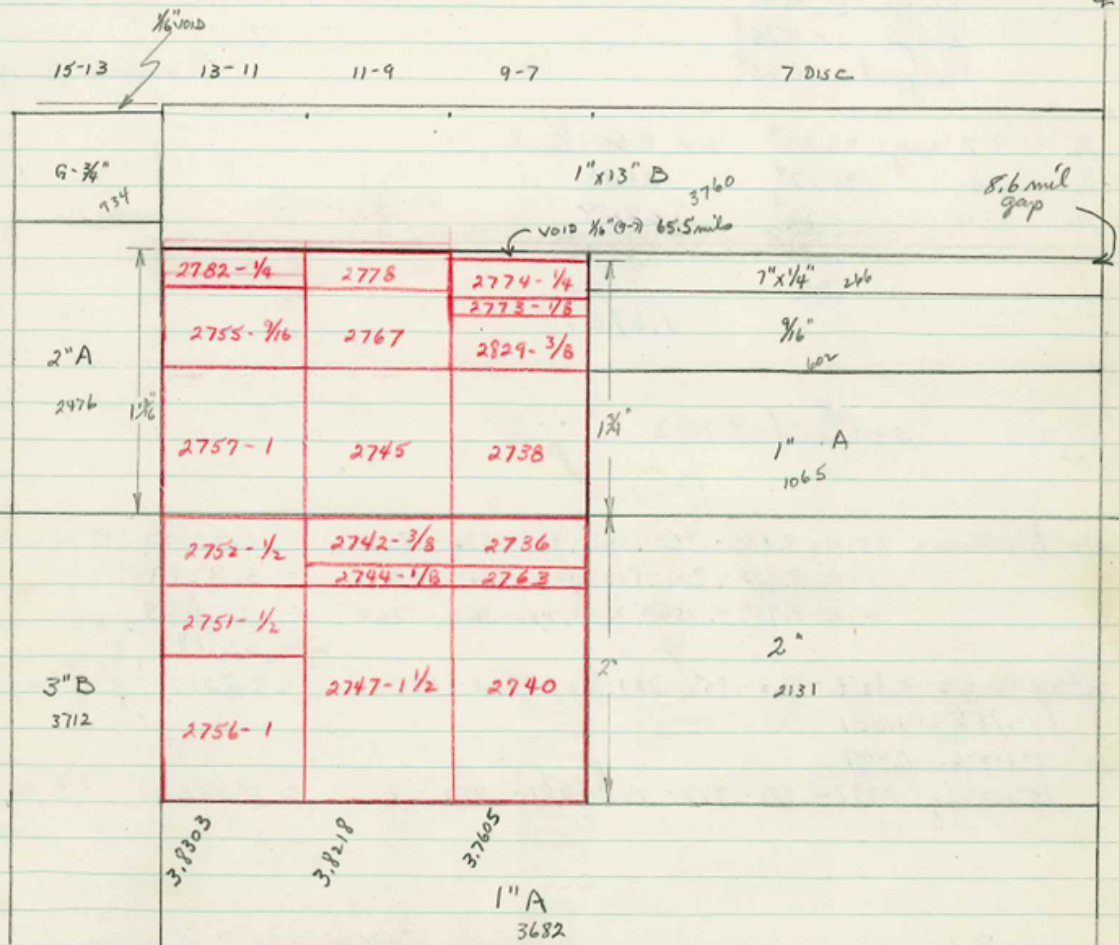
React = $+ 5.94\frac{1}{2}"$
 all support = $- 2.30$
 13-7 = 0
 $+ 3.64$

$0 = 3.8898 - .0020 = 3.8878"$

13"-7"

1" GRAPHITE REFLECTOR + GRAPHITE CORE

Run 84 @ 256



MASS OF TOP GRAPHITE = 9103gm TOTAL = 18.628Kg

BOTTOM = 9525gm

MASS OF TOP FUEL = 51955gm TOTAL = 109.847Kg

BOTTOM = 57892gm

AVG O.D. FUEL (all) wtd = 12.99605" AVG I.D. wtd = 7.00295"

AVG H. FUEL (all) wtd = 168.89731

49.04130

FUEL VOL = 5875.54499cm³FUEL ρ = 18.6956 gm/ccgraphite vol = 10937.41987cm³ ρ = 1.70314 gm/cc

Avg Refl =

13-7 1" Ref + Core (C)

Critical Nom. Ht $3\frac{1}{16}$ on (13-11) + (11-9) + $3\frac{3}{4}$ on (9-7) = + 7.26"

Rings = 3.98"
Diaph = -15.64"
F. support = 16.63"

Lower .0014"

$\frac{1}{16}$ - 9-7 ring	= 36.32"	or 0.5811"/mil
$\frac{1}{16}$ 11-9	= 39.27"	0.6283
$\frac{1}{16}$ 13-11	= 26.80"	0.4288
	102.39"	1.6382
Core		0.345
		1.6727

.024"/mil at 1513

Ht. ALL FUEL = 13-11 = 3.830 - .830 - .830 - .830 - .832 - .830 = 3.8303" ✓
 11-9 = 3.822 - .821 - .822 - .822 - .824 - .820 = 3.8218
 9-7 = 3.759 - .759 - .761 - .760 - .762 - .762 = 3.7605
 w tan = 3.8088"

Ht of Core = 3.822 - .822 - .822 - .821 - .823 - .821 - .821 = 3.8217 (26 mils)
 1" x 13" B = 1.001
 1" x 13" A = 0.999
 15" x 13" ring = 5.787 - .781 - .779 - .782 - .781 - .782 = 5.7820 (+ 26 mils)

EVEN FUEL HEIGHT = 3.8263"

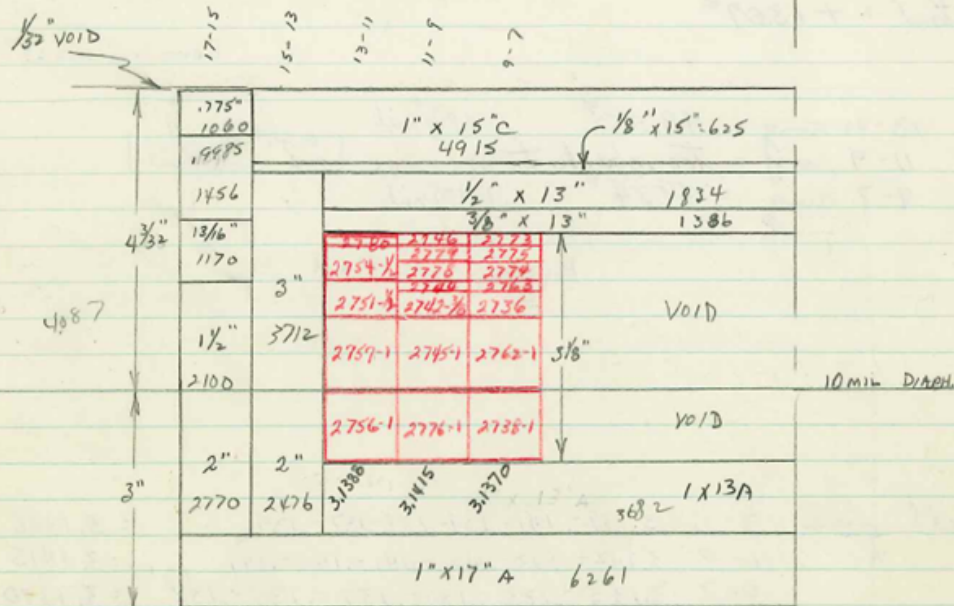
SKYHOOK REACTIVITY = +40.35% (includes $\frac{1}{16}$ " VOID GRAPHITE 15-13 ring)

O React Ht = 3.8074"

15-13 \uparrow 40 = +0.96"
 React = +7.26"
 all support = -4.97"
 13-7 = 0
 Core \downarrow 12.9 = -0.44"
 + 2.81 = 3.8088"
 O = 3.8088 - 0.016 = 3.8072"

13"-7" 2" GRAPHITE REFLECTOR AND NO CORE.

39



MASS OF TOP FUEL = 61563 gm TOTAL = 90.484 Kg
 BOTTOM = 28921 gm

MASS OF TOP GRAPHITE = 18258 gm TOTAL = 33.447 Kg
 BOTTOM = 15189 gm

AVG. O.D. ALL FUEL (W.T.D) = 12.99607" OD² = 168.89783

AVG. I.D. ALL FUEL (W.T.D) = 7.00348" ID² = 49.04873

AVG HT. ALL FUEL (W.T.D) =

FUEL Vol. = 4842.29248 cm³

FUEL ρ = 18.68619 gm/cc

graphite volume = 19687.74009 cm³
 ρ = 1.69887 gm/cc

Avg. Refl = 1.998"

13-7 2" C.ref. # No Core

Critical Nom. $\Delta t = 3\frac{1}{8}" = +16.55^\circ$

riings = $+3.45^\circ$
diagh = $+15.48^\circ$
s. stand = $+13.07^\circ$

Lower .0059"

$\frac{1}{16}"$ 13-11 ring = 48.55° .7768 $^\circ$ /mil
 $\frac{1}{16}"$ 11-9 ring = too much to measure [Est 1.05 $^\circ$ /mil]
 $\frac{1}{16}"$ 9-7 ring = 49.34° .7894 $^\circ$ /mil

Avg = 2.615 $^\circ$ /mil

Wt of all fuel 13-11 = 3.139-.141-.139-.138-.137-.139 = 3.1388"
11-9 = 3.142-.143-.142-.141-.140-.141 = 3.1415"
9-7 = 3.135-.135-.139-.137-.138-.138 = 3.1370"
wt. Wt. = 3.1392"

Top Carbon 17-15: Same as 13-7 with core (7.1435")
15-13: (7.0777")
13 DISC:

Bottom Carbon 17-15:
15-13:
13 DISC:

React = $+16.55^\circ$
all support = -1.04
13-7 = 0
17-15 mil = 0
 $+15.51^\circ$ 3.1392
0 = 3.1392 - .0059 = 3.1333

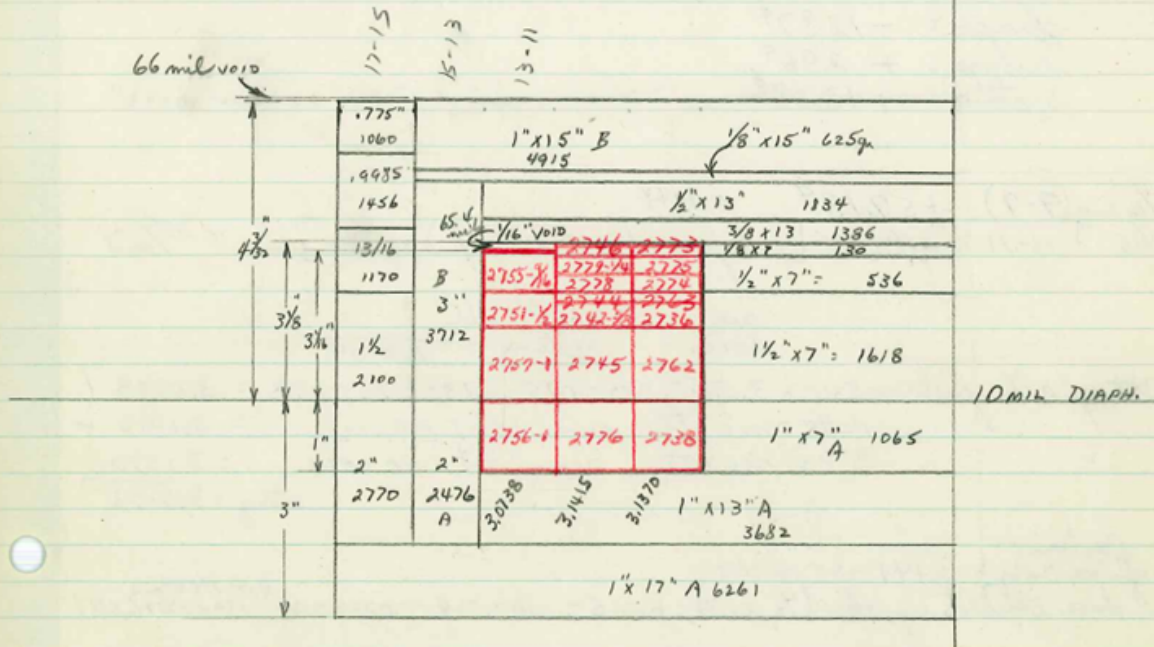
EVEN FUEL Wt. = 3.1392"

SKY NOOK REACTIVITY = $+15.51^\circ$ ($\frac{1}{32}"$ carbon gap 17-15 ring not considered)

0 React $\Delta t = 3.1333"$ ✓

13"-7" 2" GRAPHITE REFLECTOR + G. CORE

Pg 39
#41



MASS OF TOP FUEL = 60811 gm TOTAL = 89.732 Kg
BOTTOM = 28921 gm

MASS OF TOP GRAPHITE = 20542 gm TOTAL = 36.796 Kg OF THIS CORE = 3.349 Kg
BOTTOM = 16254

AVG. O.D. ALL FUEL (W.T'D) = 12.99618" OD² = 168.90069
AVG. I.D. ALL FUEL (W.T'D) = 7.00348" ID² = 49.04873
AVG HT. ALL FUEL (W.T'D) =

FUEL VOLUME = 4802.33484 cm³
FUEL ρ = 18.68507 gm/cc

graphite volume = 21670.59229 cm³
ρ = 1.6979692 gm/cc

AVG REFL = 1.998"

13"-7" 2" Cref. + C core

$$\text{Nom. Ht. Critical} = \begin{array}{l} 3/8" \text{ on } (6-9) \# (9-11) \\ 3/16" \text{ on } (13-11) \text{ ring} \end{array} = +18.97\%$$

$$\begin{array}{l} \text{diaph.} = -12.87\% \\ \text{rings} = +2.96\% \\ \text{5. stand} = +13.08\% \end{array}$$

Lower .0093"

$$\begin{array}{l} 1/16" \text{ ring } (9-7) = +57.15\% \quad 0.914\% \\ 1/16" \quad 13-11 = +41.92 \quad [\text{est. from } (15-9 \# 2" \text{ ref}) \text{ pg } 100] \text{ or } 0.67\% \text{ mil} \end{array}$$

$$\begin{array}{l} \text{avg} = 1.685\% / \text{mil} \\ \text{Core} = .0159 \quad 1.7009 \end{array}$$

$$\begin{array}{l} \text{Ht of all fuel } 13-11 = 3.075 - .075 - .075 - .073 - .072 - .073 = 3.0738 \\ 11-9 = \text{see other run } 13-7 \text{ no core} = 3.1415 \checkmark \\ 9-7 = \text{see other run } 13-7 \text{ no core} = 3.1370 \\ \text{wt avg} = 3.1132" \end{array}$$

$$\begin{array}{l} \text{Carbon} \\ \text{Ht of Core Only} = 3.141 \quad \text{NOT NEEDED} \\ \text{all discs stacked up thru } (1/2 \times 13) = 6.015 - .019 - .024 - .021 - .016 - .015 - .022 = 6.0189 \quad \text{NOT NEEDED} \end{array}$$

$$\begin{array}{l} \text{Measure all stacked } 15" \text{ dia} = 7.145 - .142 - .143 - .142 - .147 - .142 = 7.1435 \\ (17-15) \text{ ring all} = 7.081 - .078 - .073 - .070 - .081 - .079 - .082 = 7.0777 \end{array}$$

$$\begin{array}{l} \text{React} = +18.97\% \\ \text{all support} = -3.17 \\ 13-7 = 0 \\ \text{Core } \downarrow 27.8 = -0.44 \quad 0 = 3.1132 - .0090 = 3.1042" \\ 17-15 \text{ mil} = 0 \\ +15.364 = 3.1132" \end{array}$$

$$\text{EVEN FUEL Ht.} = 3.1655"$$

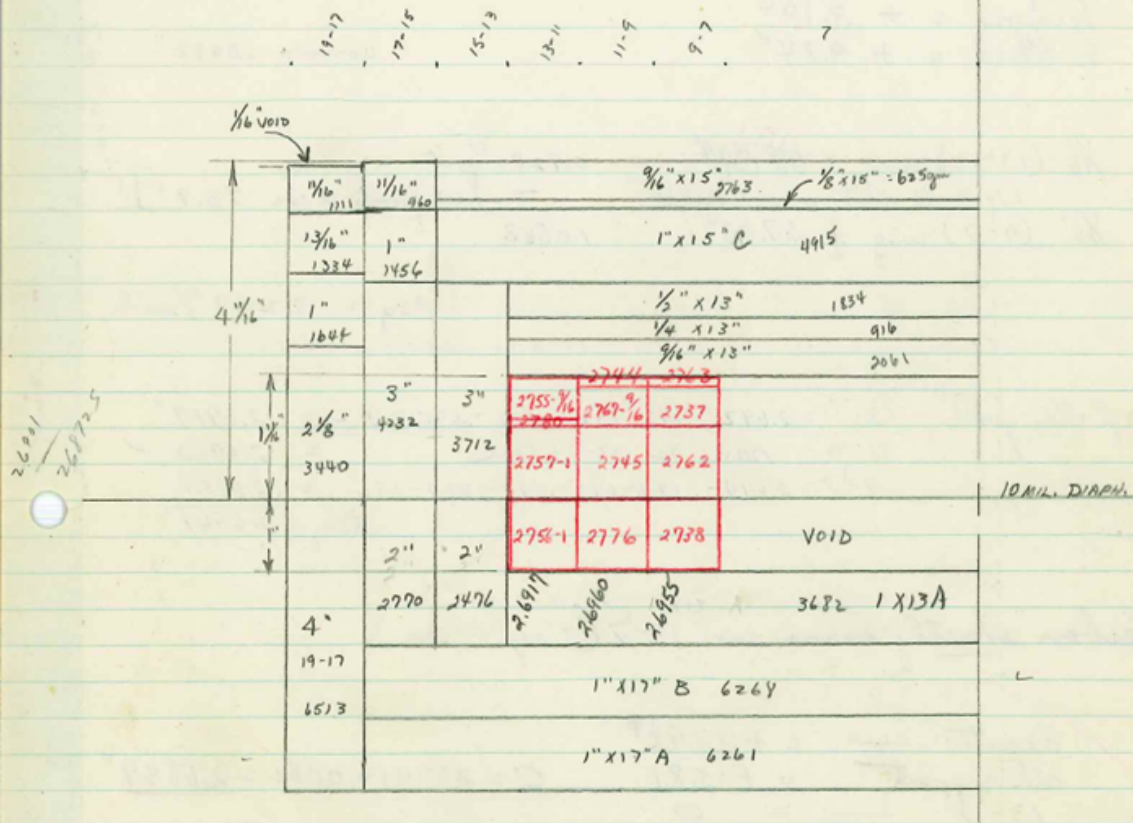
$$\text{SKY Hook REACT.} = +59.61\% \quad (66 \text{ mil carbon void } (17-15) \text{ not considered})$$

$$\text{corrected flat fuel Ht} = 3.1039\% \checkmark$$

use this: 3.106" calc from ring values est. reported.

13"-7" 3" GRAPHITE REFLECTOR \neq NO CORE

Fig 43



MASS OF TOP FUEL = 48788 gm TOTAL = 77.709 Kg
 Bottom = 28921 gm

MASS OF TOP GRAPHITE = 31003 gm TOTAL = 58.973 Kg
 Bottom = 29035 gm

AVG. O.D. ALL FUEL (WT'D) = 12.99625" OD² = 168,90251

AVG I.D. ALL FUEL (WT'D) = 7.00328" ID² = 49.04593

AVG Ht. ALL FUEL (WT'D) =

FUEL VOLUME = 4156.02026 cm³

FUEL ρ = 18.69793 gm/cc

AVG REFL = 2.999"

Vol. of graphite = 34543.76100 cm³
 ρ = 1.70719 gm/cc

13-7 3" C ref # 1/6 Core

Non. HT Critical 2 1/6"

+ 22.90⁺ reactivity

Graph = -16.84⁺

Ring = + 3.19⁺

S. Stand = + 9.84⁺

Lower .0082"

1/6" (13-11) ring = 58.01⁺

11-9 is not measurable

1/6" (9-7) ring = 67.93⁺

0.9281⁺/mil

- [est from 3" w core 75.9⁺]

1.0868

Avg = 3.229⁺/mil

HT of all fuel 13-11 = 2.692-.692-.692-.692-.690-.692 = 2.6917"

11-9 = same as 13-7 + core = 2.6960 ✓

9-7 = 2.694-.697-.695-.694-.697-.696 = 2.6955

w avg = 2.6941"

Carbon exactly same as 13-7 (3" ref + core)

Reactive — = + 22.90⁺

all support — = + 3.81

13-7 — = 0

19-17 mil = 0

0 = 2.6941 - .0082 = 2.6859"

+ 26.71 = 2.6941"

EVEN FUEL HT. = 2.6941"

SKY NOOK REACTIVITY = + 26.71⁺ (1/6" carbon gap 19-17 ring not considered)

0 Reactivity HT = 2.6859" ✓

13"-7" 3" GRAPHITE REFLECTOR + GRAPHITE CORE

243

19-17 17-15 15-13 13-11

90 MIL gap

11/16"	11/16"	9/16" x 15" 2763		1/8" x 15" 625
13/16"	1"	1" x 15" C 4915		
1"	3"	3"	1/16" VOID	1/8" x 13" 1234
2 1/8"	4232	3712	2755-1/16 2744 2760 2767-1/16 2736-1/16	1/8" x 7" 130
3490			2759-1 2745 2762	1" x 7" B 1065
	2"	2"	2756-1 2776 2738	1" x 7" A 1065
4"	2770	2476	2697 2696 2630	3682 1 x 13 A
6513				1" x 17" B 6268
				1" x 17" A 6261

10 MIL DIAPH.

MASS OF FUEL TOP = 48309 gm TOTAL = 77.230 Kg
BOTTOM = 28921 gm

MASS OF GRAPHITE TOP = 322 TOTAL = 61.835 Kg OF THIS, CORE = 2.862 Kg
BOTTOM = 322

AVG. O.D. ALL FUEL (W/T'D) = 12.99625" OD² = 168,90251

AVG I.D. ALL FUEL (W/T'D) = 7.00348" ID² = 49,04873

AVG H. ALL FUEL (W/T'D):

FUEL VOLUME = 4131.86627 cm³

FUEL ρ = 18.69131 gm/cc

graphite volume = 362.45,96655 cm³

ρ = 1.70598 gm/cc

AVG. REFL = 2.999"

13-7 3" C ref + C Core

$$\text{Nom Ht Critical} = \left. \begin{array}{l} 13-11 = 2\frac{1}{16}'' \\ 11-9 = 2\frac{1}{16}'' \\ 9-7 = 2\frac{5}{8}'' \end{array} \right\} \rightarrow \text{period}$$

$$\begin{aligned} \text{Druph} &= -14.35\% \\ \text{Rings} &= +3.54\% \\ \text{S. Stand} &= +9.44\% \end{aligned}$$

$$\begin{array}{l} \frac{1}{16}'' 13-11 = +48.68\% \text{ or } \frac{0.7788}{10105} \text{ mil} \\ \frac{1}{16}'' 11-9 = +63.16\% \text{ or } \frac{0.9124}{10105} \text{ mil} \\ \frac{1}{16}'' 9-7 = +57.00\% \text{ or } \frac{0.9124}{10105} \text{ mil} \end{array} \left. \begin{array}{l} 13-11 = 2\frac{1}{16}'' \\ 11-9 = 2\frac{5}{8}'' \\ 9-7 = 2\frac{1}{16}'' \end{array} \right\} \rightarrow -6.16\%$$

$$\begin{array}{l} \uparrow \\ \text{Avg} = 2.701\%/\text{mil} \\ \text{Core} \quad \frac{.0074}{2.7084} \end{array} \left. \begin{array}{l} 13-11 = 2\frac{7}{8}'' \\ 11-9 = 2\frac{1}{16}'' \\ 9-7 = 2\frac{1}{16}'' \end{array} \right\} \rightarrow +8.32\%$$

$$\begin{aligned} \text{Ht of all fuel } 13-11 &= \text{Same as } 13-7 \text{ Pg 43} &= 2.6917'' \\ 11-9 &= 2.695, .696, .696, .693, .697, .699 &= 2.6960'' \\ 9-7 &= 2.638, .637, .637, .637, .636, .637 &= 2.6370'' \\ & \text{wt avg} = 2.6785'' \end{aligned}$$

$$\begin{aligned} \text{Ht of core only} &= 2.696, .695, .696, .696, .700, .702, .696 = 2.6972'' \\ \frac{1}{16}'' \times \frac{1}{2} \times 13 &= 1.315, .317, .315, .315, .315, .316, .314 = 1.3153'' \end{aligned}$$

$$\begin{aligned} 15'' \text{ dia all} &= 8.710, .718, .715, .710, .709, .707 = 8.7115'' \\ 17-15 \text{ ring} &= 8.724, .719, .722, .730, .724, .720 = 8.7231'' \\ 19-17 \text{ ring} &= 8.635, .633, .632, .633, .630, .634 = 8.6328'' \end{aligned}$$

$$\begin{array}{l} \text{Reactivity} \\ \text{all support} = +1.37\% \\ 13-7 \text{ mil} = 0 \\ 19-17 \text{ mil} = 0 \\ \text{Core } \& 11.7 = -0.13 \end{array} \left. \begin{array}{l} \\ \\ \\ \end{array} \right\} = +1.24\%$$

$$0 = 2.6785 - 1.0004 = 2.6781''$$

(90 mil carbon gap 19-17 ring not considered)

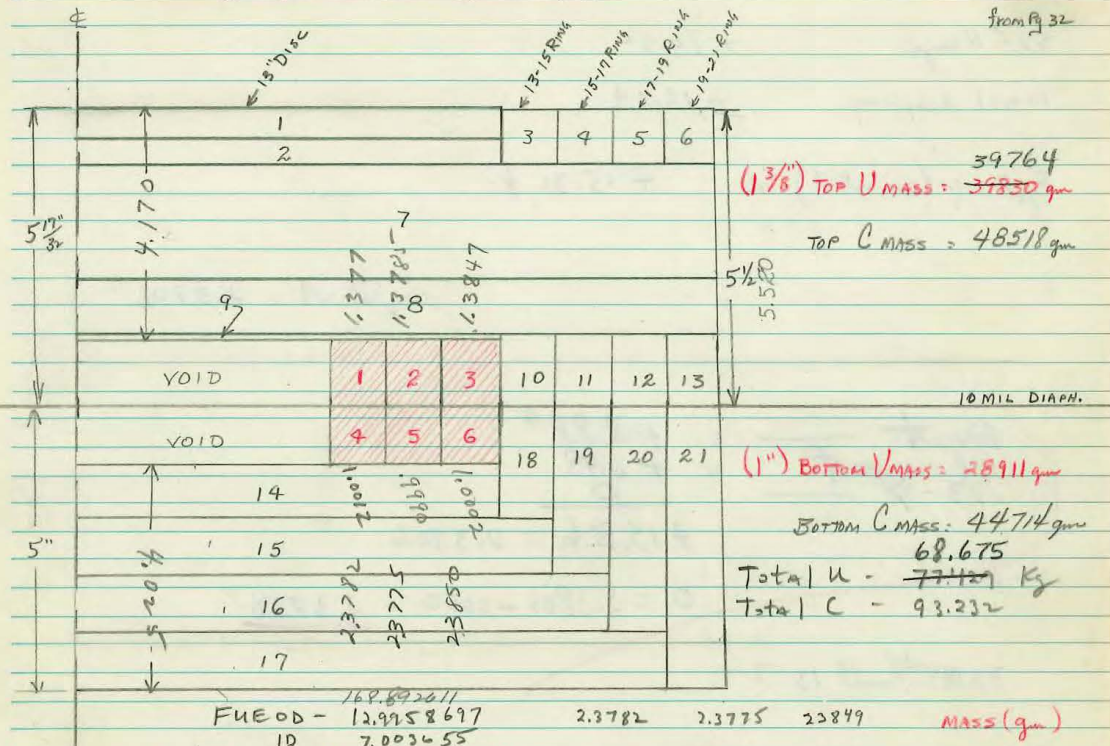
$$\begin{aligned} \text{EVEN FUEL HT.} &= 2.6960'' \\ \text{SKY Hook REACT.} &= +58.51\% \end{aligned}$$

$$\text{Corrected Hot fuel Ht} = 2.6785''$$

13"-7" - 4" C

VOID

from Pg 32



(1 3/8") TOP U MASS = 39764

TOP C MASS = 48518 gm

(1") BOTTOM U MASS = 28911 gm

BOTTOM C MASS = 44714 gm

Total U = 77475 Kg

Total C = 93.232

1	# 2762	(1" 7-9); 2829 (3/8")	7703 + 2895
2	# 2776	(1" 9-11); 2742 (3/8")	9644 + 3617
3	# 2750	(3/8" 11-13); 2781 (1/8"); 2749 (3/8"); 2754 (1/2")	4336 + 1449 + 4360 + 5826
4	# 2738	(1" 7-9)	7710
5	# 2745	(1" 11-9)	9634
6	# 2756	(1" 11-13)	11567
7	1 1/32" x 13" Disc		2007
8	1/2" x 13" A Disc		1834
9	3-4-5-6 1" RINGS	1262 + 1454 + 1644 +	1828
10	2" x 21" Disc		19263
11	1" x 21" Disc		9666
12	1/8" x 13" Disc		461
13	10-11-12-13 1 1/2" RINGS	1870 + 2100 + 2452 +	2677
14	1" x 13" # A		3682
15	1" x 15" # C		4915
16	1" x 17" # B		6268
17	1" x 19" # B		7838
18	1" x 2" B (13-15)		2439
19	1" x 3" A (15-17)		4232
20	1" x 4" (17-19)		6513
21	1" x 5" (19-21)		8827

Fuel vol = 3671.94103 cm³

$\rho = 18.70264 \text{ gm/cc}$

graphite Vol = 54747.39855 cm³

$\rho = 1.70294 \text{ gm/cc}$

AVG REFL = 3.998"

13"-7" 4" C ref WO Core

Clean critical + 8.88¢

SS + Rugs + 10.3~

10 mil diaph-rya - 16.8¢

Est p (corrected) = + 15.36¢

avg ht. wd. = 2.3806"

React
all support
13-7 = + 8.88¢
= + 6.48¢
= 0

+ 15.36 = 2.3806

0 = 2.3806 - .0050 = 2.3756"

3.0185¢/mil 13-7

EVEN FUEL HT. = 2.3806"
SKYHOOK REACT. = + 15.36¢ (extra carbon on top not considered)

13"-7"

4" GRAPHITE REFLECTOR & NO CORE

Pg = 143

10-2-910	21-19	19-17	17-15	15-13	13-11	11-9	9-7	
3/4 1364	1 1/16 1111	1 1/16 960	1 1/2					1/2 x 13 1834
1 1828	13/16 1334	2	1870					1 x 13 B 3760
1 1/2 2677	1 1/2 2438	2 7/8 2770	3 3/4					1 x 13 A 3682
		2 1/16						1 1/2 x 13 5509
2 3546	2 3/8 3863		4628					VOID
	1 1644	1 1456	1 1262	56-1	45	38		VOID
3 9325				21160	23813	24178		1 x 19 B 7838
								1 x 19 A 7828
								2 x 21 19263

10 MIL DIAPH.

MASS OF FUEL = 69383 gm
 VOLUME = 3709.97139 cm³
 $\rho = 18.70176 \text{ gm/cc}$

MASS OF GRAPHITE = 91566 gm
 VOLUME = 53610.96306 cm³
 $\rho = 1.70797 \text{ gm/cc}$

AVG REFL = 3.999"

AVG. O.D. ALL FUEL (W.T.D) = 12.99632"
 I.D. = 7.00307
 21-19 O.D. Carbon = 20.99894"

OD² = 168.90433
 ID² = 49.04298
 440.95548

13-7 4" ref # No Core

2375

Norm. Ht. Critical- $\left\{ \begin{array}{l} 13-11 \\ 9-7 \\ 11-9 \end{array} \right\} 2\frac{13}{32}"$ reactivity = +42.0¢

Rings = +3.70¢
Diaphragm = -16.39¢
S. Stand = +7.04¢

Lower 0.0158"

lms $\frac{1}{32}"$ fuel 13-11 = 23.05¢ 0.7376¢/mil
11-9 = 42.0¢ note: removed from already low ring
9-7 = 29.28¢ 0.9369¢/mil
3.0185 wt vol Avg = 3.0185¢/mil

add 486 mils graphite on 15-13 ring: 11.93 or 0.0295¢/mil

1st of fuel 13-11 = 2.416 - .416 - .415 - .417 - .416 - .416 = 2.4160"
11-9 = 2.381 - .381 - .380 - .382 - .381 - .383 = 2.3813"
9-7 = 2.420 - .418 - .416 - .416 - .418 - .419 = 2.4178"
wt vol Avg = 2.3947"

Ht of Carbon 21-19 = Same as Pg 146 = 10.3034" (-90)
19-17 = Same as 146 = 10.3873" -
17-15 = 10.384 - .386 - .383 - .384 - .381 - .379 - .384 = 10.3830" (-10)
15-13 = Same as 146 = 10.2652" (-13)
13 dia: 8.010 - .014 - .017 - .015 - .011 - .012 - .010 = 8.0127"

Raise 0.0012"

corrected flat fuel height = 2.3801" ✓

Reactivity = — = +42.0¢
all supports = +5.65
13-7 = 0
21-13 mil = 0
+47.65 = 2.3947"
0 = 2.3947 - 0.0157 = 2.3790"

13"-7" 4" GRAPHITE REFLECTOR + GRAPHITE CORE

Pg 146

	21-19	15-17	17-15	15-13	13-11	11-9	9-7	
3/4	1 1/16	7/8						1/2 x 13 1834
1364	1111	1233	1 1/2					
1	13 1/16							1 x 13 B 3760
1828	1334	1 1/2	1970					
								1 x 13 A 3682
1 1/2	1 1/2	2098						
	2438							1 1/2 x 13 5509
2677			3 3/4					
		3A						
2	2 3/8							
3546	3863	4232	4628					1 x 7 B 1065
								3/8 x 7 404
	1	1	1					1 x 7 A 1065
	1644	1456	1262					
3								1 x 19 B 7838
5325								
								1 x 19 A 7828
								2 x 21 19263

MASS OF FUEL = 68748 gm
 VOLUME = 3674.02121 cm³
 ρ = 18.71192 gm/cc

MASS OF GRAPHITE = 94157 gm
 VOLUME = 55120.86160 cm³
 ρ = 1.70795 gm/cc

AVG REFL = 3.999"

AVG. O.D. ALL FUEL (W.T'D) = 12.99592"
 I.D. = 7.00342"
 21-19 OD Carbon = 20.99894"

OD² = 168.89593
 ID² = 49.04789
 — 440.95548

13-7 4" ref. + core

Nom. Ht. Critical = $2\frac{3}{8}"$

reactivity = $+34.53^{\circ}$

Rings = $+3.54^{\circ}$
Diaphragm = -15.31°
S. Stand = $+2.84^{\circ}$

Lower $0.0140"$

$\frac{1}{32}"$ fuel 13-11 = 28.38° 0.9081 $^{\circ}/\text{mil}$
11-9 = 40.26° 1.2883
9-7 = 28.08° 0.8985
3.0949

wt vol Avg = $3.095^{\circ}/\text{mil}$
Core = $\frac{10182}{3.1132}$

add 130 mils on 21-19 ring = 0.13° .001 $^{\circ}/\text{mil}$
add 486 mils 15-13 ring = 12.42° .0245 $^{\circ}/\text{mil}$
less 242 mils 15-13 ring = 8.44° .0348 $^{\circ}/\text{mil}$

Ht of fuel 13-11 = $2.380 - .379 - .380 - .379 - .380 - .381$ = $2.3798"$
11-9 = Same as Pg 143 = $2.3813"$
9-7 = $2.384 - .385 - .385 - .388 - .386 - .387$ = $2.3858"$

wt vol Avg = $2.3779"$

Ht of Carbon: 21-19 = $10.302 - .298 - .307 - .312 - .310 - .298 - .297$ = $10.3034" (-76)$
19-17 = $10.380 - .389 - .392 - .388 - .382 - .383$ = $10.3873" -$
17-15 = $10.388 - .387 - .390 - .386 - .383 - .383$ = $10.3861" -$
15-13 = $10.264 - .272 - .266 - .266 - .266 - .264 - .259$ = $10.2652" (-113)$
13 dia = Same as Pg 143 = $8.0127"$
Core = $2.388 - .388 - .387 - .387 - .388 - .387 - .388 - .389$ = $2.3878"$

Raise $0.0011"$

Corrected flat fuel height = $2.3650"$ ✓

Reactivity = $+34.53^{\circ}$
all supports = $+8.93$
13-7 = 0
21-13 mil = 0
Core & 9.9 = -0.18
 $+43.28^{\circ} = 2.3779"$

$0 = 2.3779 - 0.0139 = 2.3640"$

13-7 6" GRAPHITE REFLECTOR & NO CORE

Pg 255

25 21 17 15 13 11 9 7

1.2 4895		$\frac{1}{16}$ 1111	$\frac{7}{8}$ 1233	1 1262	$1\frac{1}{2}$ 1588	$1\frac{1}{2} \times 11$ 3929												
	3 5325	1 1644	1 1456	2 2459		1 X 13 C 3745												
		$2\frac{3}{4}$ 3863	3B			1 X 13 B 3760												
7			4188	2 2476		1 X 13 A 3682												
28700	5					$1\frac{1}{2} \times 13$ 5509												
	8827	4 6513	3A 4232	3 3712	<table><tr><td>15-40</td><td>16</td><td>17</td></tr><tr><td>80-78</td><td>42</td><td>63</td></tr><tr><td>55-76</td><td>67</td><td>37</td></tr><tr><td>56-1</td><td>45-1</td><td>38-1</td></tr></table>	15-40	16	17	80-78	42	63	55-76	67	37	56-1	45-1	38-1	VOID
15-40	16	17																
80-78	42	63																
55-76	67	37																
56-1	45-1	38-1																
6868		$\frac{1}{2} \times 25$																
1 4234	1 1828	$1\frac{1}{2}$ 2438	$1\frac{1}{2}$ 2098			$1\frac{1}{2} \times 15$ 7485												
	$1\frac{1}{2}$ 2677					1 X 19 7828												
$4\frac{1}{2}$						1 X 21 9666												
18455						2 X 21 19263												

15 MIL DIAP.

MASS OF FUEL = 56909 gm

VOLUME = 3040.29 cm^3

$\rho = 18.71825 \text{ gm/cc}$

MASS OF GRAPHITE = 186929 gm

VOLUME = 108786.135 cm^3

$\rho = 1.718319 \text{ gm/cc}$

AVG. OD OF FUEL = 12.99659"

OD² = 168.91135

AVG ID OF FUEL = 7.00271"

ID² = 49.03794

AVG REFL = 6.001"

13-7 6" ref # No Core

nom. Ht. Critical = $1\frac{3}{32}$ "
 support stand = 2.74"
 support ring = 1.68"
 diaphragm = -1.70"
 $\frac{1}{2}$ " al diaph. support = 2.82"

two runs
 reactivity = $+15.71$ > $+15.11$ #

$\frac{1}{32}$ " fuel 13-11 = 31.56"
 11-9 = 57.70"
 9-7 = 38.11"

#/mil
 0.9632
 1.0099
 1.8464
 1.2195
 4.0758

red is avg
 ↑ & ↓ mils

-389 mils ^{top} graphite 25-21 = 1.69"
 -222 21-19 = 1.42"
 -248 19-17 = 2.59"
 -193 17-15 = 3.01"
 -244 15-13 = 5.62"
 -125 13-11 = 6.47"
 -125 11-9 = 10.13"
 -125 9-7 = 3.3"
 -125 7" dia = 5.52"
 +125 11" dia = 11.88"

React = +15.11"
 ↓ 218 mils = -0.94"
 ↓ 45 = -0.28"
 ↓ 108 = -1.12"
 ↑ 54 = +0.84"
 ↓ 58 = -1.33"
 ↓ 13 = -0.67"
 ↓ 13 = -1.05"
 ↓ 13 = -0.34"
 ↓ 13 = -0.57"
 all supports = +4.46"
 1.9706" = +14.11"
 (-3.4 mils) = 1.9672" — clean

Ht of carbon 25-21 = 14.210 - .186 - .180 - .180 = 14.184"
 21-19 = 14.020 - .007 - .020 - .018 = 14.016"
 19-17 = 14.080 - .074 - .078 - .085 = 14.079"
 17-15 = 13.912 - .929 - .912 - .914 = 13.917"
 15-13 = 14.028 - .025 - .020 - .043 = 14.020"
 13 dia = 12.006 - .023 - .011 - .015 = 12.013"

Ht of fuel 13-11 = 1.970 - 970 - 969 - 970 - 970 - 970 = 1.9698"
 11-9 = 1.971 - 971 - 971 - 970 - 970 - 971 - 971 = 1.9707"
 9-7 = 1.972 - 972 - 972 - 972 - 972 = 1.9720"
 wt avg = 1.9706"

13-7 6" GRAPHITE REFLECTOR + GRAPHITE CORE

P 262

25	21	19	17	15	13	11	9	7
.8 3283		1 1/16 1115	7/8 1233	1 1262	1 1/2 1588	1 1/2 x 11 3929		
	3 5325	1 1664	1 1456	2 2439		1 x 13 C 3745		
		2 3/8 3863				1 x 13 B 3760		
			3B 4188	2 2476		1 x 13 A 3682		
7 28700	5 8827					1 1/2 x 13 5509		
		4 6513	3A 4232	3 3712	<div> <div>13 66</div> <div>15 67</div> <div>16 68</div> </div>	<div> <div>9 1/16 x 7 602</div> <div>3 3/8 x 7 404</div> <div>1 x 7 1065</div> </div>	1/2 Void	
					<div>55</div> <div>45</div> <div>38</div>			
		6868	1 1/2 x 25					15mil DIAPH
1 4234	1 1828	1 1/2 2439	1 1/2 2098			1 1/2 x 15 7495		
	1 1/2 2677					1 x 19 7828		
4 1/2 18455						1 x 21 7666		
						2 x 21 19263		

MASS OF FUEL = (Fuel to 255) 56909 gm

ρ = Same = 18.71825 gm/cc

MASS OF GRAPHITE = 187388 gm

VOLUME = 109524.47822 cm³

ρ = 1.71092 gm/cc

AVG REFL = 6.001"

13-7 6" ref + core

Nom. Wt. Critical = $1\frac{31}{32}$ " }
Core = $1\frac{5}{16}$ " }

two runs
reactivity = $32.46\frac{+}{-}$ } $+ 30.82\frac{+}{-}$ } $+ 31.64\frac{+}{-}$

diaphragm = $-7.08\frac{+}{-}$
 $\frac{1}{2}$ " al support = $+1.80\frac{+}{-}$
qui g = $+1.02\frac{+}{-}$
s. stand = $+3.88\frac{+}{-}$

$\frac{1}{32}$ " fuel 13-11 = $30.00\frac{+}{-}$ or $0.9600\frac{+}{-}/mil$
11-9 = $41.74\frac{+}{-}$ $1.3356\frac{+}{-}/mil$
9-7 = $29.00\frac{+}{-}$ $0.9280\frac{+}{-}/mil$
Center of \swarrow $3.2236\frac{+}{-}/mil$

(-) $\frac{1}{8}$ " carbon 7" dia. located $\frac{3}{32}$ " below fuel top = $10.71\frac{+}{-}$ or @ $1.875/cm Bo\frac{+}{-}$
(+) $\frac{1}{8}$ " located 0.9375 " above bottom of fuel = $1.75\frac{+}{-}$
" " 1.1875 " = $2.44\frac{+}{-}$
" " 1.625 = $4.93\frac{+}{-}$
" " 1.750 = $8.79\frac{+}{-}$

$\approx 11\frac{+}{-}$ per $\frac{1}{8}$ " at top of graphite core = $11.0\frac{+}{-}$ = $.0880\frac{+}{-}/mil$

Wt. of carbon 25-21: $13.988 - .988 - .980 - .984 = 13.9850$ "
21-19: Same as 255 14.0162 "
19-17: Same 14.0792 "
17-15: Same 13.9167 "
15-13: Same 14.0290 "
13 dia: Same 12.0132 "
Core = $1.937 - 936 - 935 - 937 - 939 - 937 = 1.9368$ "

Wt. of fuel 13-11 = Same as pg 255 $: 1.9698$ "
11-9 = Same 255 $: 1.9707$ "
9-7 = Same 255 $: 1.9720$ "
wt avg = 1.9706 "

Reactivity: $+ 31.64\frac{+}{-}$
all supports = $+ 0.38\frac{+}{-}$

25-21 $\downarrow 14 mils = -0.06$
21-19 $\downarrow 45 = -0.28$
19-17 $\downarrow 108 = -1.12$
17-15 $\uparrow 53 = +0.82$
15-13 $\downarrow 58 = -1.33$
Core $\uparrow 35 = +2.90$
13-11 $\downarrow 13 = -0.67$
11-9 $\downarrow 13 = -1.05$
9-7 $\downarrow 13 = -0.34$
7 dia $\downarrow 13 = -0.57$

$1.9706 = +30.32\frac{+}{-}$
 $(-9.4 mils) : 1.9612 = \text{clean } \infty$

[illegible]

Avg REFL = 8,000"

13-7 8" ref. & No Core

SEE + Core below

Nom. Wt. Critical = $9-7 = 1\frac{1}{16}"$ } 1.71
 $13-9 = 1\frac{23}{32}"$

reactivity = +0.87⁺

diaphragm = -12.86⁺
 ring & ring support = +3.08⁺
 support stud = +2.00⁺ calc from prev. runs.

MASS OF FUEL = 49499 gms
 VOL = 2650.81152 cm³
 $\rho = 18.6731 \text{ gm/cc}$

MASS OF GRAPHITE = 324650 gms
 VOL = 188052.2300 cm³
 $\rho = 1.72638 \text{ gm/cc}$

$\frac{1}{32}"$ fuel 13-11 = 35.00⁺ or 1.1200⁺ /mil
 11-9 = 37.99⁺ } 38.894⁺ or 1.2444⁺ /mil
 9-7 = 39.79⁺ or 1.3168⁺ /mil
 41.15⁺ or 3.6812

FUEL OD = 12.99608"
 ID = 7.00250"
 49.0350

13-7 8" ref + core

1.7143" clean

Nom. Wt. = Same

reactivity = +16.23⁺

diaph = -13.80⁺
 all support = -12.18⁺ > -12.99⁺
 all support = +5.37⁺

ρ OF FUEL = 18.67314 gm/cc
 MASS OF GRAPHITE = 326447 gms
 VOL = 189084.61993 cm³
 $\rho = 1.72646 \text{ gm/cc}$

$\frac{1}{32}"$ fuel 13-11 = 33.54⁺ or 1.0732⁺ /mil
 11-9 = 39.91⁺ or 1.2771⁺ /mil
 9-7 = 40.75⁺ or 1.3040⁺ /mil
 3.6543

1.7094" clean

Wt of fuel 13-11 = 1.729 - 729 - 729 - 730 - 729 - 730 - 731 - 730
 11-9 = 1.724 - 724 - 724 - 724 - 724 - 724
 9-7 = 1.694 - 694 - 694 - 696 - 695 - 694

= 1.7296"
 = 1.7240"
 = 1.6945"

wt avg = 1.7183

Wt of Carbon = 29-25 = 17.300 - .287 - .290 - .290 = 17.2917"

25-21 = 17.995 - 18.010 - .002 - 17.980 = 17.9967"

21-19 = 17.929 - .925 - .926 - .928 - .928 = 17.9272"

19-17 = 17.976 - .970 - .980 - .974 - 17.9750"

17-15 = 17.731 - .734 - .735 - .743 = 17.7357"

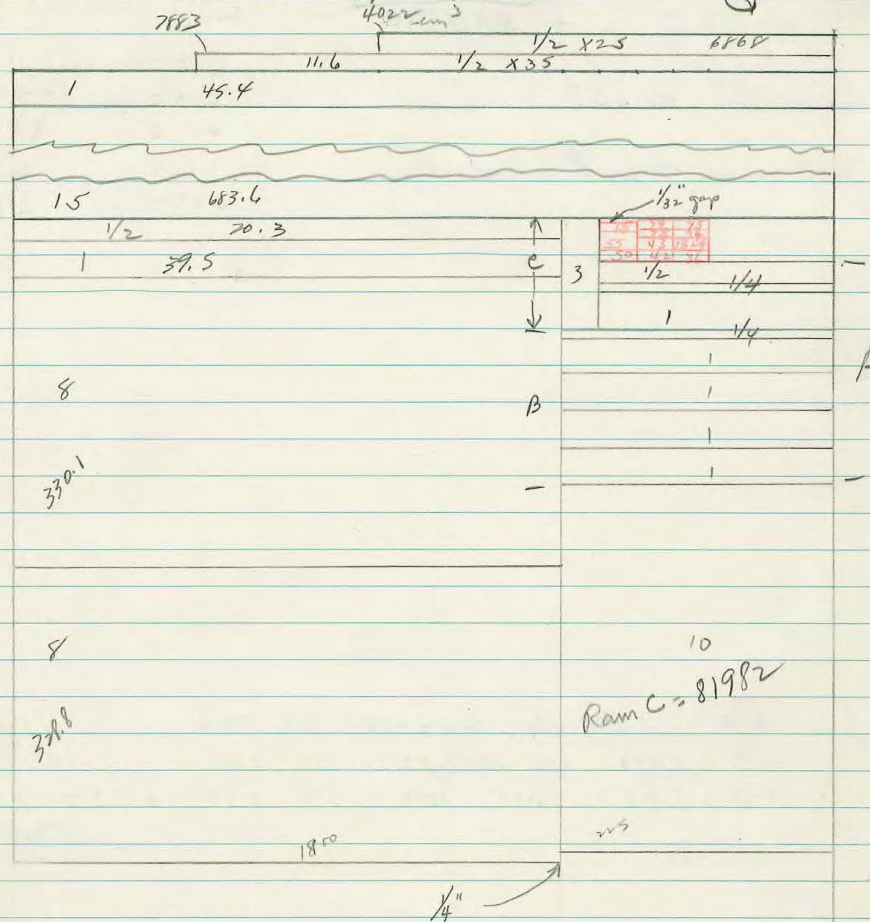
15-13 = 17.774 - .760 - .775 - .760 = 17.7672"

13-11 = 16.016 - .008 - .006 - .025 = 16.0137"

7" core = ~~1.636~~ 637 636 638 636 638 636 = ~~1.6367~~
 1.688"

13" 7" & 16" GRAPHITE REFLECTOR # No One

By 4-202



Mass of fuel = 35800 gm
 Vol = 1914.2743 cm³
 $\rho = 18.7016 \text{ gm/cc}$
 Fuel OD = 12.99591" (π) = 168.89367
 ID = 7.00312" (π) = 49.04368

Mass of C = 1548150 gms
 Vol = 884226 - 2732 = 881494 cm³
 $\rho = 1.756 \text{ gm/cc}$

Avg REFL = 16.000"

13-7 & 16" C. up. No Core

nom. 1st. Critical: (11-7) = $1\frac{1}{4}$ " & (13-11) = $1\frac{7}{32}$ "
reactivity = + 7.54%

Supports: +1.65%

fuel value \rightarrow not measured

25" x 2" Core 10.76%

fuel 13-11 = 1.220 - .220 - .220 - .219 - .219 - .219 = 1.2195
11-9 = 1.256 - .256 - .256 - .257 - .256 - .256 = 1.2561
9-7 = 1.255 - .255 - .254 - .254 - .254 - .255 - .255 = 1.2545
wt avg = 1.2510

A Same 4-204 = 6.0120"
B Same 4-204 = 4.2527"
C Same 4-204 = 3.0030"

1.241
1.240
8

13-7 $\pm 16"$ C. of + Core

nom. Ht. Critical : $(13-9) = 1\frac{1}{4}"$ & $(9-7) = 1\frac{7}{32}"$

Reactivity: +27.06%

fuel value = not measured

$25" \times \frac{1}{2}" C = 10.76 \text{¢}$

Final 13-11: 1,255-255-255-255-255-255-255. = 1,2550
11-9: = 1,2561 = 1,2561
9-7: 1,224-224-224-224-224-225 = 1,2241 = 1,2241
wt avg: 1,2471

A = 6.015 - .012 - .011 - .010 = 6.0120
B = 4.255 - .252 - .252 - .252 = 4.2527
C = Fork hp = 3.0030
D = 1.251 - .252 - .251 - .251 = 1.2510

1,247
1,240

		GRAPHITE - C - 1.72176		13-9
		3745g		1" C Refl + C Core
G R A P H I T E	2781	2767	✓ G 1/4 2212	(p.62 BK 1)
	2780		G 1/4 715g	
	2783			
	2755	2747	✓ G 3/8 668g	
	2782		✓ G 1/2 583g 1.694012	
	2750		✓ G 9/16 978g 1.701888	
	2749	2742 2776	✓ G 1 1771g 1.698777	P6 in h 1.70275 1.69292
	2754			
6781g		2753	✓ G 1 1/2 2075g 1.710628	
14.998 13.015 1.983		2756		
		2745		

H	5.5	4.078625	4.06375	
M		47.088	4.0711975 - Av.	7661g
P		18.68402	37.124	Av U
			18.700979	

G R A P H I T E	2752	2746		n ₁ 9.001747
	2751	2742		n ₂ 10.99677
	2757	2748	GRAPHITE 2"	n ₃ 11.00283
			3533gm	n ₄ 12.99591
3710g			1.69448	n ₅ 13.00
15.000 13.000				
		GRAPHITE - A		4.0625 2.0465 6.0702
		3682g		

H	3"	2.01225	2.0065	
		2.009375		
M		23.208	19.317	Av H of fuel
P		18.66906	18.7003	6.0805625
Total Mass = U =		128.737 Kg		Av. P 18.6932

TOT. Mass of C = 28.647 Kg ± P = 1.707

13-9 RING 1" GRAPHITE REFLECTOR

AVG REFL = 0.998"

Measurements

Clear Critical

-1.46 ϕ

REACTIVITY EFFECTS

Lower Support

11.54 + 4.89 ϕ \rightarrow +5.15 ϕ

10 mil Diaphragm

-8.27 ϕ

Support ring

6.96 ϕ

Planks - 0.63 ϕ

CORRECTED REACTIVITY

-5.3 ϕ

S_g 16 gr 10⁻⁵ TOC HANSEN

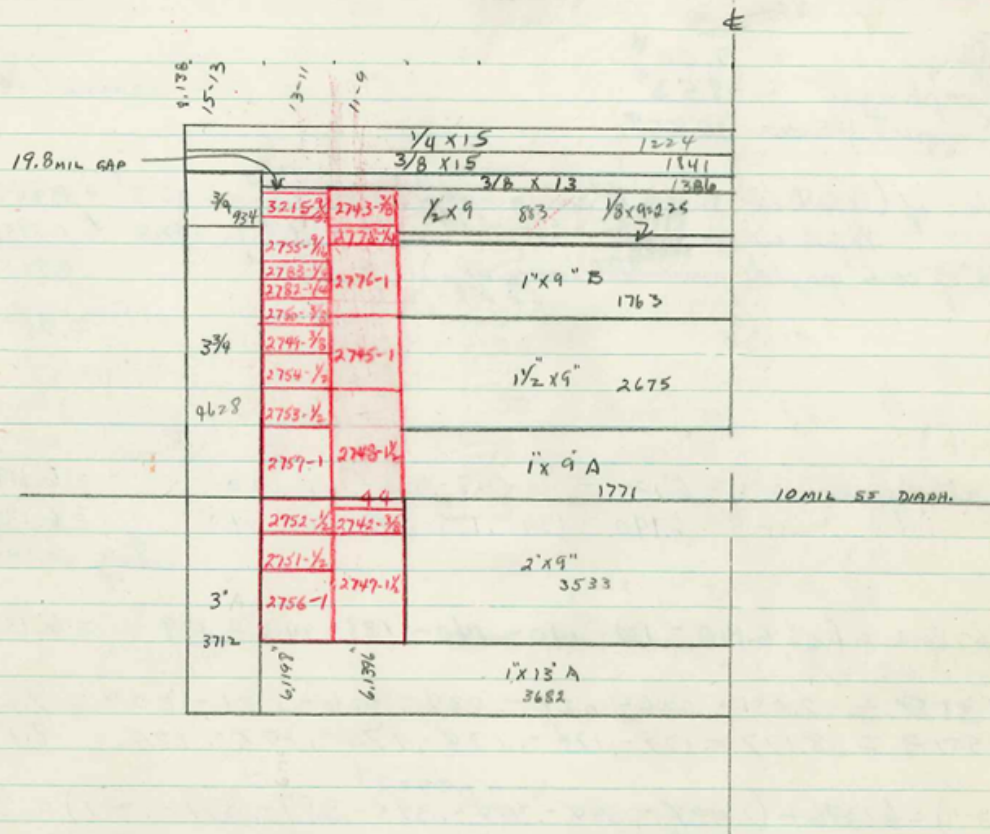
K = 1.003341

C HT = 6.062"

+ .006" (7 per, 1 mil per spou)
6.068"

13"-9" 1" GRAPHITE REFLECTOR & G. CORE

Q 85



MASS OF FUEL = 129702 gm
VOLUME = 6930.41620 cm³
 $\rho = 18.7148 \text{ gm/cc}$

MASS OF GRAPHITE = 28257 gm
VOLUME = 16708.56935 cm³
 $\rho = 1.69116 \text{ gm/cc}$

AVG. O.D. ALL FUEL (WT'D) = 12.99597" $OD^2 = 168.89523$
AVG. I.D. ALL FUEL (WT'D) = 9.00197" $ID^2 = 81.03546$
15-13 OD Carbon " = 14.99865" $(?) = 224.95950$

Avg Refl = 0.999"

13-9 1" ref. + core

Norm. Wt. Critical = $13-11 = 6\frac{3}{32}" \nless 11-9 = 6\frac{1}{8}" = -25.00^{\circ}$

Rings = 7.00¢
Diaphragm = -8.53¢
Support Stand = 10.35¢

Raise .0641"

Value of (1/8 fuel on 13-11 + 1/8" core graphite) = +54.9⁴ = 30.5⁴ ✓ 0.2440⁴ fuel
 " " 1/8 fuel on 11-9 + 1/8" " " = +59.8⁴ = 35.4 ✓ 0.2832
 1/8" of core graphite removed (leaving gap) = 24.4⁴
 + Core = 0.5693

1st. all fuel $13-11 = 6.120 - .119 - .117 - .120 - .121 - .122 = 6.1198''$
 $11-9 = 6.140 - .139 - .139 - .140 - .140 - .140 = 6.1396''$
 average $= 6.1288''$

$$\text{Net of Core only} = 6.140 - .139 - .140 - .140 - .138 - .140 - .139 - .14 = 6.1394''$$

$$13-9 = 2.031 - .026 - .028 - .029 - .026 - .031 - .029 = 2.0285''$$

$$115-13 = 8.177-177-174-174-175-177-174 = 8.1754'' \quad OK$$

$$(13-9) = 6.1396 + (1.394 - 394 - .394 - .395 - .389 - .391 - .391) = 7.5321''$$

$(3 + 3\frac{3}{4} + 3\frac{3}{4}) = \frac{\text{compare for gap at where? mil}}{7.530 - .524 - .535 - .534 - .526 - .531} = 7.530''$

Corrected flat fuel $HX = 6.1929''$ ✓

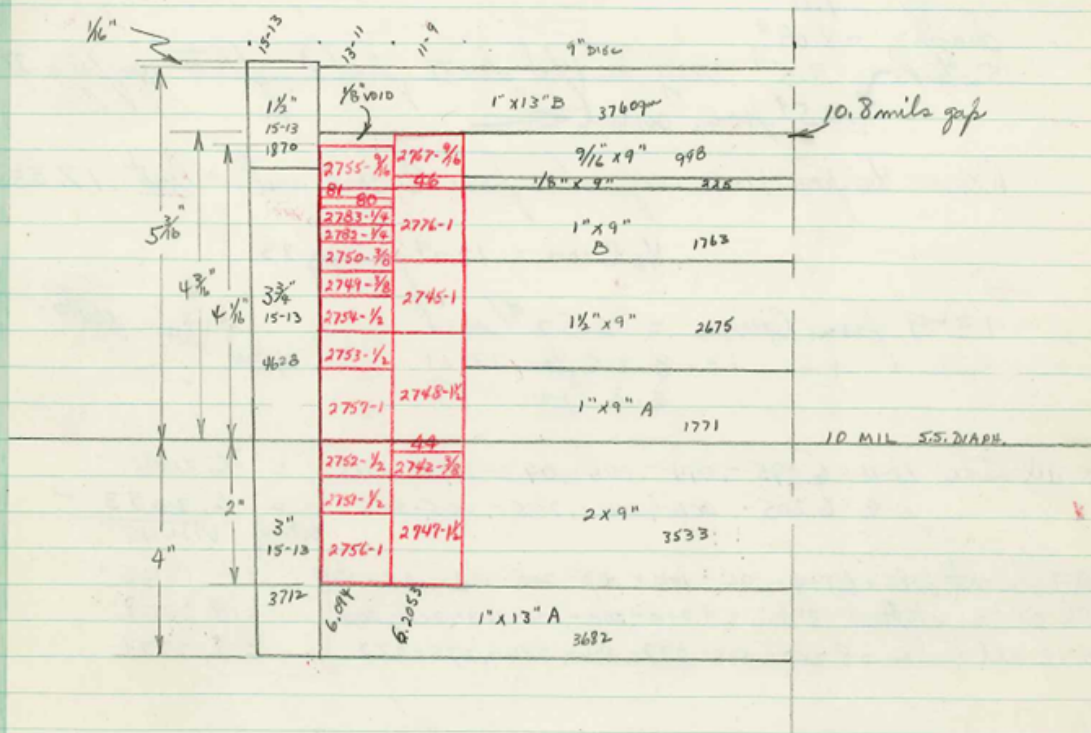
Reactivity = -25.00 ϕ
 all Support - 8.82 ϕ
 13-11 - 0 ϕ
 11-9 down 19.8 miles = -5.60 ϕ
 Core (+0.0421 mi) down 14.6 +0.82 ϕ
 -40.97 ϕ

$$-40.92^\circ = 6.1198''$$

$$O = 6.1198 + 0.0719 = \underline{6.1917}$$

13"-9" 1" GRAPHITE REFLECTOR + GRAPHITE CORE

292



MASS OF TOP GRAPHITE: 17690 gm TOTAL = 28.617 Kg
 BOTTOM = 10927

MASS OF TOP FUEL = 87484 gm TOTAL = 129.960 Kg
 BOTTOM = 42476

AVG O.D. ALL FUEL (W.T'D) = 12.99591" (O.D.)² = 168,89367
 AVG I.D. ALL FUEL (W.T'D) = 9.00184" (I.D.)² = 81.03312
~~AVG H.C. ALL FUEL (W.T'D):~~

FUEL VOLUME = 6948.39069 cm³
 FUEL ρ = 18.70361 gm/cc

graphite vol = 16787.91791 cm³
 ρ = 1.70461 gm/cc

AVG REF L = 0.998"

13"-9" 1" ref + C Core

NOTE: RERUN pg 85 (BK 3)
+ p. 62 (BK-1)

Dom. Ht. Critical = $6\frac{1}{16}$ on 13-11 \neq $6\frac{3}{16}$ on 11-9 = $+13.25\frac{1}{16}$

ring = $7.11\frac{1}{16}$

chaph = $-8.09\frac{1}{16}$

S. stand = $3.5\frac{1}{16}$

very doubtful due to fuel & reflector configuration.
 $\rightarrow 10.5\frac{1}{16}$ from curve \leftarrow

Remove $\frac{1}{16}$ from 11-9 ring also from C core and we lost $17.55\frac{1}{16}$

$\frac{1}{16}$ C core = $12.2\frac{1}{16}$ from pg 85 ?

13-9 from Curve = $0.52\frac{1}{16}$ mil

LC = $0.25\frac{1}{16}$ for 13-11

$0.27\frac{1}{16}$ for 11-9

Total Value = $156\frac{1}{16}$ mil

Ht. all FUEL 13-11 = $6.095 - .094 - .094 - .093 - .093 - .095 = 6.094''$

11-9 = $6.205 - .206 - .206 - .205 - .205 - .205 = 6.2053''$
wt avg $6.1445''$

all Core ht. only = $6.194 - .194 - .194 - .198 - .200 - .194 - .195 - .195 = 6.1945$

all carbon stalked 13" dia = $8.200 - .200 - .201 - .203 - .201 - .200 = 8.2008$

15-13 all carbon = $8.280 - .275 - .277 - .274 - .284 - .275 - .277 = 8.2774$

Reactivity $+13.25\frac{1}{16}$

all Support $-9.52\frac{1}{16}$

13-11 0

11-9 down 111.3 mils = $-30.05\frac{1}{16}$

Core = $0.0416\frac{1}{16}$ mil est. core

down 100.5 mils = $+4.18$

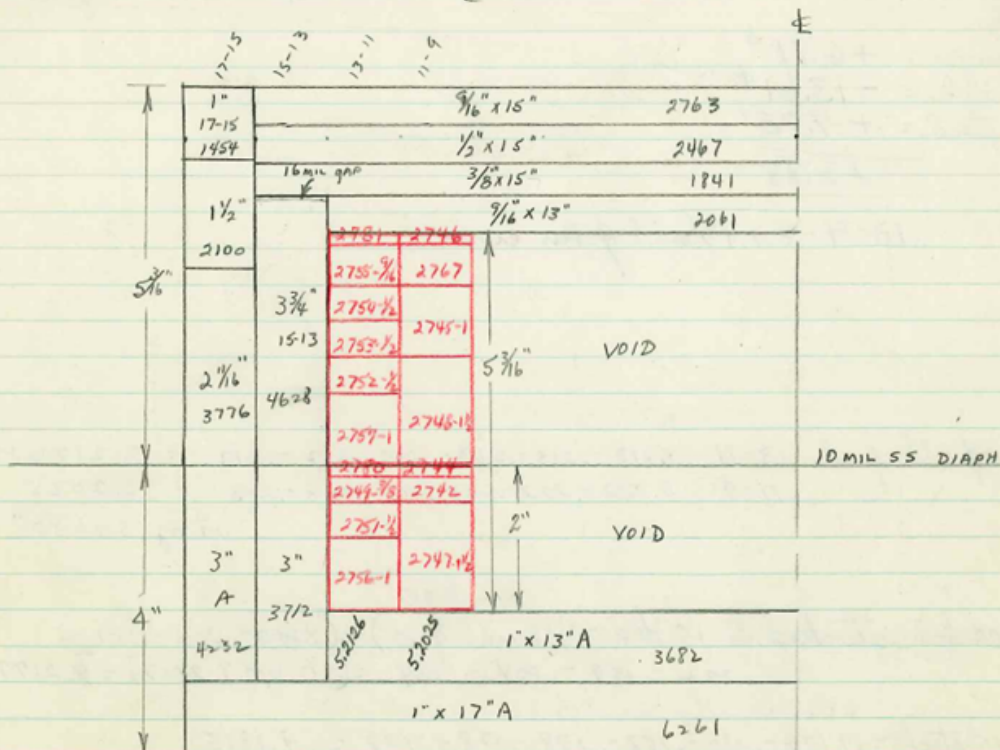
$-30.54\frac{1}{16}$

$-30.54\frac{1}{16} = 6.0940''$

$0 = 6.0940 + 0.0543 = 6.1483''$

13"-9" 2" C. REFLECTOR No Coll

33



MASS OF TOP GRAPHITE = 21090 gm TOTAL = 38.977 Kg
 BOTTOM = 17887 gm

MASS OF TOP FUEL = 67701 gm TOTAL = 110.166 Kg
 BOTTOM = 42465 gm

AVG. O.D. ALL FUEL (W.T.D) = 12.99604"

AVG. I.D. ALL FUEL (W.T.D) = 9.00191"

AVG Ht. ALL FUEL (W.T.D) = 5.20800"

FUEL VOLUME = 5889.38567 cm³

FUEL ρ = 18.70585 gm/cc

Vol of graphite not including 16 mil gap = 22923.41374 cm³
 graphite ρ = 1.70031 gm/cc

AVG REFL = 2.001"

13'-9" 2" C ref # No Core

clean Critical Nom. Ht: $5\frac{3}{16}" = +18.34^{\circ}$ reactivity

$$\begin{array}{r} \text{rings} = +6.71^{\circ} \\ \text{diaph} = -13.61^{\circ} \\ \text{S. stand} = +9.78^{\circ} \\ \hline +2.88 \end{array}$$

13-9 = 1.14/mil from curve

$$\begin{array}{r} \text{Ht. of all fuel } 13-11 = 5.212 - .213 - .213 - .212 - .212 - .212 = 5.2126 \\ 11-9 = 5.202 - .202 - .203 - .202 - .203 - .203 = 5.2025 \\ \text{wt. avg} = 5.2080" \end{array}$$

all carbon stacked to 15" dia ^{see chart} = (16 mil gap) + (9.200 - .202 - .201 - .202 - .199 - .204 - .204 = 0.016 + 9.2017) = 9.2177

$$(17-15) \text{ stack} = 9.179 - .180 - .187 - .178 - .178 - .187 = 9.1815$$

Carbon Bottom 17-15

15-13 =

13 DISC

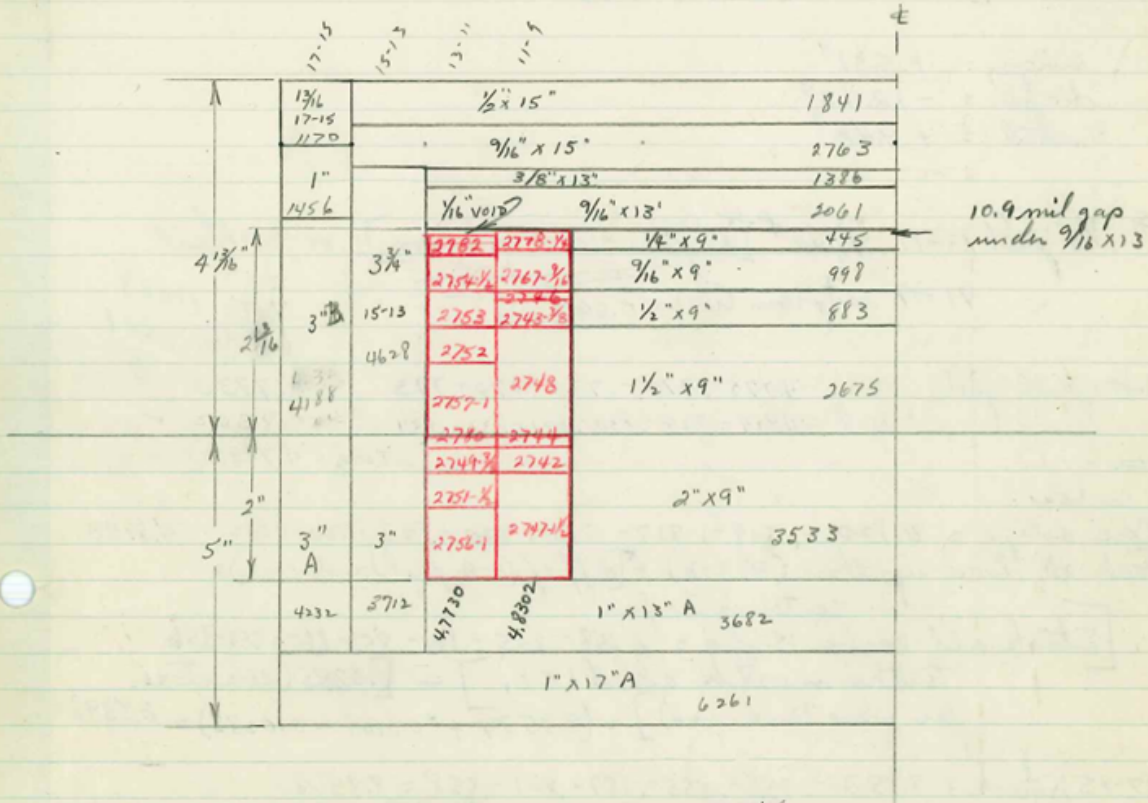
EVEN FUEL HT. = 5.2080"

SKYHOOK REACT. = +15.46⁺ (16 mil gap 15-13 carbon not considered)

$$O_{\text{react}} = 5.2080 - .0140 = \underline{5.1940"} \quad \text{"$$

13"-9" 2" C REFLECTOR + C CORE

B 36



MASS OF TOP FUEL = 59050 gm TOTAL = 101.515 Kg
 BOTTOM = 42465 gm

MASS OF TOP GRAPHITE = 24494 gm TOTAL = 45.914 gm Core = 8.534 Kg / TOTAL
 BOTTOM = 21420 gm

AVG. O.D. ALL FUEL (w't'd) = 12.99601" OD² = 168.89627
 AVG. I.D. ALL FUEL (w't'd) = 9.00215" ID² = 81.03870
 AVG. Ht. ALL FUEL (w't'd) =

FUEL VOL = 5426.57854 cm³
 FUEL ρ = 18.70699 gm/cc

graphite volume = 27428.55743 cm³
 ρ = 1.6739487 gm/cc

AVG REFL = 2.001"

13"-9" 2" Cref + Core.

Critical Nom. HT: $13-11 = 4\frac{3}{4}"$
 $11-9 = 4\frac{1}{2}"$

reactivity = +15.99%

rings = +5.31%
 diaph. = -12.43%
 S. stand = +9.48%

* $\frac{1}{16}"$ fuel 13-11 = 31.40% [est from 15-11 2" ref + core] or 0.502% mil
 11-9 est from Curve 0.69% mil

TOT = 1.1068
 with Core 1.201

HT of all fuel $13-11 = 4.775-.772-.773-.772-.773 = 4.7730"$
 $11-9 = 4.829-.829-.830-.831-.831-.831 = 4.8302"$
 wt. avg = 4.7990"

carbon
 HT Core only = 4.820-.819-.817-.818-.820-.823-.820-.818 = 4.8193
 stack all discs up thru ($\frac{3}{8} \times 13$) + [diff of (11-9 fuel) and core] =

center is higher
 \therefore [Stack all Carbon 15" dia = 8.858-.855-.861-.858-.860-.854-.856
 to this must be added (*) - 0.0285 (correction
 for piece thickness)] = (8.8574 + *0.0109 - 0.0285) = 8.8398

(17-15) stack = 8.853-.856-.855-.857-.861-.858 = 8.8566

Reactivity +15.99%
 all support -2.36%
 $13-11$ down 57.2 mils = -39.46%
 Core = 0.0942% mil \downarrow 46.3 = +4.36%
 -30.19% @ 4.7730"

all gaps considered

0 = 4.7730 + 0.0251 = 4.7981"

NOTE: (13-11) & (11-9) rings of fuel assumed near equal value per unit HT.

EVEN FUEL HT. = 4.8016"

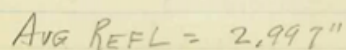
SKY HOOK REACT. = +13.63%

($\frac{1}{32}"$ carbon gap 13-9 (over fuel) &
 10.9 mil gap over core not considered)

* EVEN FUEL HT. = 4.8302"
 SKY HOOK React = +42.34%

(10.9 mil carbon gap over core not considered)

Pg 53



13-9 3' ref & No Core

Dom. Ht. Critical $4\frac{1}{4}" = +24.87\frac{1}{4}$ reactivity

Drumh. = $-9.79\frac{1}{4}$
Rings = $+6.07\frac{1}{4}$
S. Stand = $+8.15\frac{1}{4}$

Lower .013"

$\frac{1}{16}"$ 13-11 ring = $46.13\frac{1}{4}$ $0.7380\frac{1}{4}/\text{mil}$
 $\frac{1}{16}"$ 11-9 ring = $51.65\frac{1}{4}$ $0.826\frac{1}{4}$
 $19-17$ Carbon = $.0077\frac{1}{4}/\text{mil}$ (taken from Bq 13-1 15-11 3" ref)
 $1.5644\frac{1}{4}/\text{mil}$

Ht. of all fuel 13-11 = $4.268 - .268 - .269 - .269 - .270 - .269 = 4.2688"$
11-9 = $4.261 - .260 - .260 - .260 - .259 - .258 = 4.2597"$
avg = $4.2646"$

$\frac{1}{2} 113 = 0.4987$
15" dia = $10.265 - .261 - .265 - .260 - .262 - .266 = 10.2631$
17-15 ring = $10.266 - .270 - .273 - .265 - .264 - .267 = 10.2675$
19-17 ring = $10.192 - .194 - .190 - .194 - .194 - .198 - .196 = 10.1940 (-70)$

Reactivity = $+24.87\frac{1}{4}$

all support = $-4.43\frac{1}{4}$

13-11 = 0

11-9 up 9.1 mils = $+7.52\frac{1}{4}$

15 mil gap = $-1.0\frac{1}{4}$
 $+26.96\frac{1}{4}$

$+26.96\frac{1}{4} = 4.2688"$

$0 = 4.2688 - .0172 = 4.2516"$

Raise .0003"

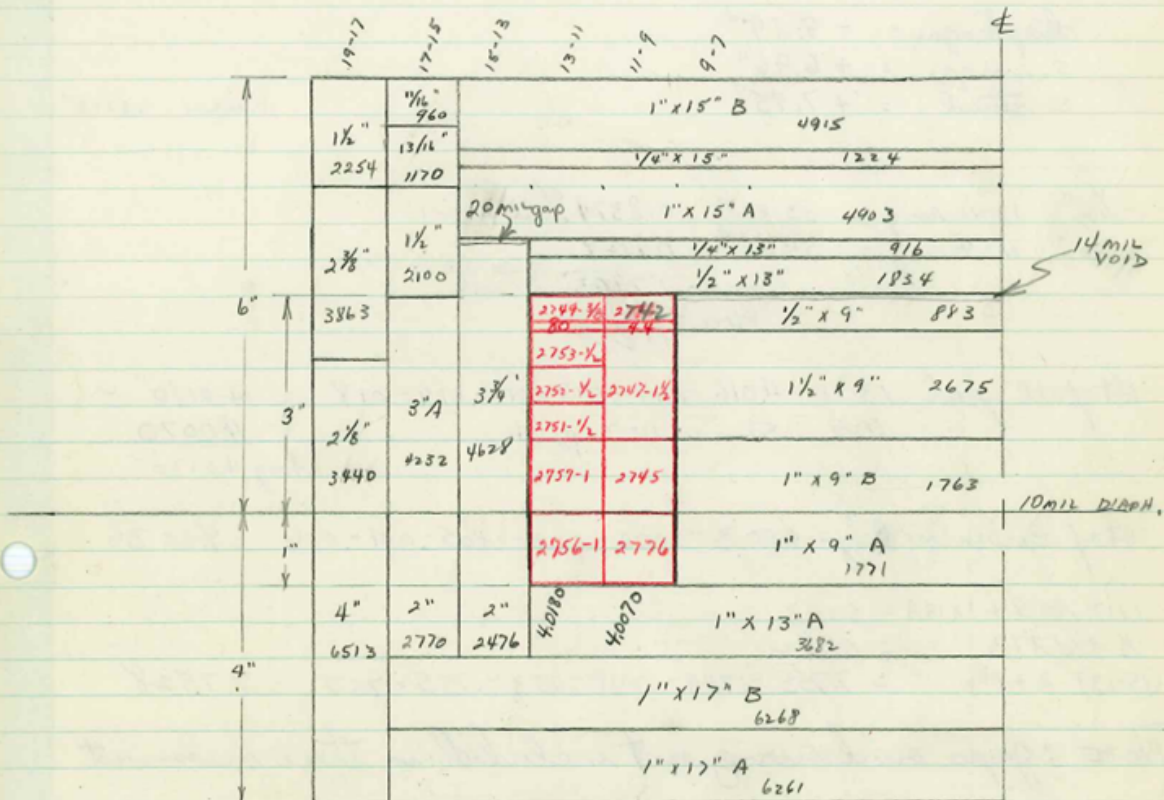
EVEN FUEL HT. = $4.2646"$

SKY Hook REACT. = $+21.00\frac{1}{4}$ (15 mil gap 15-13 Carbon not considered underdrawing)

correct flat fuel HT = $4.2519"$ ✓

13"-9" 3" GRAPHITE REFLECTOR + GRAPHITE CORE

Fig 54



MASS OF FUEL TOP = 63700 TOTAL 84.911 Kg
 BOTTOM = 2121 gm

MASS OF GRAPHITE TOP = 41760 gm TOTAL = 72.566 Kg OF THIS THE CORE = 7.092 Kg
 BOTTOM = 30806 gm

AVG. O.D. ALL FUEL (w't'd) = 12.99613"
 AVG. I.D. ALL FUEL (w't'd) = 9.00171"
 AVG. HT. ALL FUEL (w't'd) = 4.0120"

Vol. of graphite not incl. 20 or 14 mil gap = 43082.02634 cm³
 ρ = 1.68436 gm/cc

FUEL VOLUME = 45322135 cm³
 FUEL ρ = 18.71434 gm/cc

AVG REFL = 2.996"

13-9 3"ref + C core

Non. Ht. Critical 4" = -13.58⁺ reactivity

diaphragm = -9.29⁺
 5. rings = +6.96⁺
 5. stand = +7.75⁺

Raise .0106"

1/16" 13-11 ring: 52.34⁺ 0.8374⁺/mil
 1/16" 11-9 ring: 59.56⁺ 0.9529⁺
 1.7903⁺/mil
 flow = 1.8920

Ht of all fuel 13-11 = 4.016 - .017 - .019 - .019 - .019 - .018 = 4.0180" ✓
 11-9 = Same as 11-7 pg 64 = 4.0070
 wtag 4.0130"

Ht of Carbon Core Only = 4.003 - .002 - .005 - .005 - .001 - .006 = 4.0036

1x17 A+B + 1x13A = 3.003
 1/2 4 1/4 x 13 = 0.752
 (15-13) 2 + 3 3/4 = 7.755 - .749 - .748 - .753 - .755 - .757 = 7.7528

NOTE: gaps on drawing not included in these measurement

15" dia. all stacked = 10.015 - .005 - .007 - .012 - .007 - .010 = 10.0093
 17-15 ring = 10.015 - .012 - .010 - .011 - .004 - .009 - .010 = 10.0101
 19-17 ring = 10.025 - .017 - .012 - .017 - .027 - .030 = 10.0213

React = -13.58⁺
 all Support = -5.42⁺
 13-11 = 10.48⁺
 11-9 up 11.0 mil = +10.48⁺
 Core up 14.4 = +1.46⁺
 } = -7.06⁺ @ 4.0180"
 0 = 4.0180 + .0037 = 4.0217"

OK

EVEN FUEL HT. = 4.0120"

SICKY LOOK REACT. = -19.00⁺

(20 mil gap 15-13 Carbon see drawing
 not considered also 14 mil gap over core)

0 React HT = 4.0226" ✓

Core = .1017⁺/mil

4" GRAPHITE REFLECTOR & NO CORE

Pg-136

MASS OF FUEL = 77.595 gm
VOLUME = 4145.01903 cm³
 $\rho = 18.72005 \text{ gm/cc}$

MASS OF GRAPHITE = 99992 gm
VOLUME = 59533.117 cm³
 $\rho = 1.67958 \text{ gm/cc}$

AVG. O.D. ALL FUEL (w/IT'D) 12.99611" OD² = 168.89887
I.D. = 9.00178" ID² = 81.03204
21-19 OD Carbon = 20.99950" ——— 440,97900
AVG REPL = 3.999"

13-9 4" ref # No Core

Now. Wt. Critical = $3\frac{2}{32}$ "

reactivity = +28.14%

Rings = +5.15%
Diaphragm = -11.52%
5. Stand = +4.81%

Lower 0.0189"

19-17 graphite ring (121 mils) = 1.18% or .00975%/mil

1/32" fuel 13-11 = 23.13% 0.7401%/mil
11-9 = 26.33% 0.8425
1.5826

Avg = 1.582%/mil

Wt. of fuel : 13-11 = 3.668-.667-.666-.668-.668-.669 = 3.6676"
11-9 = Same as Pg 152 = 3.6625"

w + vol Avg = 3.6652"

Ht. of Carbon : 21-19 = 11.743-.750-.746-.759-.757-.754-.759-.747 = 11.7518"
19-17 = 11.688-.689-.689-.689-.693-.702-.704-.694 = 11.6931"
17-15 = 11.728-.724-.728-.738-.738-.731-.730 = 11.7310"
15-13 = 11.752-.748-.750-.766-.757-.772-.772 = 11.7595"
13 dia = Same as Pg 143 = 8.0127"

OK

corrected flat fuel height = 3.6463" ✓

Reactivity = +28.14%
Support (all) = +1.56%

+29.70 = 3.6652"

○ = 3.6652 - .0187 = 3.6465"

13"-9" 4" GRAPHITE REFLECTOR + GRAPHITE CORE

2140

11-10-8	21-19	19-17	17-15	15-13	13-11	11-9	
1 1/2		1 1/2	1 1/2				1/2 x 13 1834
2677	2 3/8	2098	1870				1 x 13 B 3760
	3 9/16						1 x 13 A 3682
5"		2	2				1 1/2 x 13 5509
		2770	2476				
	4"						
	66/3	3A	3"	82-7/8 78	52-7/8 43		1 x 9 B 1763
				49-7/8 42	51-1/2		
8827		4232	3712	54-1	47-1 1/2		1 1/2 x 9 2675
				56-1	45		
	1	1	1				1 x 9 A 1771
	1694	1456	1262				
3"				5530	3523		1 x 9 B 7838
							1 x 9 A 7828
5325							
							2 x 21 19263

10 mm DIAPH.

MASS OF FUEL = 74293 gm
 VOLUME = 3967.13665 cm³
 ρ = 18.72710 gm/cc

MASS OF GRAPHITE = 104648 gm
 VOLUME = 61260.27052 cm³
 ρ = 1.70825 gm/cc

AVG. O.D. ALL FUEL (WY'D) = 12.99592" O.D. = 168.89393
 I.D. = 9.00171" I.D. = 81.03078
 21-19 O.D. Carbon = 20.99956" 440.98152
 AVG REFL = 4.001"

13-9 4" ref + Core

Norm. Wt. Critical = $3\frac{1}{2}$ "

reactivity = + 4.64%

Rings = + 4.79%
Diaphragm = -10.52%
S. Stand = + 4.57%

Lower 0.0076"

$\frac{1}{32}$ " fuel 13-11 = 29.28% 0.9369%/mil
11-9 = 36.40% 1.1648%

wt vol Avg = 2.101%/mil

add 319 mils graphite 19-17 ring = 1.95% or .0061%/mil
+ Cor $\frac{2.101}{.0061} = 2.186\%$

Wt of fuel = 13-11 = 3.513-.513-.510-.513-.514-.515 = 3.5130"
11-9 = 3.502-.502-.502-.504-.502-.502 = 3.5023"

wt vol Avg = 3.5081"

Wt of Carbon = 21-19 = 11.492-.494-.499-.508-.507-.503-.497-.492 = 11.4990"
19-17 = 11.375-.378-.373-.375-.375-.370-.371 = 11.3738%
17-15 = 11.503-.506-.513-.508-.508-.504-.513 = 11.5078"
15-13 = 11.538-.543-.544-.538-.537-.532-.539 = 11.5378%
13 dia. Same as Pg 143 = 8.0127"
Core = 3.505-.506-.504-.505-.504-.508-.505 = 3.5048"

corrected flat fuel height = 3.4995"
Core Value Δ .088%/mil

React = + 4.64
all Support = + 1.16
13-9 = 0

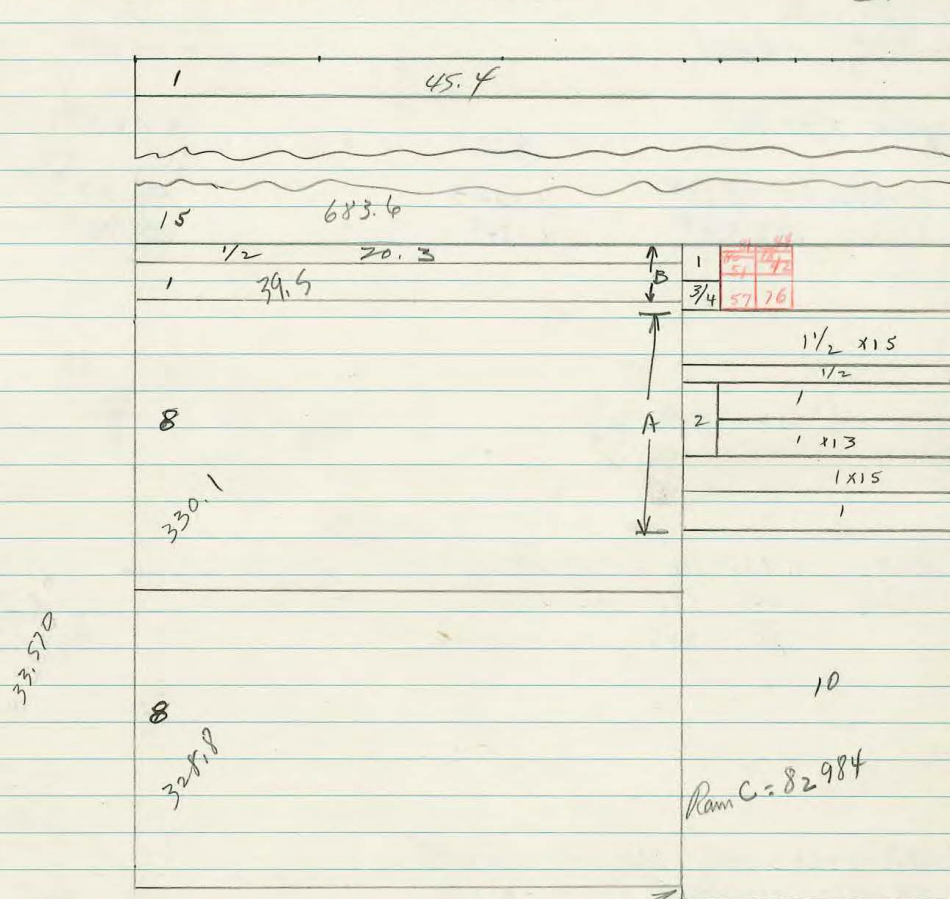
Core hp 3.3 = + 0.29

+ 6.09 = 3.5081"

0 = 3.5081 - 0.027 = 3.5054

NO CORE
+ CORE

197
4-200



No Core

 $\frac{1}{4}$ m

+ Core
same

$$Vol = 1985.3615 \text{ cm}^3$$

$\rho = 18.7275 \text{ gm/cc}$

$$(OD)^2 = 168.89549$$

81.034743

Mass C = 1530684 gm

$$V_{\text{sl. C}} = 874927 \text{ cm}^3 - 3821 \text{ cm}^3 = 871106 \text{ cm}^3$$

$\rho = 1.757 \text{ gm/cc}$

1533782 gm

872 934 cm³

1.757 gm/cc

Avg Refl = 16.001"

13-9 #16" C ref
No Core

Nom. Wt. = $1\frac{3}{4}"$
reactivity: -4.43%

Supports = $+1.96\%$

fuel 11-9 ($\frac{1}{32}"$) = 38.51%
13-11 = 38.59%

$\frac{\text{fuel}}{\text{fuel}}$
1.2323
1.2348

Core

$1\frac{3}{4}"$
 $+30.88\%$

$+1.27\%$

46.87%
 55.70%

$\frac{\text{fuel}}{\text{fuel}}$
1.5000
1.7824

35" x 15" x $\frac{1}{2}"$ C: $+9.12\%$

fuel 13-11 = $1.755, .756, .755, .755, .755, .755 = 1.7551$
11-9 = $1.757, .757, .756, .757, .757, .756 > 1.7566$

Same 1.7551
Same 1.7566
avg = 1.7557

A = $6.017 - .012 - .005 - .005 - .010 = 6.0098$
B = $1.756 - .750 - .749 - .756 - .757 = 1.7536$

1.7551

1.756
- 1.7536

1.7424

[No Core &
+ Core]

[illegible]

+ Core

40592 gm

$$2162.1503 \text{ cm}^3$$

18.7739 gm/cc

$$12.99574 \quad (2) = 168.88925$$

11,00251 (2) = 121,05522

Mass_g = 1623195 gms

$V_{\text{ol}} = 926353 \text{ cm}^3$

$\rho = 1.752 \text{ gm/cc}$

Aug. Ref 1 = 15,992"

13-11 #16" C. ref.

Dom. WT = $3\frac{3}{4}$ "

reactivity = +30.36¢

Supports = 2.19¢

$\frac{1}{32}$ " fuel : 42.27¢

1.352¢/ml

measured fuel ht 13-11 =

$$3.770 - .770 - .770 - .770 = 3.7700$$

A = Same as 4-200

$$= 6.0098"$$

B = Look up

$$= 3.7533"$$

$$C = 3.507 - .513 - .512 - .514 - \cancel{.515} = 3.5115"$$

13-11 #16" C. ref + Core

$3\frac{1}{2}$ "

+14.24¢

2.19¢

$$3.512 - \overset{.512}{.512} - \overset{.512}{.512} - \overset{.512}{.512} = 3.5120$$

$$\begin{array}{r} 8 \\ 3.770 \\ - .770 \\ \hline 3.749 \end{array}$$

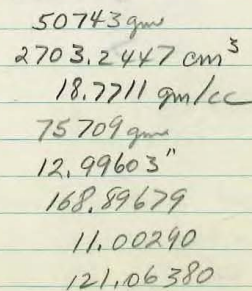
$$\begin{array}{r} 3.512 \\ - .513 \\ \hline 3.503 \end{array}$$

Note added by Jim
5/2023

C-15-13 = 3.75 must
have been Replaced

C-15-13-35

Pg 4-91



13-11 Ring Only $\pm 11''$ w/c

No Core

"Clean" Critical Num. Wt. = $4\frac{15}{16}''^*$
 reactivity = $+17.50\%$
 $\frac{1}{32}''$ fuel value = 25.19%
 all supports value = 5.75%

$(13.00) \times \frac{1}{32} C = 2.75\%$
 $.525''$ Carbon on $11\frac{1}{16}''$ TOP = 29.95%
 $\therefore \frac{1}{16}'' C$ TOP = 3.57%
 $(35-15) \times 0.525$ —

Wt of fuel 13-11 =
 $4.955 - .955 - .955 - .956 - .956 - .955 - .955 = 4.9550$

A $11.026 - .026 - .025 - .024 = 11.0252$
 B $17.062 - .063 - .057 - .067 = 17.0622$
 C $0.814 - .815 - .818 - .813 = 0.8150$

4.955
 4.941

*** Void $\frac{1}{32}''$ over 15-13 carbon

* HAS EXTRA $\frac{1}{16}'' C$ on TOP (35"OD)

** SHY $\frac{1}{16}'' C$ on TOP (35"OD) also $\frac{1}{16}''$ excess

+ Core

$4\frac{3}{8}''^* \times \frac{1}{16}''$
 -7.06%
 $26.32\% \times \frac{1}{16}''$
 5.41%

30.07%

13.39%

$4.391 - .391 - .391 - .391 - .391 = 4.3910$

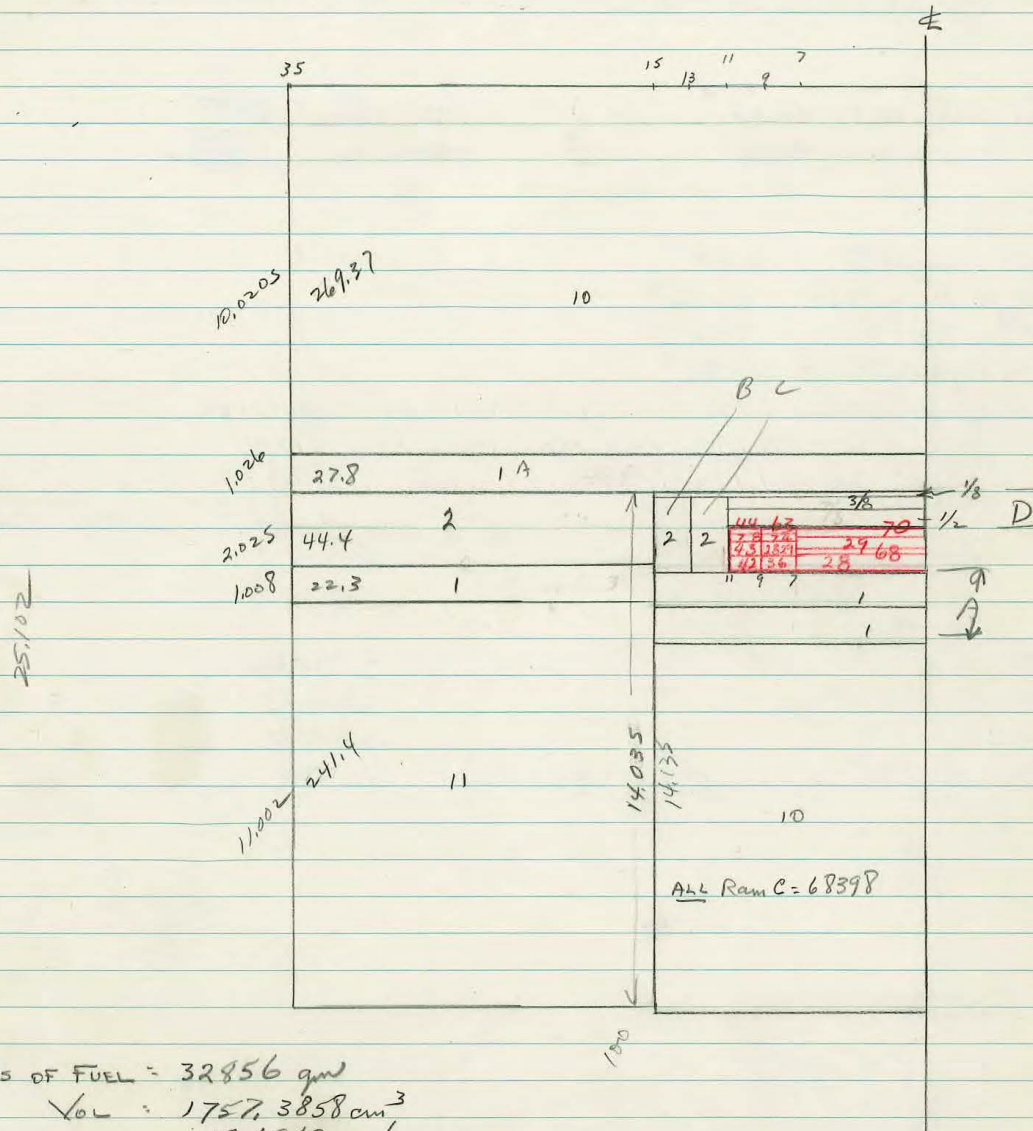
A ← Same = 11.0252
 B: (+A) = $5.332 - .332 - .335 - .332 = 5.3330$

Core Only: $4.378 - .383 - .380 - .380 = 4.3802$
 C: $13 \times \frac{1}{8}''$ lock up = 0.1240

4.391
 4.406

11" DIA CYL. (SOLID) ; 12" GRAPHITE REF.

4-112



MASS OF FUEL = 32856 gm
 Vol = 1757.3858 cm³
 ρ = 18.6959 gm/cc
 Avg OD = 10.99641"
 (OD)² = 120.92103

Mass C = 673.668 Kg
 Vol = 394010 cm³
 ρ = 1.709 gm/cc

Avg Refl = 12.015"

11" dia. cyl. & 12" C. ref.

Mem. Ht. Critical ~ $1\frac{1}{8}$ "
reactivity = -3.52%

$\frac{1}{32}$ " fuel 11-9 = 47.47%

9-7 = 49.98%

?

7 dia: Not measurable

~~7.5190~~ ~~mil~~ ~~1.15~~
~~7.5893~~ ~~mil~~ ~~1.86~~

↑

all supports = 6.34%

35-15 Ring, 525" = 10.52%

15 dia Top $\frac{1}{4}$ " = 7.02%

ADD $\frac{1}{2}$ " more 15 dia = 11.81%

10200 / mil 0.12

Ht. of fuel 11-9: 1.130-.130-.130-.131-.131-.131-.131

= 1.1305

9-7: 1.130-.130-.130-.130-.130-.130

= 1.1300

7 dia: 1.128-.127-.128-.128-.128-.127-.128

= 1.1277

avg = 1.129 ✓

A = "A" 4-12%

= 2.0022

B = look up

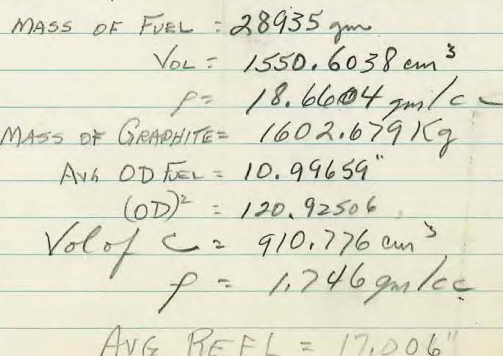
= 2.0043

C = " "

= 2.0020

D 1.002-.002-.001-.001-.002 = 1.0026

B9 4-141



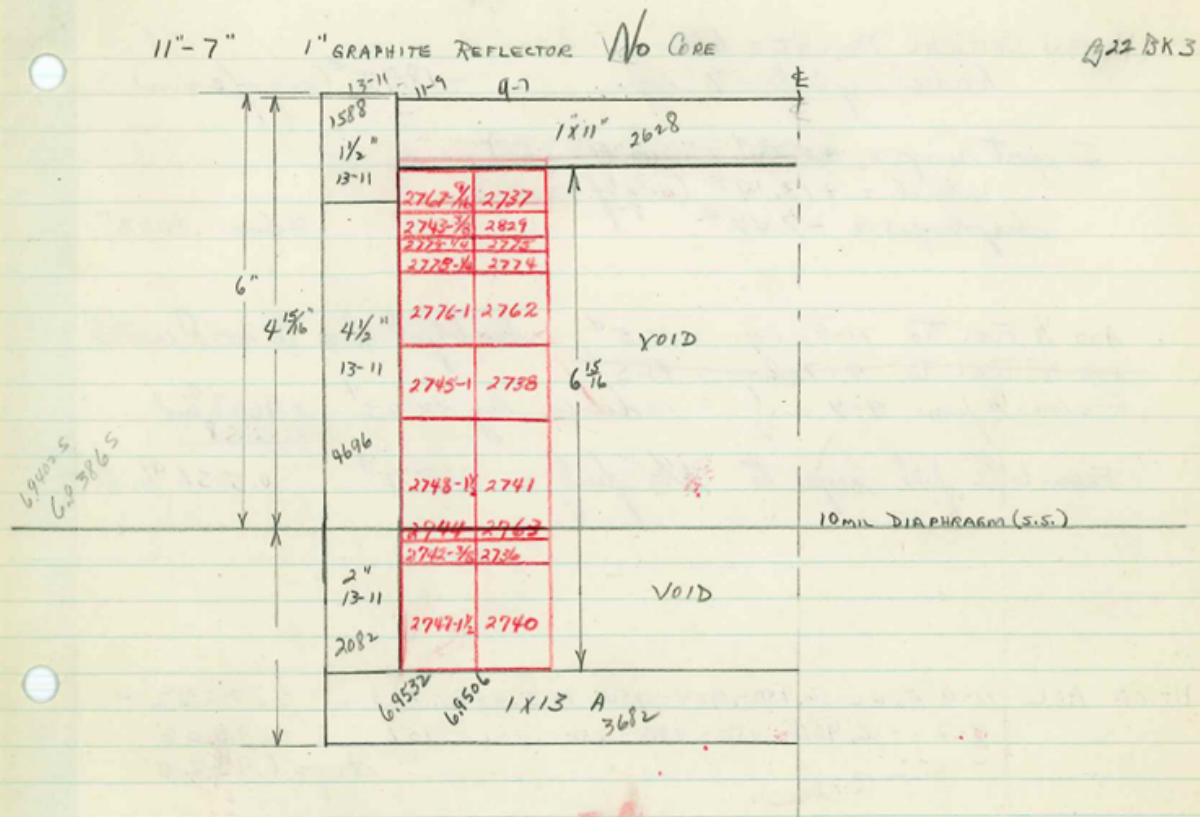
11" diacyl # 17" C.ry.

Dem Ht critical = 11-9 & 7" dia = 1"
9-7 = $\frac{3}{32}$ "

Reactivity = Snt. but close
Supports = est 2.0¢
fuel value ?

Wt. of 11-9 = 1.004 - .004 - .005 - .005 - .005 - .006 = 1.0048"
9-7 = 0.973 - .973 - .973 - .973 - .972 - .973 - .974 = 0.9730"
7dia = 1.004 - .005 - .006 - .005 - .004 - .004 - .005 = 1.0047"
avg = .9963

A = 3.505 - .507 - .507 - .508 = 3.5072"
B = 7.016 - .017 - .016 - .015 = 7.0160
C = 4.503 - .505 - .505 - .503 = 4.2776
D = Look up = 4.5000



MASS OF TOP GRAPHITE = 8912 gm TOTAL = 14.676 Kg
 BOTTOM = 5764 gm
 85658 120,350
 MASS OF TOP FUEL = 64446 gm TOTAL = 99.138 Kg
 BOTTOM = 34692 gm

AVG. O.D. ALL FUEL (WTD) = 10.99673" OD² = 120.92807
 AVG I.D. ALL FUEL (WTD) = 7.00292" ID² = 49.04088
 AVG HT. ALL FUEL (WTD):

FUEL VOLUME = 6432.18690 cm³
 FUEL ρ = 18.7106 gm/cc

graphite vol = 8695.03454 cm³
 ρ = 1.68785 gm/cc

AVG REFL = 1.000"

11-7 1" Cnf \pm Void Core

CLEAN CRITICAL Nems. Ht. = $6\frac{5}{16}$ "

Radial reflector = 7" high = -18.72° (avg of 2 runs)

Support rings = $+5.28^\circ$ (avg of 2 runs)

stand = $+13.19^\circ$ (avg of 2 runs)

diaphragm = -7.44°

Raise .0608"

ADD $\frac{1}{8}$ " FUEL TO 11-9 ring = 20.5° doubtful due to void created

~~ADD $\frac{1}{8}$ " FUEL TO 9-7 ring = 45.5°~~

Remove $\frac{1}{8}$ " from 9-7 ring = reduces by 33.73° $\frac{0.2698^\circ/\text{mil}}{11-9 = .2358}$

From $6\frac{5}{16}$ " fuel up to $7\frac{1}{16}$ " fuel = $+63.2^\circ$ $\frac{0.5056^\circ/\text{mil}}{\frac{1}{8}"}$

Ht OF ALL 11-9 FUEL = $6.950 - .954 - .954 - .953 - .955 - .953 = 6.9532$ ✓

9-7 = $6.950 - .950 - .950 - .950 - .951 - .951 = 6.9506$

avg = 6.9520 "

ALL(C) 13-11 = $9.014 - .014 - .014 - .014 - .011 - .014 = 9.0135$

1"X11" DISC = 1.002

EVEN FUEL HEIGHT = 6.9520 "

SKY HOOK REACTIVITY = -29.75° (includes extra $\frac{1}{16}$ graphite on 13-11 ring)

0 React $11^\circ = 7.0128$ ✓

REACT = -18.72°

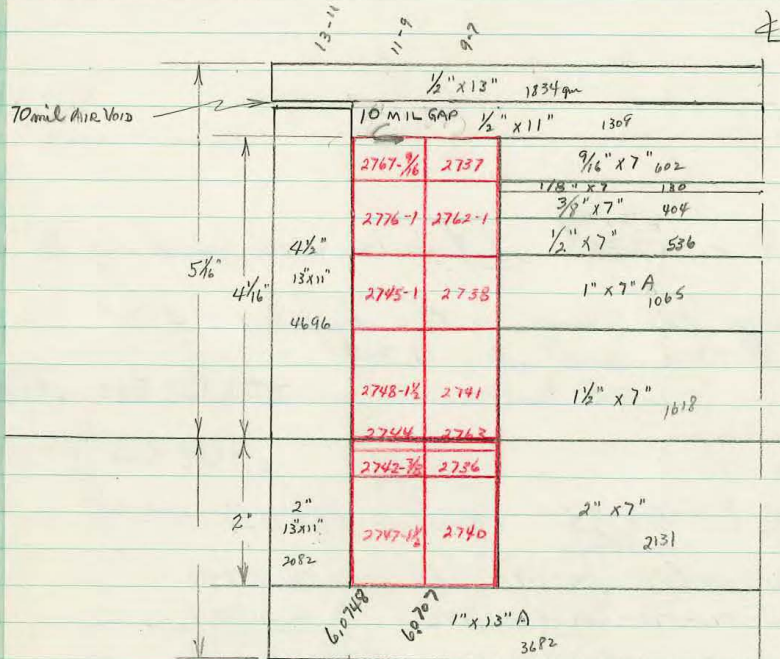
ALL SUPPORT = -11.03°

$-29.75 = 6.9520$

0 = $6.9520 + .0589 = 7.0109$ "

11"-7" 1" GRAPHITE REFLECTOR + GRAPHITE CORE

Run 37F B 289



MASS OF TOP GRAPHITE = 12244 gm TOTAL = 20.139 kg
 BOTTOM = 7885

MASS OF TOP FUEL = 70467 gm TOTAL = 105.159 kg
 BOTTOM = 34692

AVG O.D. ALL FUEL (W.T.D) = 10.99674" $OD^2 = 120.92829$
 AVG I.D. ALL FUEL (W.T.D) = 7.00285" $ID^2 = 49.03990$
 AVG H. ALL FUEL (W.T.D) =

FUEL VOLUME = 5618.94825 cm³
 FUEL ρ = 18.71506 gm/cc

graphite vol = 11904.73979 cm³
 ρ = 1.69167 gm/cc

AVG REFL = 1.000"

11-7" 1" C ref. + C Core

Dom. Ht. Critical $6\frac{1}{16}" = -4.45"$

rings = $6.81"$
diaph = $-8.15"$
s. stand = $10.28"$

Raise $.0163"$

add $\frac{1}{16}"$ to 11-9 = $17.36"$ but carbon was raised by $\frac{1}{16}"$.

Now interchange the 2 rings = the difference = $4.71"$
Add $\frac{1}{16}"$ C. to core and it = $9.71"$

75 mil, 7828

Total $\frac{1}{16}"$ F&C = .8855

11-9 = 17.36

9-7 = 22.07

$\frac{1}{16}"$ total fuel + $\frac{1}{16}"$ C = 58.95

$\frac{1}{16}"$ 0.7878 mil
w/o C = 49.24 ← used

HT ALL FUEL 11-9: $6.075, .075, .075, .074, .075, .075$ = $6.0748"$

9-7: $6.072, .071, .070, .069, .070, .072$ = 6.0707

w/avg $6.0729"$

HT of all Core only = 6.085

HT of all Carbon DIA. 13" = $8.086, .087, .084, .084, .087, .084, .084$ = 8.0851

13-11 = $.030$ mil est

EVEN FUEL HT. = $6.0729"$

SKY Hook REACTIVITY = -12.89% (includes a 70 mil gap ^{Carbon} 13-11 see drawing)
(also 10 mil gap over fuel)

0 React 14 = $6.0892"$ ✓

13-11 $\uparrow 70 = +2.1$

REACT = -8.45

ALL SUPPORT = -8.44

11-9 $\uparrow 10.2 = +8.33$

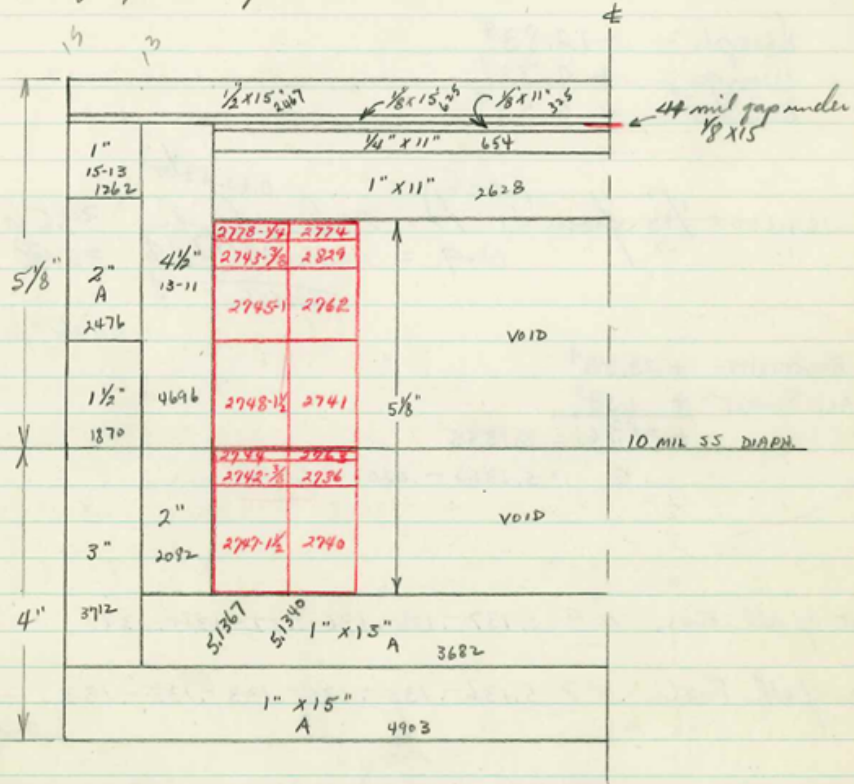
9-7 $\uparrow 14.3 =$

Core (.1028 mil) = 0

$-2.46 = 6.085"$
 $0 = 6.085 + .0027 = 6.0877"$

11"-7" 2" graphite reflector & No Core

Run 1c Pg 24



MASS OF TOP GRAPHITE = 17003 gm TOTAL = 31.382 Kg
 BOTTOM = 14379 gm

MASS OF TOP FUEL : 54.224 gm TOTAL = 88.916 Kg
 BOTTOM = 34692 gm

AVG. O.D. ALL FUEL (w't'd) = 10.99685"

AVG. I.D. ALL FUEL (w't'd) = 7.00285"

AVG. HT. ALL FUEL (w't'd) = 5.135499"

FUEL VOLUME = 4751.71751 cm³

FUEL ρ = 18.71239 gm/cc

Vol. of graphite (not incl) 44 mil gap = 18563.08641

ρ = 1.69055 gm/cc

AVG REFL = 2.000"

11'-7" 2" ref \neq No Core

clean critical diam. $1/4" = 5\frac{1}{8}" = +23.38^\circ$ reactivity

Graph = -12.83°

Rings: + 4.72 \$

S. Stand: + 6.534

remove $\frac{1}{16}$ " from (9-7) = reduced by $0.6249 \frac{\text{¢}}{\text{mil}}$ 39.06 ¢ (reference to clean
 " " " 11-9 = reduced by $0.5757 \frac{\text{¢}}{\text{mil}}$ 35.98 ¢ (" " ")
1.2006
 1.2006 ¢ / mil

REACTIVITY: +23,38⁺

ALL SUPPORT: + 1.58¢

$$+ 24.96 = 5.1355''$$
$$O \approx 5.1355 - .0207 = 5.1148''$$

Wt. of all FUEL 11-9 = 5.137 - .136 - .136 - .137 - .138 - .137 = 5.1367" ✓

Ht. of all FUEL 9-7: 5.136 - 135 - 135 - 133 - 133 - 133 = 5.1340
avg = 5.1355"

15-13 tuning up to ($1/8 \times 15$ disc) = 8.560 - .558 - .556 - .556 - .557 - .558 = 8.5595

$$13-11 \text{ mid} = 8.517 - 512 - 509 - 509 - 501 - 513 = 8.5101$$

add Disc $\frac{1}{8} \times \frac{1}{2} \times 15$ on top of 15-13 ring = 9.194-.195-.1922
 .193-.196-.195-.194 = 9.1941

$$(1 \frac{1}{4} \div \frac{1}{8} \times 11) = 1.378 - .379 - .378 - .379 - .379 = 1.3786$$

≈ 41 mil gap under $(\frac{1}{8} \times 15)$ from 13" dia. inward.

EVEN FUEL WT. = 5.1354"

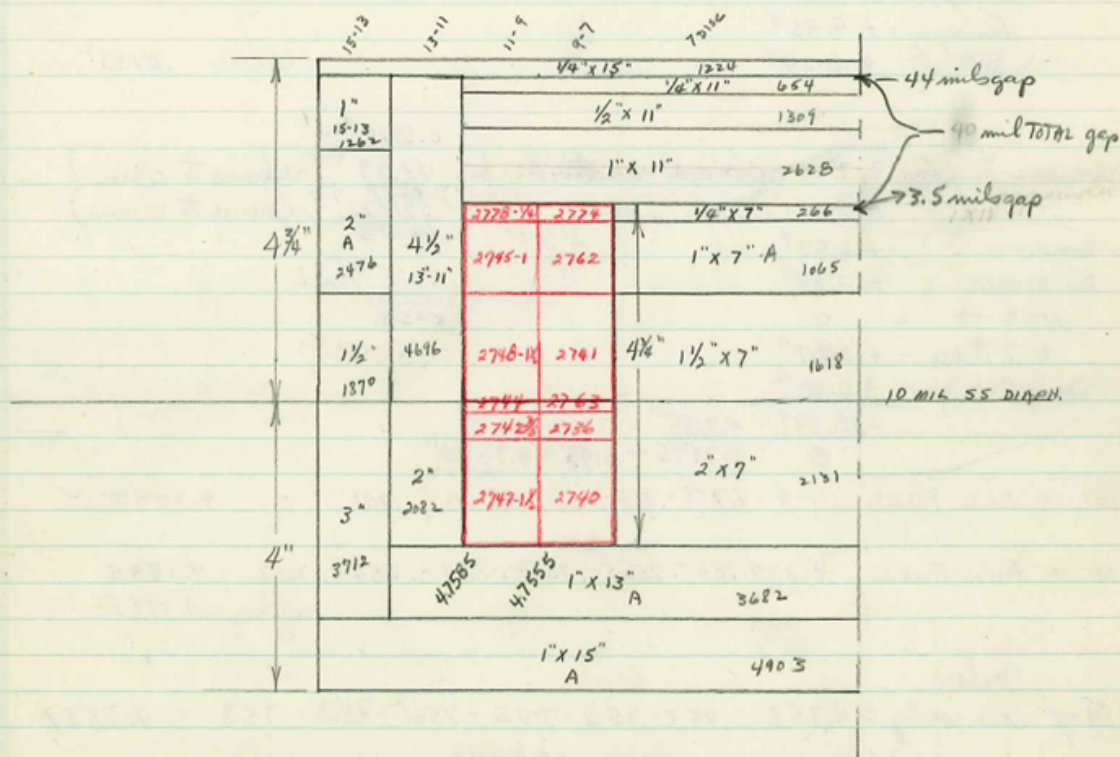
EVEN FUEL HT. = 5.1354"
SKYHOOK REACTIVITY = +24.96% (44 mil carbon gap over 1/2 x 11 dia not considered)
O React HT = 5.1147" ✓

0 React H^+ = 5.1147" ✓

11" - 7"

2" graphite reflector + graphite Core

224



MASS OF TOP GRAPHITE = 19068 gm TOTAL = 35.578 Kg OF THIS THE CORE IS = 5.080 Kg
 BOTTOM : 16510 gm

MASS OF TOP FUEL = 47708 gm TOTAL = 82.400 Kg
 BOTTOM : 34692 gm

AVG O.D. ALL FUEL (w.t'd) = 10.99687"
 AVG I.D. ALL FUEL (w.t'd) = 7.00283"
 AVG HT. ALL FUEL (w.t'd) = 4.95716"

522543975 / 475175
 3326484879 / 47502

FUEL VOLUME = 4401.16968 cm³
 FUEL ρ = 18.72229 gm/cc

Vol. of graphite net incl gaps = 21048.44479 cm³
 ρ = 1.690291 gm/cc

AVG REFL = 1.999"

11"-7" 2'ref + C Core

Clean Critical Nom. Ht = $4\frac{3}{4}" = +16.03\%$

Diaph = -12.88%
Rings = +4.35%
S. Stand = +6.24%

Lower .0133"

remove $\frac{1}{16}"$ from 9-7 = reduced reactivity by 0.6926%
" " " 11-9 = " " 43.29% (reference to clean)
" " " 11-9 = " " 59.42% (reference to clean)
" " " 11-9 = " " 13313

REACTIVITY = +16.03%

AKA SUPPORTS = +2.29%

11-9 → = 0

9-7 ↑ 3.0 = +2.07%

Core ↑ 4.8 = +0.50%

+20.89% = 4.7585"

0 = 4.7585 - .0145 = 4.7440"

Core = $\frac{1.3313}{1.1041} \%$ / mil
1.1955

Ht. OF ALL FUEL 11-9 = 4.758 - .758 - .758 - .759 - .760 - .758 = 4.7585" ✓

Ht. OF ALL FUEL 9-7 = 4.756 - .7565 - .756 - .754 - .756 - .757 = 4.7555
wt avg = 4.7571"

Carbon

Ht of Core only = 4.753 - .753 - .753 - .755 - .756 - .753 - .753 = 4.7537

stack all discs thru $\frac{1}{4}"$ = $(4.7585 - \text{Core Only}) + [8.513 - .510 - .514 - .516 - .517 - .515] = (8.514 + .0048) = 8.5189$

13-11 ring = 8.517 - .512 - .509 - .509 - .501 - .513 = 8.5101

all carbon on, with top $\frac{1}{4} \times 15$ resting on the 15-13 ring
∴ measure all top (thereby giving us the 15-13 ring)
→ 8.814 - .814 - .813 - .810 - .812 - .814 - .814 = 8.8130 (+56)

EVEN FUEL HT. = 4.7571"

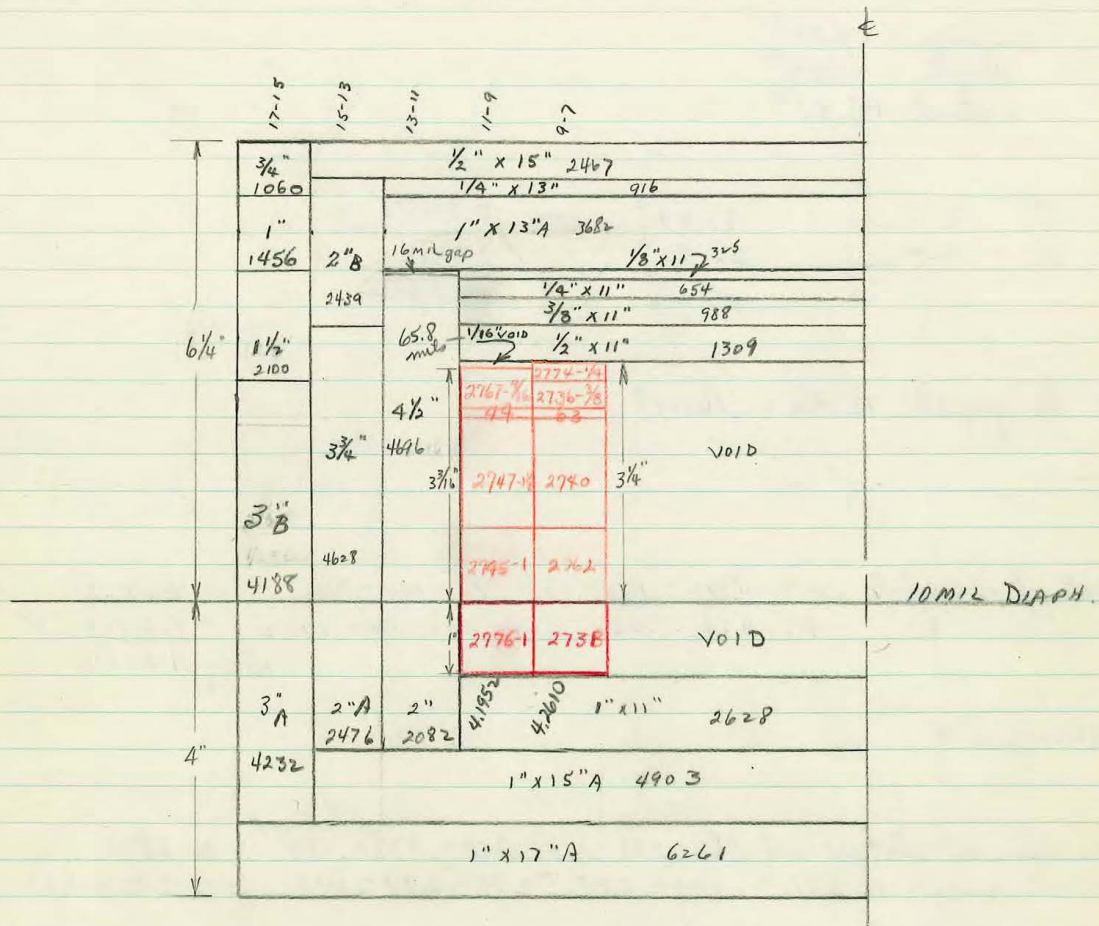
SKY HOOK REACT. = +18.32%

(44 mil & 3.5 mil carbon gaps (see drawing))
not considered

0 React Ht = 4.7434" ✓

11'-7" 3" GRAPHITE REFLECTOR & NO CORE

264



MASS OF FUEL TOP = 55 752 gm TOTAL = 73.106 Kg
 BOTTOM = 17 354 gm

MASS OF GRAPHITE TOP = 30 908 TOTAL = 53.490 Kg
 BOTTOM = 22 582 gm

AVG. O.D. ALL FUEL (W.T.D) = 10.99650"
 AVG. I.D. ALL FUEL (W.T.D) = 7.00316"
 AVG. HT. ALL FUEL (W.T.D) =

OD² = 120.92301
 ID² = 49.04424

FUEL VOL = 3908.10107 cm³
 FUEL ρ = 18.706271 gm/cc
 AVG REFL = 2.999"

Graphite volume = 31400.18957 cm³
 ρ = 1.703503 gm/cc

11-7 3" Cref & No Core

Nom. Ht Critical = (11-9) = 4³/₁₆" & (9-7) = 4¹/₄" → +1.04¢ reactivity

ring = +4.27¢
graph. = -9.54¢
stand. = +6.51¢

OK

¹/₁₆" 11-9 ring = 46.24¢ or 0.7398¢/mil
¹/₁₆" 9-7 ring = 52.40¢
0.8384
1.5782

Top ¹/₁₆" graphite 15" dia = 16.11¢

Ht. of all fuel 11-9 = 4.194, .197, .196, .195, .194, .195 = 4.1952"
9-7 = 4.262, .262, .261, .259, .260, .262 = 4.2610 ✓
wt avg = 4.2244"

4.2610 fuel +

15 dia. all stacked = 10.280, .281, .280, .280, .279, .280 = 10.2800 (+56)

17-15 ring = 10.291, .296, .297, .295, .297, .296 = 10.2953 (+71)

(¹/₂ × ³/₈ × ¹/₄ × 11) = 1.254, .256, .253, .255, .256, .258 = 1.2553

EVEN FUEL HT. = 4.2610"
SKYHOOK REACTIVITY = +48.47¢

REACT = +1.04¢

ALL SUPPORT = -0.20

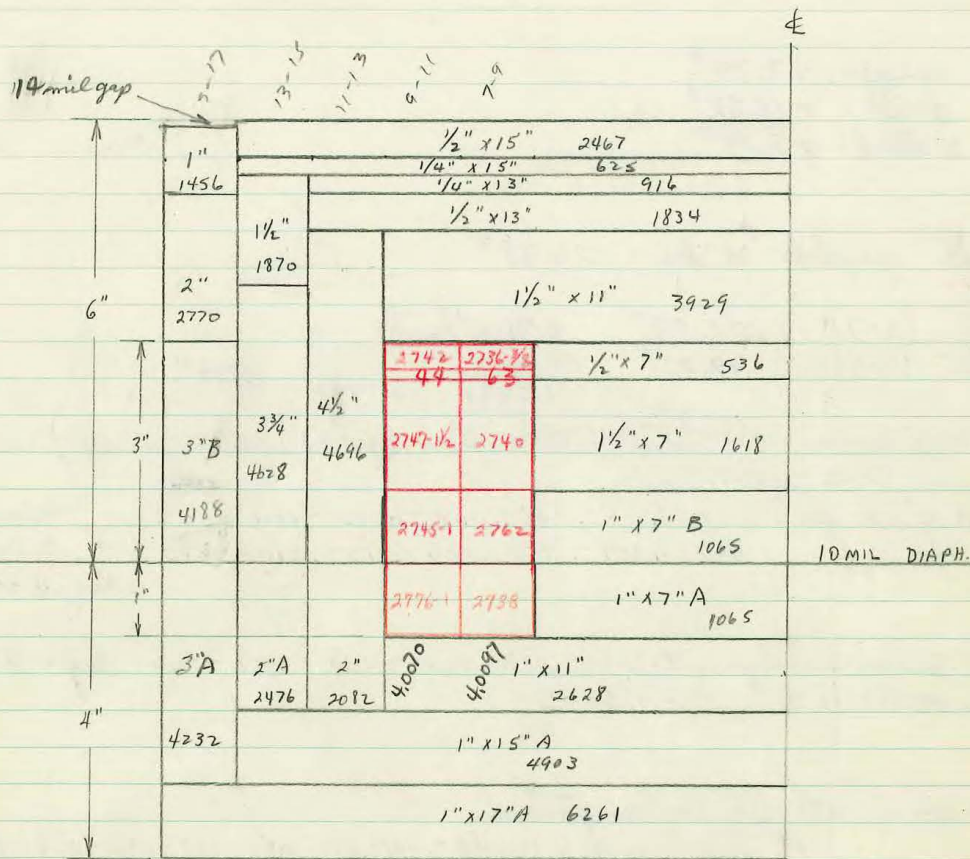
+0.84 = 4.2244"

0 = 4.2244 - .0005 = 4.2239"

0 React HT = 4.2244" ✓

11"-7" 3" GRAPHITE REFLECTOR + GRAPHITE CORE

Pg 64



MASS OF FUEL TOP = 52029 gm TOTAL = 69.383 Kg
 BOTTOM = 17354 gm

MASS OF GRAPHITE TOP = 32598 gm TOTAL = 56.245 Kg OF THIS, Core = 4.284 Kg
 BOTTOM = 23647 gm

AVG. O.D. ALL FUEL (W.T'D): 10.99657"
 AVG. I.D. ALL FUEL (W.T'D): 7.00317"
 AVG. H. ALL FUEL (W.T'D): 4.00820"

VOL of TOTAL = 33641.24758 cm³
 ρ = 1.67190 gm/cc

FUEL VOLUME = 3708.11356 cm³
 FUEL ρ = 18.71113 gm/cc
 AVG REFL = 3.000"

11-7 3"ref + Core

Non Ht. Critical = 4" = -20.65⁺

rings: +7.74⁺
diaph: -10.82⁺
5. stand: +7.39⁺

Raise .0161"

1/8" graphite 15" dia = 26.38⁺

1/16" (9-7) = 52.59⁺ 0.8414⁺/mil
1/16" (11-9) = 44.21⁺ 0.7073

17-15 Carbon: .0027⁺ mil (taken from (9 131) 15-11 3"ref)
Core = .0077⁺/mil

Ht. of all fuel 11-9: 4.008-.008-.008-.0065-.006-.005 = 4.0070"
9-7: 4.009-.010-.009-.010-.010-.010 = 4.0097"
wt avg = 4.0082"

Ht. of Carbon Core only = 4.006-.007-.0011-.008-.007-.006 Avg = 4.0075"
Core + (1 1/2 x 11) = +1.5025

Measure with all Carbon stacked

15" dia. Area h = 10.040-.041-.042-.043-.037-.036-.036 = 10.0392
17-15 ring = 10.052-.048-.056-.051-.050-.057 = 10.0523

OK

EVEN FUEL HT. = 4.0082"
SICK Hook React. = -24.96⁺

0 React Ht = 4.0243" ✓

React. = -20.65⁺
AHL SUPPLY = -4.31⁺
11-9 ↑ 2.7 = +1.90⁺
9-7 → = 0
Core ↑ 2.2 = +0.01⁺
17-15 ↑ 14 = +0.10⁺
-22.95⁺ = 4.0097"
0 = 4.0097 + 0.0147 = 4.0244"

$\cong P_9 152$

MASS OF FUEL: 63427 gm
VOLUME: 3392.02059 cm³
 $\rho = 18.69888 \text{ gm/cc}$

MASS OF GRAPHITE: 81407 am

VOLUME: 48201.48740 cm³

$\rho = 1.68888 \text{ gm/cc}$

AVG REFL = 4.002"

AVG. O.D. ALL FUEL (w't'd) = 10.99678"

$$CD^2 = 120.92917$$

I.D.: 7.00284"

ID: 49,03976

19.17 OD Carbon - 18.99662"

— 360,87176

11-7 4" ref #Nore

Norm. Ht. Critical = $3\frac{2}{3}$

reactivity = -4.38°

Rings = $+4.38^\circ$
Diaphragm = -11.01°
S. Stand = $+5.01^\circ$

Raise 0.0014"

(-) $\frac{1}{32}$ " fuel 11-9 = 28.34° $0.9068^\circ/\text{mil}$ $\rightarrow -2.0719$
(-) 9-7 = 36.41° 1.1651 add 9-7 = 16.05° (?)

Aug = $2.014^\circ/\text{mil}$

add 238^{mil} graphite on 15-13 ring = $+5.83^\circ$ $0.245^\circ/\text{mil}$

Ht. of Carbon = 19-17 = 11.493° 475° 473° 471° 463° 467° 479° = 11.4730° (195)
17-15 = 11.600° 600° 601° 599° 605° 598° 596° 594° = 11.5991° (167)
15-13 = 11.556° 551° 554° 546° 558° 568° 556° = 11.5555° (111)
13-11 = 11.645° 648° 649° 646° 639° 645° 651° 649° = 11.6465° (23)
11 dia = 8.027° 037° 031° 029° 037° 032° 027° = 8.0314°
Raise 0.0021

Ht of fuel 11-9 = 3.664° 662° 660° 663° 661° 665° = 3.6625°
9-7 = 3.670° 671° 672° 670° 670° 670° = 3.6705° ✓
wt vol Avg = 3.6661°

13-11 up to dia = --- = 11.0030°
11 dia up to 2nd $\frac{3}{8}$ " piece = $3.6705 + [7.392^\circ, 397^\circ, 392^\circ, 400^\circ, 399^\circ, 392^\circ]$ = 11.0658°

gap difference = 63 mils gap

corrected flat fuel height = 3.6696°

REACTIVITY = -4.38°
ANL SUPPORT = $+1.62^\circ$
11-9 \uparrow 8.0 = $+7.25^\circ$ $+9.20^\circ = 3.6705^\circ$
9-7 \rightarrow = 0 $0 = 3.6705 - .0044 = 3.6661^\circ$
15-13 \uparrow III = $+2.71^\circ$
13-11 \uparrow 63 = $+2.00^\circ$
 \rightarrow

11-7" 4" GRAPHITE REFLECTOR + GRAPHITE CORE

~ Pg 155

11.4764	19.17	17.15	15.13	13.11	11.9	9.7	
3/4"	1/8"	1 1/2"	562 mil gap		1/2 x 13	1834	
1255	1233						
13/16"		1 1/2"	1 1/2"		1 1/2 x 11	4212	
1334		1870	1588				
1"	2 1/8"				1/2 x 11	1309	
1444		2 3/8"					
	3776	2439			1 1/2 x 11	3929	345 mil gap
1 1/2"			4 1/2"				
2438							
2 3/8"	3 3/8"	3"	4 6/8"		1 x 7 1/2	1065	
3863	4188	3712					
					1 1/2 x 7	1618	
					1 x 7 A	1065	
4"	3"	2 7/8"	2"		1 x 11	2628	
	4232	2476	2082				
6513					1 x 15	4403	
					1 x 17	6268	
					1 x 19	7828	

MASS OF FUEL = 61251 gm
 VOLUME = 3273.31780 cm³
 ρ = 18.71220 gm/cc

MASS OF GRAPHITE = 85998 gm
 VOLUME = 50314.14519 cm³
 ρ = 1.70922 gm/cc

AVG REFL = 4.000"

Avs. O.D. All Fuel (w't b) = 10.99685"
 I.D. = 7.00281"
 19-17 Carbon O.D. avg wtd = 18.99662"

OD = 120.93070
 ID = 49.03934
 360.87157

11-7 4" ref + core

Mem. Ht. Critical = $3\frac{17}{32}$ "

reactivity = +14.36⁺

Rings = +2.15⁺
Diaphragm = -10.15⁺
S. Stand = +5.76⁺

Lower 0.0100"

$\frac{1}{32}$ " fuel 11-9 = 26.51⁺ 0.8483⁺/mil
9-7 = 25.04⁺ 0.8012

Aug = 1.649⁺/mil

13-11 ext 0.030⁺/mil
Core 0.0646⁺/mil

$\frac{1.6495}{-0.0646}$
1.7141⁺/mil

Wt. of Carbon = 19-17 =

17-15 =

15-13 =

13-11 = Same as 11" dia

11.4730" (-45)

11.5991" (+62)

11.5555" (+10)

= 11.5648" (-32)

8.022" ← 11 dia: 11.505 - .448 - .448 - .500 - .511 - .514 - .508 = 11.5648"

Core = 3.510 - .509 - .510 - .509 - .510 - .509 = 3.5095"

OK

Wt. of fuel = 11-9 = 3.582 - .533 - .532 - .534 - .533 - .532 = 3.5326"
9-7 = 3.544 - .544 - .544 - .544 - .544 - .544 = 3.5440"

Wt Vol Avg = 3.5376"

13-11 thru $\frac{1}{2}$ " = 11.004 - 11.000 - 10.997 - 11.005 - .006 - .006 = 11.0030"

11 dia thru $\frac{1}{2}$ " = 3.544 + [7.521 - .521 - .523 - .519 - .523 - .521 - .521] = 11.0652"
+ .550

gap diff = 62 mils

11" dia

Corrected flat fuel height = 3.5276"

use

React = +14.36⁺
ALL Support = +2.24
11-9 ↑ 11.4 = +9.67
9-7 ↓ 44.5 = +1.86
13-11 ↑ 62 = +2.22
Core ↑ 345 = +2.22
+ 30.35 = 3.5440"

O = 3.5440 - .0177 = 3.5263"

React = +14.36⁺
all Support = +2.24
11-9 ↓ 23.1 = -19.59
9-7 ↓ 44.5 = -35.65
13-11 ↑ 62 = +1.86
Core → 0
- 36.78⁺ = 3.5095"

O = 3.5095 + 0.214 = 3.5309"

~ Pg 179

[illegible]

25-21 OD Carbon = 24.99787" $(^2) = 624.89350$

FUEL MASS = 47944 gm; VOLUME = 2563.51344 cm³; ρ = 18.70245 gm/cc

GRAPHITE MASS: 221.745 gm; VOLUME: 131620.74551 cm³ $\rho = 1.68472 \text{ gm/cc}$

QD. (Ave) Fuel (WTD) = 10.99653" QD² = 120.92367

$$\pm D = 7.00331'' \quad \pm D^2 = 49.04635$$

AVG REFL = 6.997"

11-7

7" ref & No Core

New. Ht. Critical

$$11-9 = 2\frac{3}{4}"$$

$$9-7 = 2\frac{25}{32}"$$

$$\text{reactivity} = -3.17\%$$

$$\text{extra braces on sides} = +1.27\%$$

Rings

S. Stand

$$\text{Diaphragm} = -1.99\%$$

$$804 \text{ miles } (25 \times 21) = +2.90\% \text{ or } .00361\%/\text{mil}$$

$$\frac{1}{32}" \text{ fuel } 11-9 = 37.65\%$$

$$9-7 = 36.63\%$$

$$\text{or } 1.2048\%/\text{mil}$$

$$\text{or } 1.172\%/\text{mil}$$

$$\text{Av.} = 2.376\%/\text{mil}$$

$$\text{Raise } .0034"$$

$$\text{Ht of fuel } 11-9 = 2.756, .755, .754, .756, .755, .756$$

$$9-7 = 2.790, .790, .793, .791, .791, .790$$

$$= 2.7553"$$

$$= 2.7908"$$

$$\text{wt Val Avg} = 2.77107"$$

$$\text{Ht of carbon} = 25-21: \text{ Same as } 181$$

$$21-19: \text{ Same}$$

$$19-17: \text{ Same}$$

$$17-15: \text{ Same}$$

$$15-13: \text{ Same}$$

$$13-11: \text{ Same but } - (.0625") + (.125)$$

$$11 \text{ dia: Same } - (.0625 + .0625) + (.125)$$

$$= 16.1983" (-58)$$

$$= 16.8013" (+224)$$

$$= 16.6786" (-109)$$

$$= 16.8108" (+38)$$

$$= 16.7736"$$

$$= 16.7748"$$

$$= 14.0358"$$

$$\text{Raise } 1.0005$$

$$(19-17) \text{ C ring} = .0049\%/\text{mil} \text{ from p. 181}$$

$$\text{Corrected flat fuel height} = 2.7750"$$

$$\text{React.} = -3.17\%$$

$$\text{ALL Support} = -6.17$$

$$11-9 \uparrow 35.5 = +42.77$$

$$9-7 \rightarrow = 0$$

$$25-21 \uparrow 580 = +2.09$$

$$+35.52\% = 2.7908"$$

$$0 = 2.7908 - .0149 = 2.7759"$$

Pg 181

25-21 OD Carbon 24.99787" $(^2) = 624,89350$
 FUEL MASS = 46932 gm ; VOLUME = 2510.3256 cm³ ; $\rho = 18.69558 \text{ gm/cc}$
 GRAPHITE MASS = 223101 gm ; VOLUME = 133286.2002 cm³ ; $\rho = 1.67384 \text{ gm/cc}$

Avg. O.D. FULL (with D) = 10.99663" OD² = 120.92587 Avg REFL = 6.997"
 I.D. = 7.00296" ID² = 49.0444

11-7 7"ref + Core

Now. 1st. Critical 11-9 = $2\frac{23}{32}$ "
9-7 = $2\frac{1}{16}$ "

reactivity = -0.34%

Value of S. stand + rings + other supports "arms" = +6.84%
diaphragm = -2.71%

Reine 0.0019"

25-21 ring graphite : .00361% / mil (taken from the coreless run)
0.311" on 19-17 mil = 1.54% .0049% / mil
1/32" fuel 11-9 = 35.43% 1.1337% / mil
9-7 = 34.86% 1.1155% / mil
Core = .0494% / mil
2.2492
- .0494
2.2986
net Avg = 2.249% / mil

Ht. of fuel 11-9 = 2.727 - .726 - .726 - .727 - .726 - .726 = 2.7263"
9-7 = 2.696 - .697 - .695 - .696 - .699 - .700 = 2.6971" ✓
net Val Avg = 2.7133"

1st of Carbon 25-21 : 16.200 - .218 - .206 - .183 - .183 - .200 = 16.1983" (-518)
21-19 = 16.796 - .803 - .802 - .803 - .803 - .801 = 16.8013" (+84)
19-17 = 16.669 - .682 - .677 - .686 - .681 - .677 = 16.6786" (-34)
17-15 = 16.809 - .797 - .815 - .822 - .813 - .809 = 16.8108" (+94)
15-13 = 16.765 - .775 - .781 - .784 - .775 - .762 = 16.7736" (+56)
13-11 = 16.708 - .713 - .716 - .713 - .712 - .712 = 16.7123"
11 dia : 14.028 - .038 - .045 - .037 - .038 - .037 = 14.0358"
Core = 2.700 = 2.700"
Reine .001

Corrected flat fuel height = 2.7162" ✓

React. = -0.34%
ALL SUPPORT = -4.13
11-9 ↓ 29.2 = -33.10
9-7 → 0
25-21 ↑ 518 = +1.86
Core ↓ 2.9 = -0.14
-35.85% = 2.6971"
0 = 2.6971 + .0155 = 2.7126"

Pg 293

29	25	21	19	17	15	13
3/4 3664	1/8 3223	3/4 1368	1/16 1285	3/4 1880	3/4 934	9/16 x 13 2061
1 1/2	1.2	1368	1362	2	2B	3/8 x 13 1386
7427	4895	1497	1334	2770	2434	1/2 x 13 1824
3	3	2	2 1/8	2 1/8	2A	1 x 13 B 3760
14600	12350	3546	3440	3776	2476	9/16 x 11 1474
		3	2 3/8	3	1 1/2	1 1/2 x 11
		5325	3B	3712	2	1 1/2 A 3929
9	7	5	4	4 1/2	4 1/2	5273 2 x 11
43550	28700	8827	6513	4222	4628	79 67 37 78 42 36 45 38
						74 101D
						1 x 19 B
						7838
						2 x 25
						27650
1 4485	1 4234	1' 1828	1 x 19 A			7828
			1/2 x 25			6868
5	4 1/2	1 1/2 2673	1 1/2 2438	1 1/2 2098	1 1/2 x 15 A	7485
24550	18455				1 x 21	9666
					2 x 21	19263

11-7 9" ref & No Core

nom. 1st. Critical: $2\frac{7}{16}"$
 support stand & ring }
 ring support } = -5.22°
 diaphragm }

reactivity = -10.35°

fuel value 11-9 = $+23.39^{\circ}$
 9-7 = $+23.11^{\circ}$

$0.7484^{\circ}/\text{mil}$
 $\frac{.7395}{1.4879}$

values run few days later: Use
 calc from 11-9 = 42.84
 11-7 meas \rightarrow 9-7 = 28.3°

$1.3646^{\circ}/\text{mil}$
 $\frac{0.9056}{2.2752}$

Nt. of Carbon 29-25 = $20.272 - .278 - .289 - .295 = 20.2835"$
 25-21 = $20.004 - .980 - .984 - 20.007 = 19.9937"$
 21-19 = $19.920 - .800 - .800 - .805 = 19.920"$
 19-17 = $20.802 - .800 - .800 - .805 = 20.8017"$
 17-15 = $20.479 - .484 - .484 - .473 = 20.4800"$
 15-13 = $20.552 - .551 - .548 - .536 = 20.5467"$
 13-11 = $20.441 - .450 - .435 - .470 = 20.4490"$
 11 di = (Same as 13-11) = $2.4443 = 18.0047"$

Nt. of fuel 11-9 = $2.444 - .445 - .444 - .443 - .444 - .446 = 2.4443"$
 9-7 = $2.443 - .442 - .443 - .443 - .444 - .443 - .444 = 2.4431"$
 wt avg = $2.4437"$

Reactivity = -10.35°
 all supp. = $+5.22^{\circ}$
 29-25 \uparrow 160 mils = $+0.01^{\circ}$
 25-21 \uparrow 450 = $+0.09$
 21-19 \uparrow 523 = $+0.20$
 19-17 \downarrow 358 = -0.21
 17-15 \downarrow 36 = -0.59
 15-13 \downarrow 103 = -1.60
 13-11 \downarrow 5 = -0.11
 $2.4437^{\circ} = -7.34^{\circ}$

(+3.2 mils) $2.4469^{\circ} = \text{clean } \infty$

11-7" 9" REFLECTOR + CORE

PG 295

29 25 21 19 17 15 13 11 9 7										t	
3/4 3664	1 1/2 3283	3/4 1364	1 1/2 1364	3/4 1364	1 1/2 1364	3/4 1364	1 1/2 1364	3/4 1364	1 1/2 1364	1 x 13 A	3682
7427	4895	1997	1	2770	2439	2	20	20	20	3/8 x 13	1386
3	3	2	2 1/8	2 1/8	2 1/8	2 1/8	2 1/8	2 1/8	2 1/8	1 x 13 C	3745
14600	12350	3546	3440	3776	2476	1 1/2	1588	1 1/2	1588	1 x 13 B	3760
9	7	5	4	3	2	1 1/2	1588	1 1/2	1588	1 1/2 x 11	4212
43550	28700	8827	6513	4232	4638	4 1/2	4096	4 1/2	4096	1 1/2 x 11	3929
						3 3/4	4638	3 3/4	4638	2 x 11	5273
						3 3/4	4638	3 3/4	4638	1 x 7 B	1065
						3 3/4	4638	3 3/4	4638	3/8 x 7	404
						3 3/4	4638	3 3/4	4638	1 x 7 A	1065
						3 3/4	4638	3 3/4	4638	1 x 19 B	7838
						3 3/4	4638	3 3/4	4638	2 x 25	27650
4985	4234	1828								1 x 19 A	7828
										1/2 x 25	6868
5	4 1/2	1 1/2	1 1/2	1 1/2	1 1/2	1 1/2	1 1/2	1 1/2	1 1/2	1 1/2 x 15 A	7485
24550	18455	2677	2438	2098						1 x 21	9666
										2 x 21	19263

Gap = 0.101"
13-11 ring

29 MILS VOID

15 MIN DIAPHR

MASS OF FUEL = 41764 gm
 VOLUME = 22 33.36207 cm³
 $\rho = 18.70005 \text{ gm/cc}$
 MASS OF GRAPHITE = 374040 gm
 VOLUME = 217392.14212 cm³
 $\rho = 1.72057 \text{ gm/cc}$
 WTD OD FUEL = 10.99678"
 (2) : 120.92917
 ID = 7.00307"
 (2) : 49.04298

AVG REFL = 9.002"

11-7 9" ref + Cor

Norm. Wt. Critical = $2\frac{13}{32}$ "

reactivity = +15.29⁺

Support stand & ring
& ring support
& diaphragm } = -3.98⁺

fuel value 11-9 = 44.58⁺
9-7 = 47.48⁺

1.4265⁺/mil
1.5193⁺/mil
2.9458⁺/mil

$\frac{1}{8}$ " x 13" dia C = 5.42⁺

or .04336⁺/mil

$\frac{13}{16}$ " (814 mils) 15-17 C = 4.71⁺

or .00578⁺/mil

Wt of carbon 29-25 Same as Pg 293

25-21
21-19
19-17
17-15

15-13

13-11

11 dia

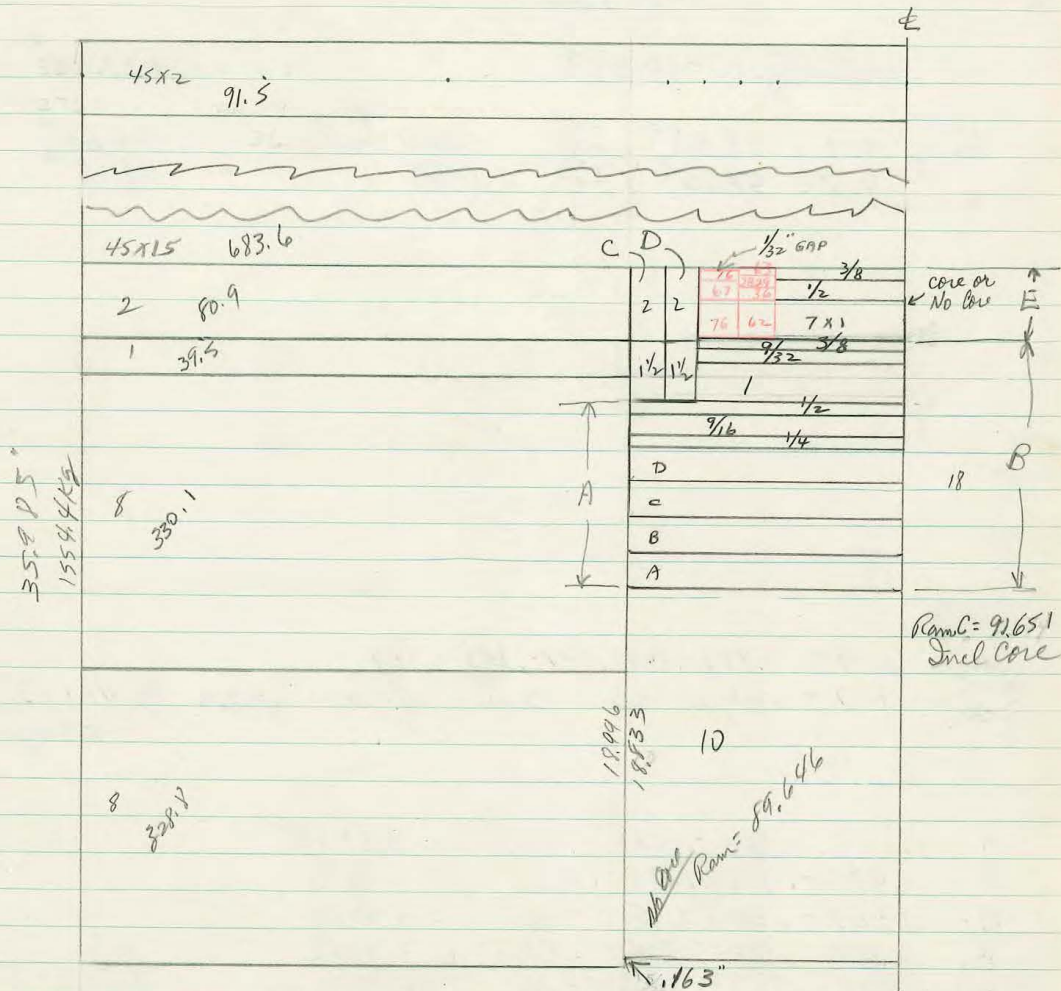
Core

</

TOT. Vol - 937869

11"-7" & 17" GRAPHITE REFLECTOR also + Core

B94-205
207



MASS OF FUEL = 32208 gm

$$Vol = 1724,3438 \text{ cm}^3$$
$$\rho = 18.6784 \text{ gm/cc}$$

Fuel OD = 10.9967 " ⁽²⁾ = 120,92741

1792 ID = 7.0034" (2) = 49.04761

Mass of C = 1644.046 Kg

$$Vol = 934965 \text{ cm}^3$$

$\rho = 1.758 \text{ gm/cc}$

Avg REFL = 16.999"

+ Core

Same

- 1646.051 Kg

- 936 145 cm

$\rho = 1.758 \text{ gm/cc}$

11-7 #17" C. ref Core & No Core
No Core

Norm. Wt. Critical: 9-7 = $1\frac{1}{8}$
 11-9 = $1\frac{2}{32}$

reactivity = -10.384

$\frac{1}{32}$ " of 11-9 = 58,384 ± 54
 9-7 = 44,654 ± 54 1.8681 $\frac{\text{in}}{\text{mil}}$
 1.4288

Core
 Same Core 17"

+33.754

56.734 \pm 1.8153 $\frac{\text{in}}{\text{mil}}$
 39.484 1.2633

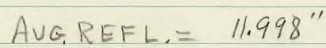
fuel 11-9 = 1.849-.849-.849-.849-.849 = 1.8490
 9-7 - same as 15 dia cf. #10" graph by 4-103 = 1.8826
 wt avg = 1.8639

A = 5.328-.325-.325-.322 = 5.3250"
 B = 6.990-.988-.988-.988 = 6.9855
 C = 3.509-.508-.505-.508 = 3.5075
 D = 3.504-.504-.504-.505 = 3.5042
 E = 1.879-.879-.879-.879 = 1.8790

1.864
 + 1.870 = 3.734

1.864
 - 1.855 = .009

Pg 4-128



11-9 Ring Only \neq 12" ref.

Nom. Wt. Critical = $4\frac{15}{16}$ " (3500 ref. TOP is $\frac{1}{16}$ " TOO MUCH)
reactivity = +11.69%

$\frac{1}{32}$ " fuel value = 24.84% ✓ .7948% fuel

all supports = 4.28%

$\frac{1}{2}$ " 3500 TOP = 21.17%

$\therefore \frac{1}{16}$ " graphite 3500 TOP = 2.64%

fuel ht 11-9 = $(4.943 - .943 - .943 - .942 - .943 - .943 - .944) = 4.9430$ "

A = 2.002, 002, 003, 002 = 2.0022"

B = 6.521, 522, 518, 520 = 6.5202

C = 6.500, 505, 502, 502 = 6.5022

D = ~~1.566~~ - .566 - .563 - .563 - .563 - .565 = 1.5643

$$\begin{array}{r} 4.943 \\ - .943 \\ \hline 4.943 \end{array}$$

11-9 Ring only 12" ref. carbon + Core

"Clean" critical Nom. Wt. = $4\frac{1}{2}$ "
reactivity = $+28.89\%$

$-\frac{1}{32}$ " fuel value = $29.91\%*$ $.9571\%/mil$
all supports value = 3.42%

fuel Wt 11-9 = $4.505 - .505 - .505 - .505 - .505 - .505$ = 4.5050

$$A = 12.006 - .015 - .020 - .020 = 12.0152$$

$$B = 17.042 - .040 - .040 - .045 = 17.0417$$

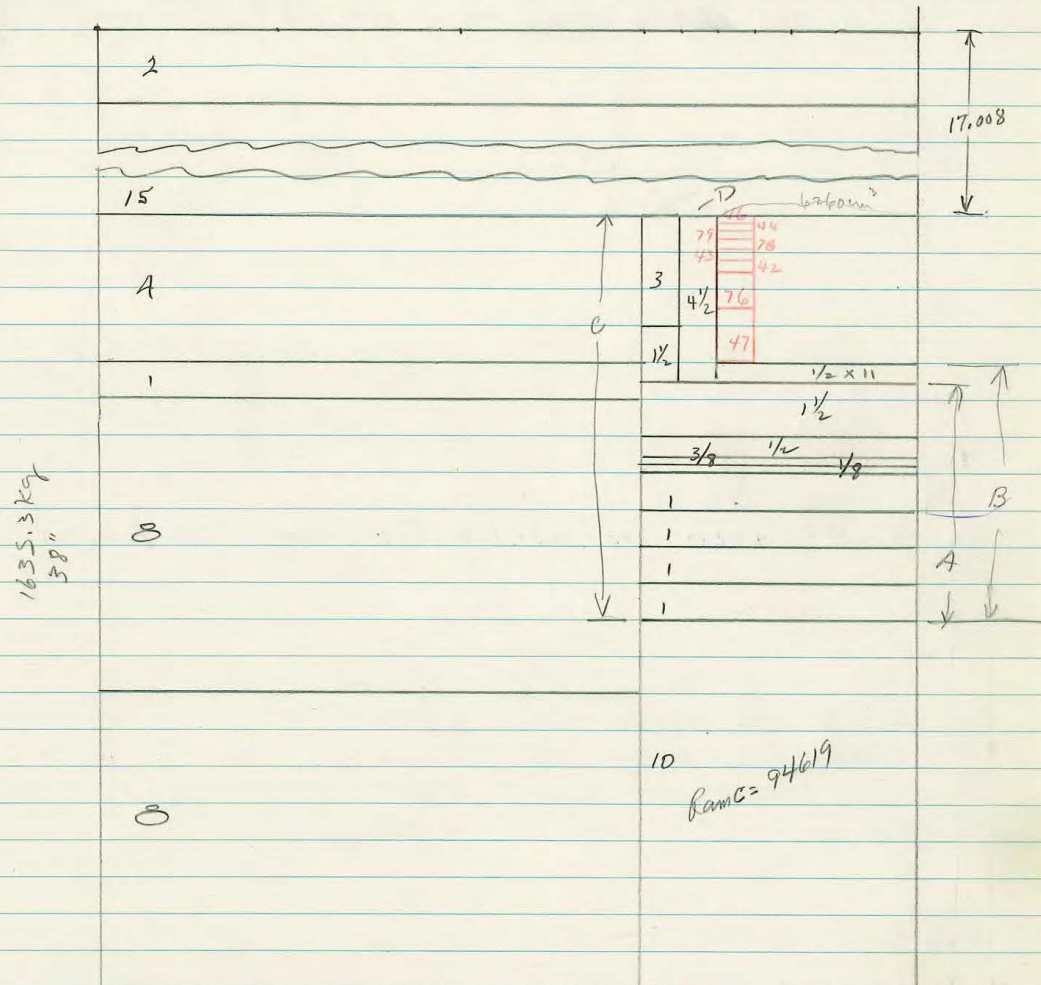
$$Core = 4.497 - .500 - .500 = 4.4990$$

$$\begin{array}{r} 4.505 \\ 1.27 \\ \hline 4.478 \end{array}$$

* Also void $\frac{1}{32}$ " over fuel

11"-9" x 17" GRAPHITE REFLECTOR

4-209



Mass of fuel = 38607 gms
 Vol = 2063.8061 cm³
 P = 18.7066 gm/cc
 OD fuel = 10.99660" (2) = 128.92521
 ID fuel = 9.00176" (2) = 81.03168

Mass C = 1729.919 Kg.
 Vol = 984125 cm³
 P = 1.757 gm/cc
 Avg REFL = 17.004"

11-9 & 17" C. ref No Core

Norm. Wt. Critical = 4"

reactivity = +25.95 \$

$$\frac{1}{32}'' (11-9) = 58.25 + 48.22 \div 2 = 53.24 \text{ } \checkmark \text{ or } 1.7036 \text{ } \checkmark \text{ /mil}$$

fuel kit: 11-9-4.020-020-019-019-019-020 = 4.0195

$$A = 6.503 - .516 - .515 - .511 = 6.5112$$
$$B = 7.002 - .012 - .015 - .016 = 7.012$$

$C = 11.036 - .025 - .037 - .030 = 11.0320$

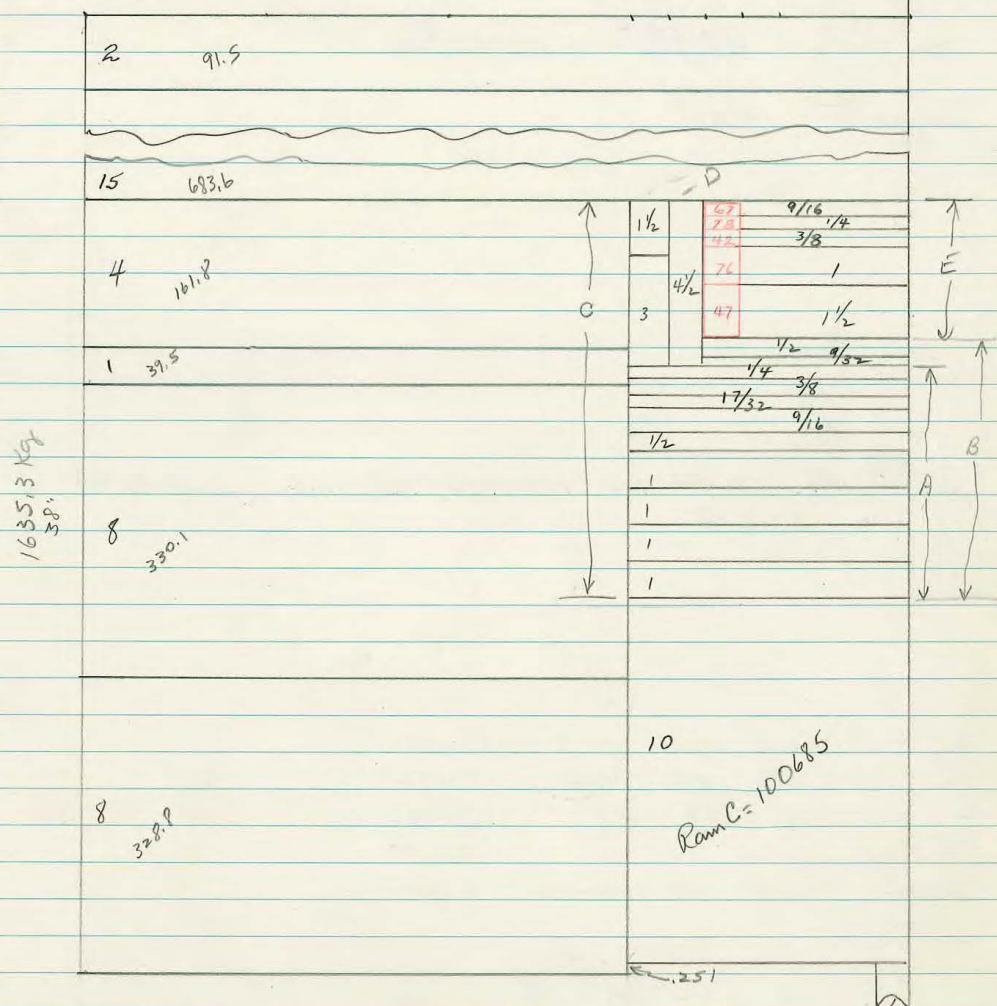
$D = \text{Lacklip} \quad \therefore 4.5000$

Rad. Refl = 16.9945

$$\begin{array}{r} 25007 \\ \times 4019 \\ \hline \end{array}$$

11" 9" & 17" GRAPHITE REFLECTOR + Core

Eg 4-211



Mass of fuel: 35518 gm
 $V_L = 1898.2418 \text{ cm}^3$
 $\rho = 18.7109 \text{ gm/cc}$
 $OD = 10.99654" \text{ } (^2) = 120.92389$
 $ID = 9.00166" \text{ } (^2) = 81.02988$

Mass = 1735.985 Kg
 $Vol = 987174 \text{ cm}^3$
 $\rho = 1.758$
 $AVG \text{ REFL} = 17.007"$

11-9 #17" C. ref + Core

Nom. WT. = $3 \frac{1}{16}$ "
reactivity = -22.32%

$\frac{1}{32}$ " fuel = 47.98% or 1.5353% fuel ✓

Supports = 1.31%

fuel ht: 11-9 = ~~$3.727, 727, 727, 726, 726, 722$~~ = 3.7266
 3.6970

A = $6.235, 235, 228, 233$ = 6.2327

B = $7.013, 026, 018, 020$ = 7.0192

C = $10.745, 740, 746, 739$ = 10.7425

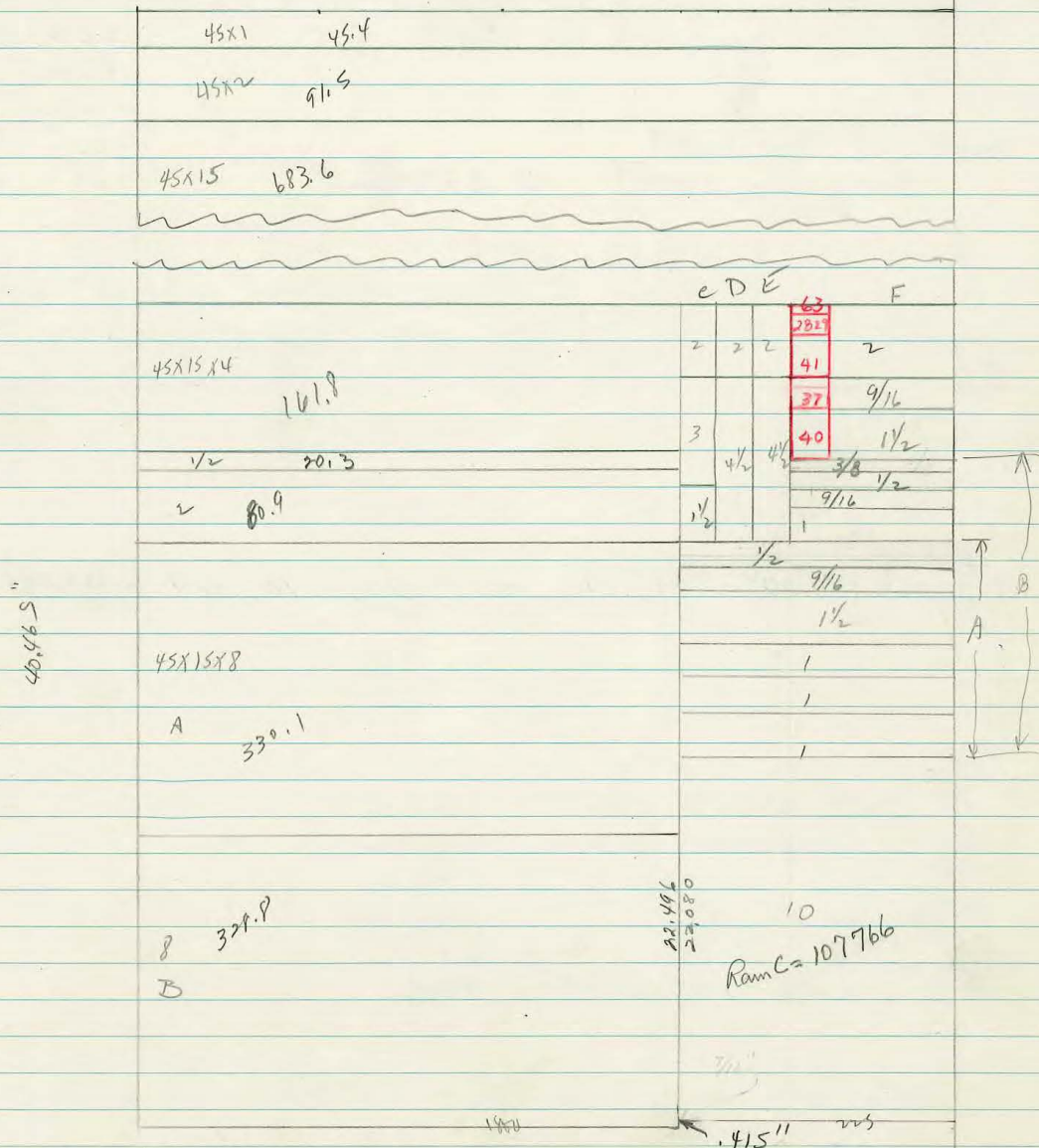
D. ~~fuel~~ 4.5000

Core E = $3.697, 690, 690, 690$ = 3.6917

$$\begin{array}{r} 3697 \\ + 15 \\ \hline 3712 \end{array} = 8$$

9'-7" \pm 18" GRAPHITE REFLECTOR + Core

Pg. 2/4
E



mass of fuel = 31320 gm
 $V_{fuel} = 1670.8090 \text{ cm}^3$
 $\rho = 18.7454 \text{ gm/cc}$
 $\text{OD} = 8.99636" \text{ } (^2) = 80.93449$
 $\text{ID} = 7.00246" \text{ } (^2) = 49.03444$
 $\text{AVG REFL} = 18.005"$

Mass of C = 1850.166 Kg
 $V_{C} = 1052924 \text{ cm}^3$
 $\rho = 1.757 \text{ gm/cc}$

9-7 # 18" C. ref + Core

nom. WT. = $4\frac{1}{16}"$
reactivity = + 11.01 #

45x15x1 C (TDP) = 6.30 #
 $\frac{1}{32}"$ fuel = 27.28 # ✓ .8730 #/in

9-7
wt. of fuel: 4.068, .069, .070, .071, .070, .070, .069 = 4.0695

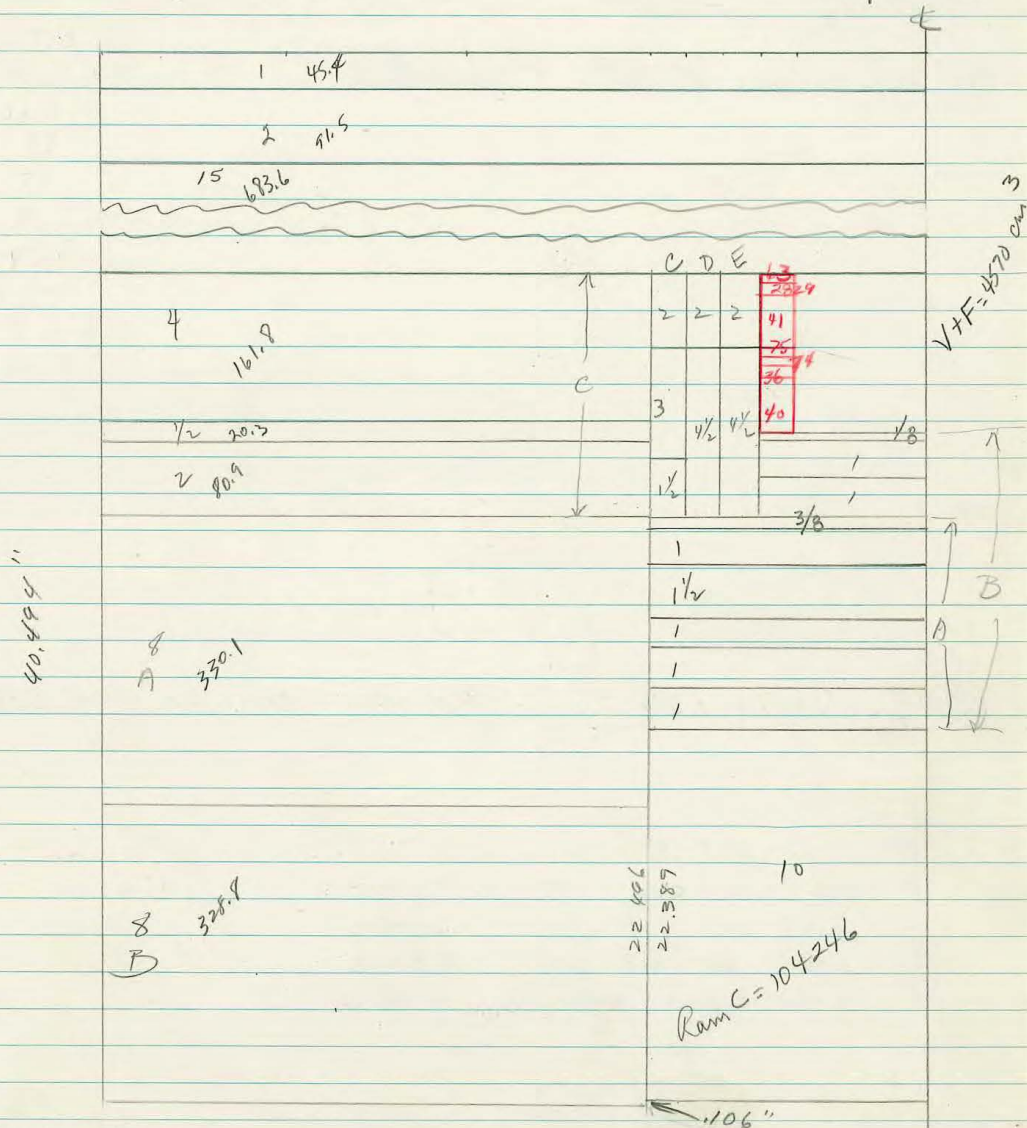
A	5.575, .568, .570, .572	= 5.5712
B	8.016, .014, .015, .012	= 8.0142
C		= 6.5092
D	Same as 4-213	= 6.5012
E		= 6.4982
F	Core = 4.065, .065, .065, .065	= 4.0650

8
4.069
- 1.3

4.059

9"-7" & 18" GRAPHITE REFLECTOR

Pg 4-213



mass of fuel = 33726 gm

Vol = 1800.8645 cm³

$\rho = 18.7276 \text{ gm/cc}$

OD = 8.99634" (²) = 80.93413

ID = 7.00271" (²) = 49.03794

AVG REFL = 18.001"

Mass of C = 1846.646 gm

Vol = 1050.816 cm³

$\rho = 1.757 \text{ gm/cc}$

9-7 #18" C. ref

Nom. Wt. Critical = $4\frac{3}{4}$ "
reactivity = -5.37%

$\frac{1}{32}$ " fuel value = 38.36% \checkmark 1.2275% mil

Wt. of fuel 9-7: 4.387 - .387 - .386 - .387 - .387 - .387 = 4.3868

A $5.877 - .875 - .875 - .880 = 5.8767$

B $8.003 - .005 - .000 - .7998 = 8.0015$

C $6.508 - .510 - .508 - .511 = 6.5092$

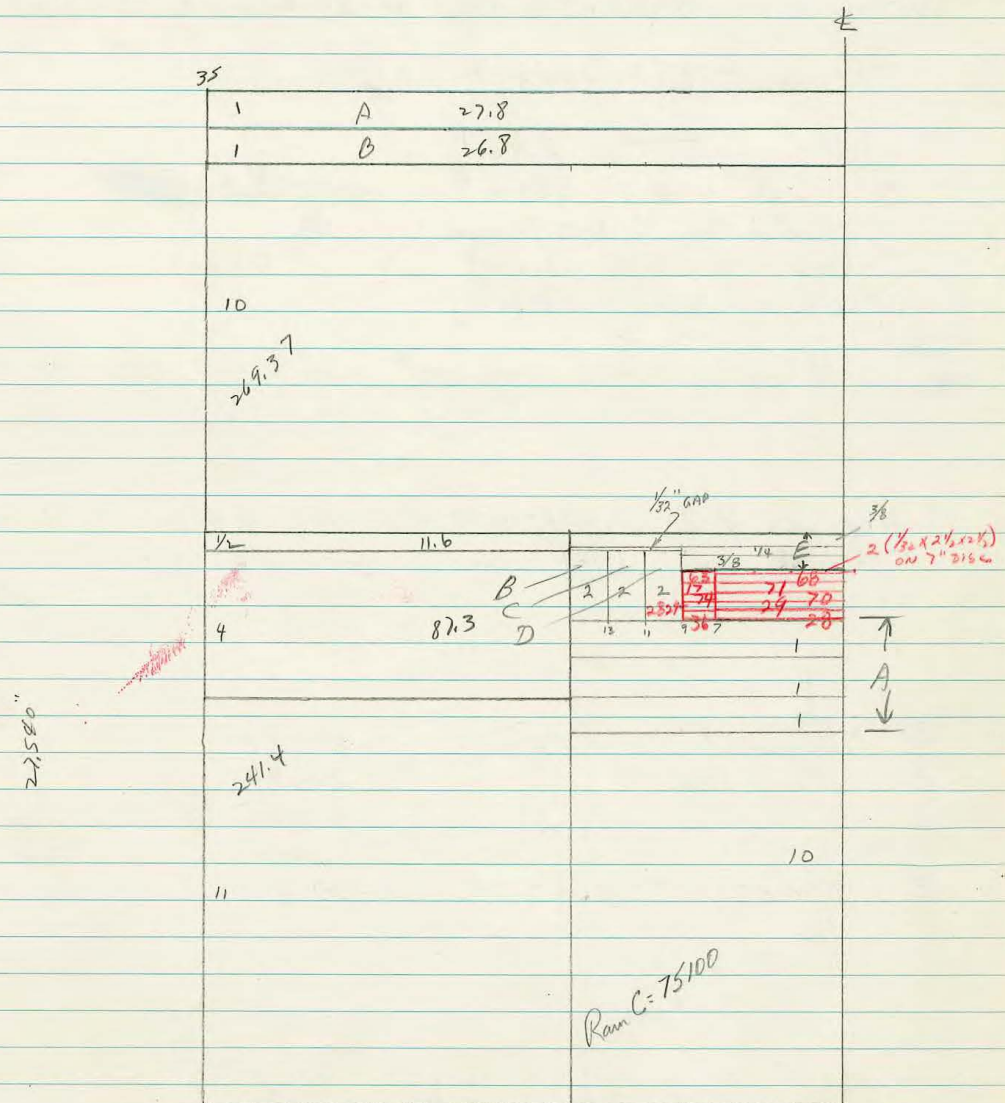
D $6.502 - .500 - .503 - .500 = 6.5012$

E $6.497 - .650 - .6499 - .6496 = 6.4982$

$$\begin{array}{r} 4.386 \\ + \quad \quad \\ \hline 4.390 \end{array}$$

9" DIA. CYL. (SOLID); 13" GRAPHITE REFLECTOR

B4-117



$$\text{MASS OF FUEL} = 27067 + 120 = 27187 \text{ gm}$$

$$\text{VOL} = 1452.670 + 6.4121 = 1459.0821 \text{ cm}^3$$

$$\rho = 18.6336 \text{ gm/cc}$$

$$\text{Ave OD} = 8.99673"$$

$$(\text{OD})^2 = 80.94115$$

$$\text{mass of C} = 739.390 \text{ Kg}$$

$$\text{Vol} = 432746 \text{ cm}^3$$

$$\rho = 1.708 \text{ gm/cc}$$

$$\text{Avg Refl} = 13.013"$$

9" dia cyl #13" w/.

Dom. Ht critical = 9-7 ring @ $1\frac{13}{32}$ "
7" dia c @ $1\frac{13}{32}$ " + 2 ($\frac{1}{32} \times 2\frac{1}{2} \times 2\frac{1}{2}$) pieces

NOTE: GAP ($\frac{1}{32}$ ") over 15-9 Carbon

reactivity = +19.35¢

all supports = 2.96¢

$\frac{1}{32}$ " fuel 11-9 = 39.46¢

7" dia $\frac{1}{32}$ " = Not Meas.

#1 ($\frac{1}{32} \times 2\frac{1}{2} \times 2\frac{1}{2}$) = 20.49¢

#2 ($\frac{1}{32} \times 2\frac{1}{2} \times 2\frac{1}{2}$) = 18.36¢



$\frac{1}{8}$ " gap over 15-9 C = 26.03¢

1.2627¢/mil ~~1.1775~~

01C

.208

Wt of fuel 9-7 = 1.414 - .414 - .415 - .414 - .415 - .415 - .415 = 1.4146"

7" dia = 1.381 - .381 - .381 - .382 - .382 - .381

= 1.3813

wt avg = 1.3944"

A = Same "A" 4-14¢ = 3.0042

B = Look up = 2.0043

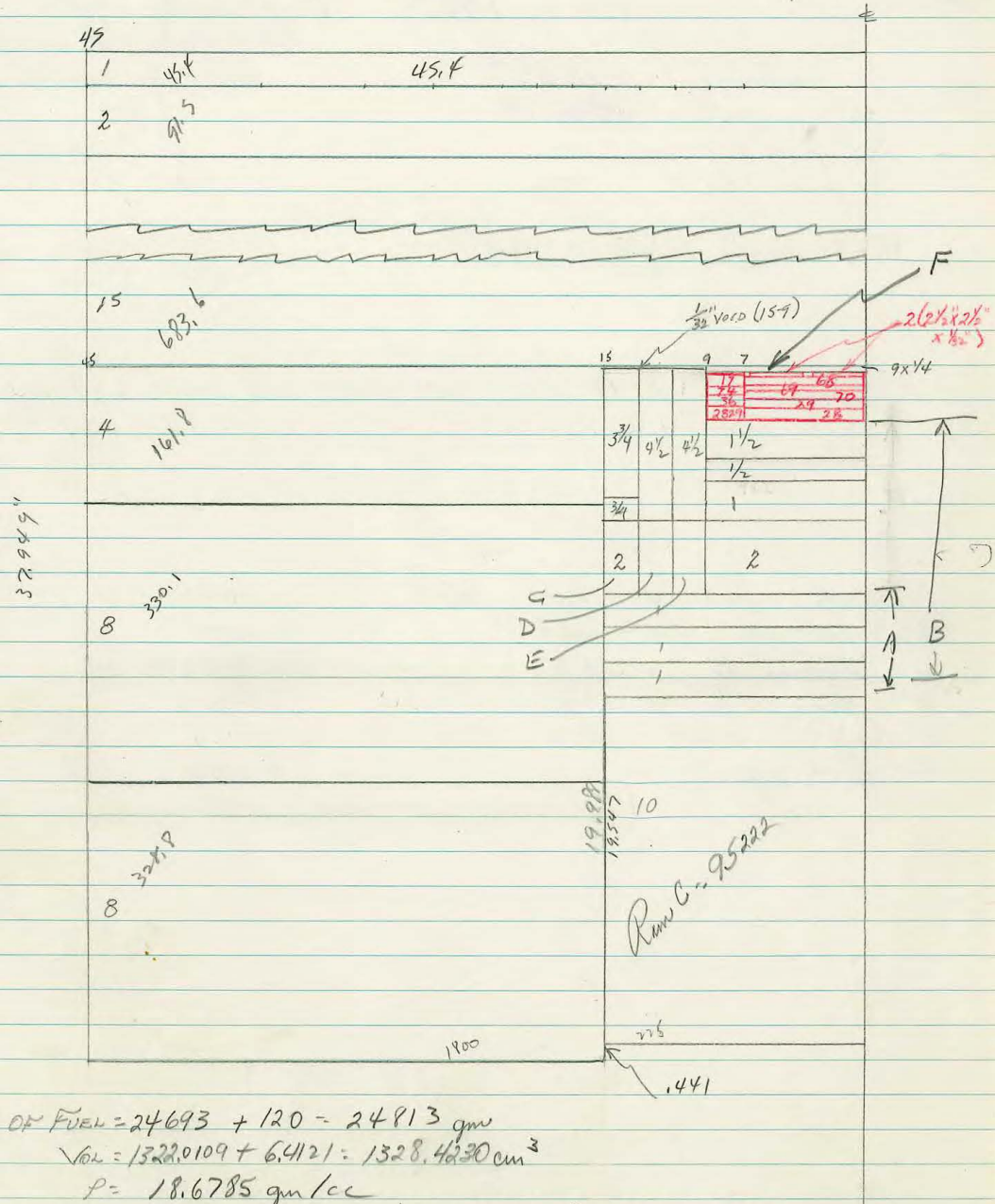
C = " " = 2.0020

D = " " = 2.0000

E = 1.006 - .007 - .004 - .005 = 1.0055

9" dia. CYL (SOLID) & 18" GRAPHITE REF.

Q 4-144



$$\text{MASS OF FUEL} = 24693 + 120 = 24813 \text{ gm}$$

$$\text{VOL} = 1322.0109 + 6.4121 = 1328.4230 \text{ cm}^3$$

$$\rho = 18.6785 \text{ gm/cc}$$

$$\text{MASS OF GRAPHITE} = 1736.422 \text{ Kg} ; \text{Vol} = 987727 \text{ cm}^3 \quad \rho = 1.757$$

$$\text{Avg OD of FUEL} = 8.99683"$$

$$(\text{OD})^2 = 80.94295$$

$$\text{Avg Refl} = 18.004"$$

9" dia cyl (solid) & 18" C ref.

nom. Ht. critical 7" dia = $1\frac{1}{4}" + 2(2\frac{1}{2}" \times 2\frac{1}{2}" \times \frac{1}{32})$
9-7 = $1\frac{9}{32}"$ (ref. ex. stop = $\frac{1}{4}"$)
void over 7" dia as shown)
also $\approx \frac{1}{2}"$ excess on bottom (45-15)

reactivity = +11.57%

all supports = est. @ 14

$\frac{1}{32}"$ fuel 9-7 = —

$\frac{1}{32}"$ fuel 7" dia = —

see pg 134

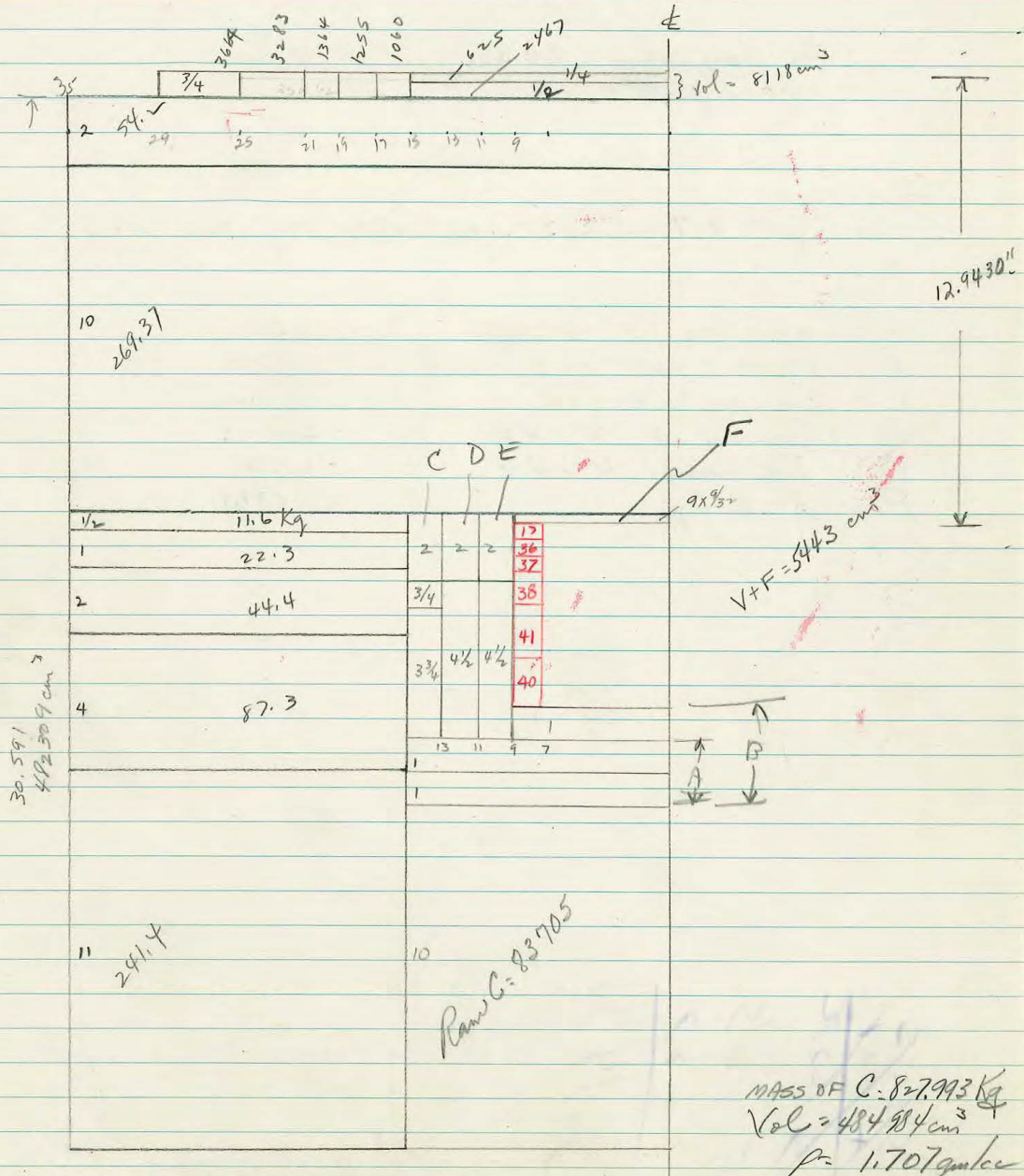
$1(2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{32})$ on 7" dia = 14.98%

Ht of fuel 9-7 = 1.288 - .288 - .288 - .288 - .287 - .288 - .289 - .288 = 1.2880
7" dia = 1.257 - .257 - .256 - .257 - .257 - .257 - .256 = 1.2567
w/ tang = 1.2690

A = 3.005 - .004 - .004 - .000 - .3008	= 3.0042"
B = 8.010 - .010 - .008 - .008 -	= 8.0090
C = Same "B" 4-128	= 6.5202
D = Same as "B" 4-128	= 6.5022
E = 6.497 - .6.500 - .502 - .500	= 6.4997
F = Link Up	= 0.2500

9-7 Ring Only & 13" GRAPHITE REFLECTOR

Eq 4-122



MASS OF FUEL = 40244 gm
 Vol = 2145.2837 cm³
 ρ = 18.7592 gm/cc

AVG OD = 8.99638"
 (OD) = 80.93485
 AVG ID = 7.00255"
 ID = 49.03570

MASS OF C = 827.993 Kg
 Vol = 4848 cm³
 ρ = 1.707 gm/cc

AVG REFL = 12.976"

9-7 Ring only $\pm 13''$ ref.

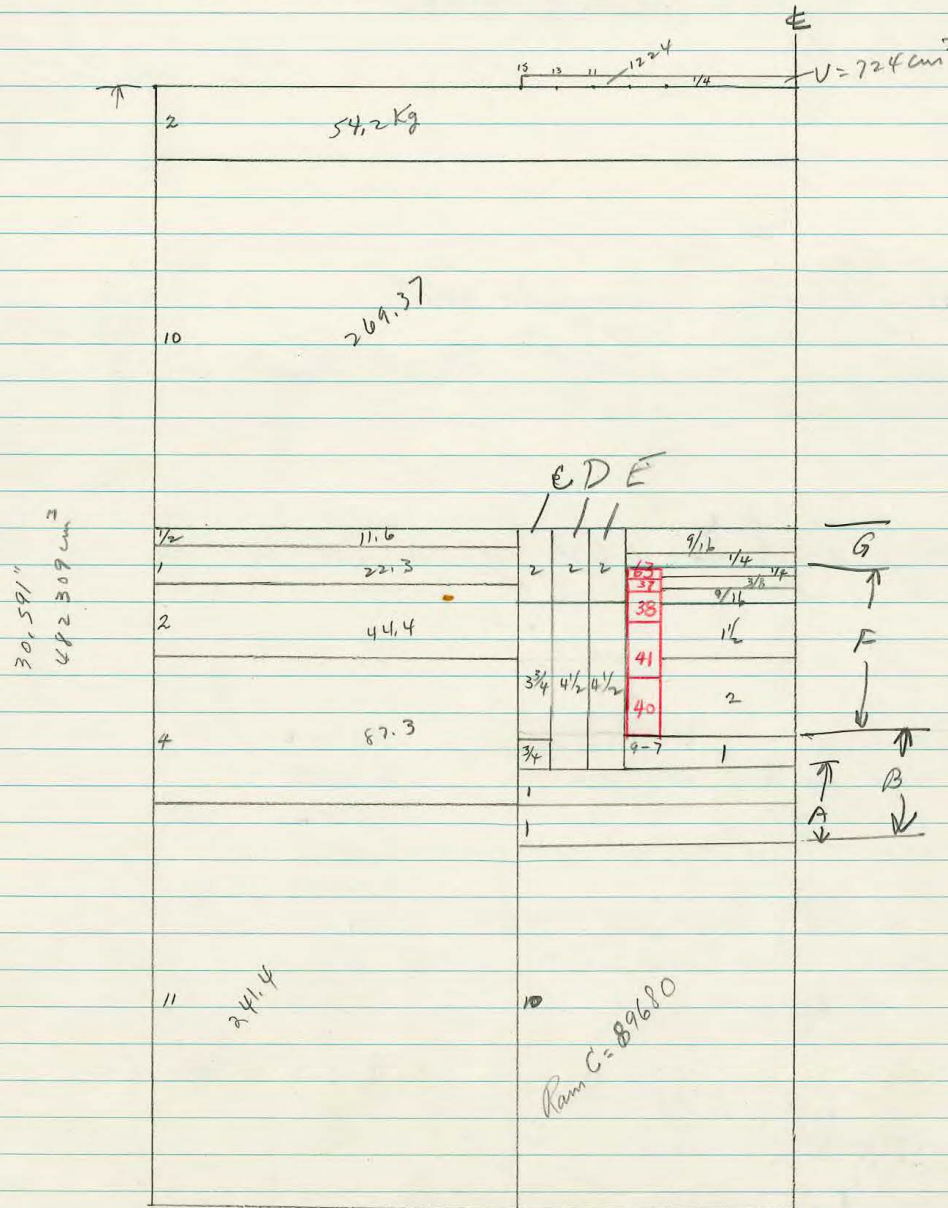
"Clean" Nom. Critical Ht. = $5\frac{7}{32}''$
reactivity = $+26.51\%$

$\frac{1}{32}''$ fuel value = 26.95% ✓ $.8624\%$ mil
all supports = 2.55%

fuel ht 9-7 = $5.225 - .225 - .225 - .226 - .226 - .225 = 5.2253$

A = Same as "A" 4-128	= 2.0022"
B = $3.003 - .004 - .003 - .004$	= 3.0035
C = Same as "C" 4-144	= 6.5202
D = Same as D 4-144	= 6.5022
E = Same as E 4-144	= 6.4997
F = Look up	= 0.2790

~~5.225~~
 ~~$+ .225$~~
 ~~$+ .225$~~
 ~~$+ .226$~~
 ~~$+ .226$~~
 ~~$+ .225$~~
 5.225
 $- .225$
 5.198



MASS OF FUEL = 36135 gm

Vol = 1927.4673 cm³

$\rho = 18.7473 \text{ gm/cc}$

OD_{fuel} = 8.99624" (2) = 80.93233

ID_{fuel} = 7.00268 (2) = 49.03752

Mass of C = 821.474 Kg

Vol = 481106 cm³

$\rho = 1.707 \text{ gm/cc}$

AVG REFL = 13.013"

9-7 Ring only & 13" ref + Core

"Clean" Nom. 1st. Critical = $4\frac{1}{16}$ "
reactivity = -2.82%

gap
51 mil (9" dia) $\frac{1}{16}$ " above fuel = 9.01%
 \therefore 13 mil void = 2.3%
 $\therefore \frac{1}{32}$ " fuel = 23.36% \checkmark 0.7475% /mil
all supports = 2.22%

Wt of 9-7 fuel = $4.695, .695, .696, .695, .697, .695, .695 = 4.6954$

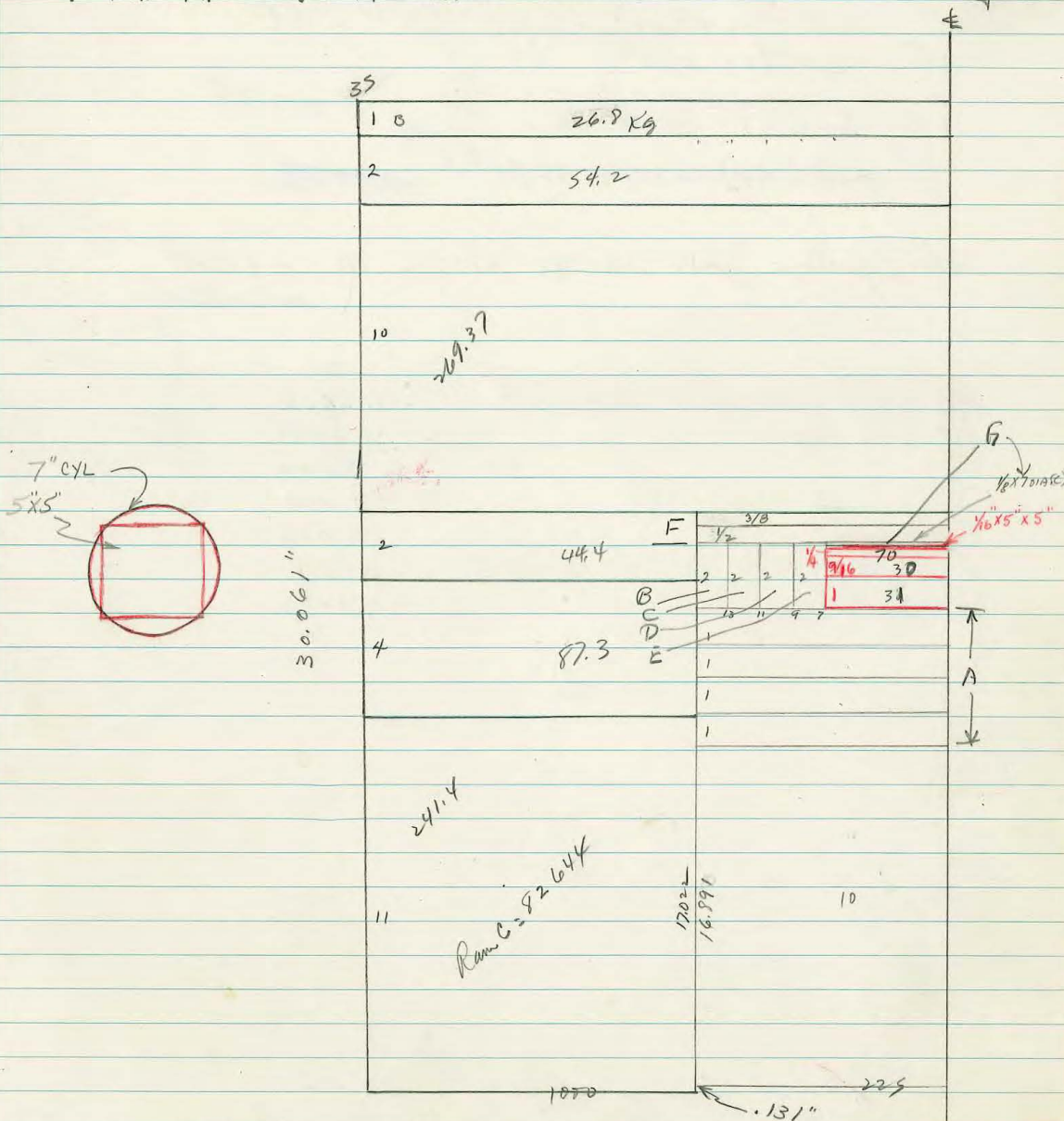
A = Same as "A"	4-122	= 2.0022"
B = Same as "B"	4-122	= 3.0035
C = Same	"	= 6.5202
D =	"	= 6.5022
E =	"	= 6.4997
F =	$4.694, .692, .694, .693$	= 4.6932
G =	$0.815, .813, .813, .814$	= 0.8187

4.6954
+ 4.702

9.3974

7" DIA. CYL. (SOLID) & 14" GRAPHITE REFLECTOR

Pg 4-120



$$\text{Mass of Fuel} = 21442 + 477 \text{ gm} = 21919 \text{ gm}$$

$$\text{Vol} = 11442859 + 25.6049 = 1169.8908 \text{ cm}^3$$

$$\rho = 18.7359 \text{ gm/cc}$$

$$\text{Avg. OD} = 6.99623"$$

$$(\text{OD})^2 = 48.94729$$

$$\text{Aug. Refl} = 14.008"$$

$$\text{Mass of C} = 806.114 \text{ Kg}$$

$$\text{Vol} = 472783 \text{ cm}^3$$

$$\rho = 1.705 \text{ gm/cc}$$

7" dia cyl & 14" ref.

$$\text{Nom. Ht. Critical} = 7" \text{ dia} = 1\frac{13}{16} + 1(\frac{1}{16} \times 5 \times 5)$$

$$\text{reactivity} = +8.66\%$$

$$\text{all supports} = 1.88\%$$

$$1(\frac{1}{32} \times \frac{1}{2} \times \frac{1}{2}) = 20.64\%$$

$$\text{factor}(1.54)(20.64) = 31.79\% \times 4 \quad 4.07\%$$

$$\text{Ht. of fuel} = 1.816 - .816 - .817 - .817 - .816 - .8165 = 1.8164$$

not used 5x5

$$A = 4.008, .006 - .007, .006 - .006 = 4.0066"$$

$$B = \text{Look Up} = 2.0043$$

$$C = " " = 2.0020$$

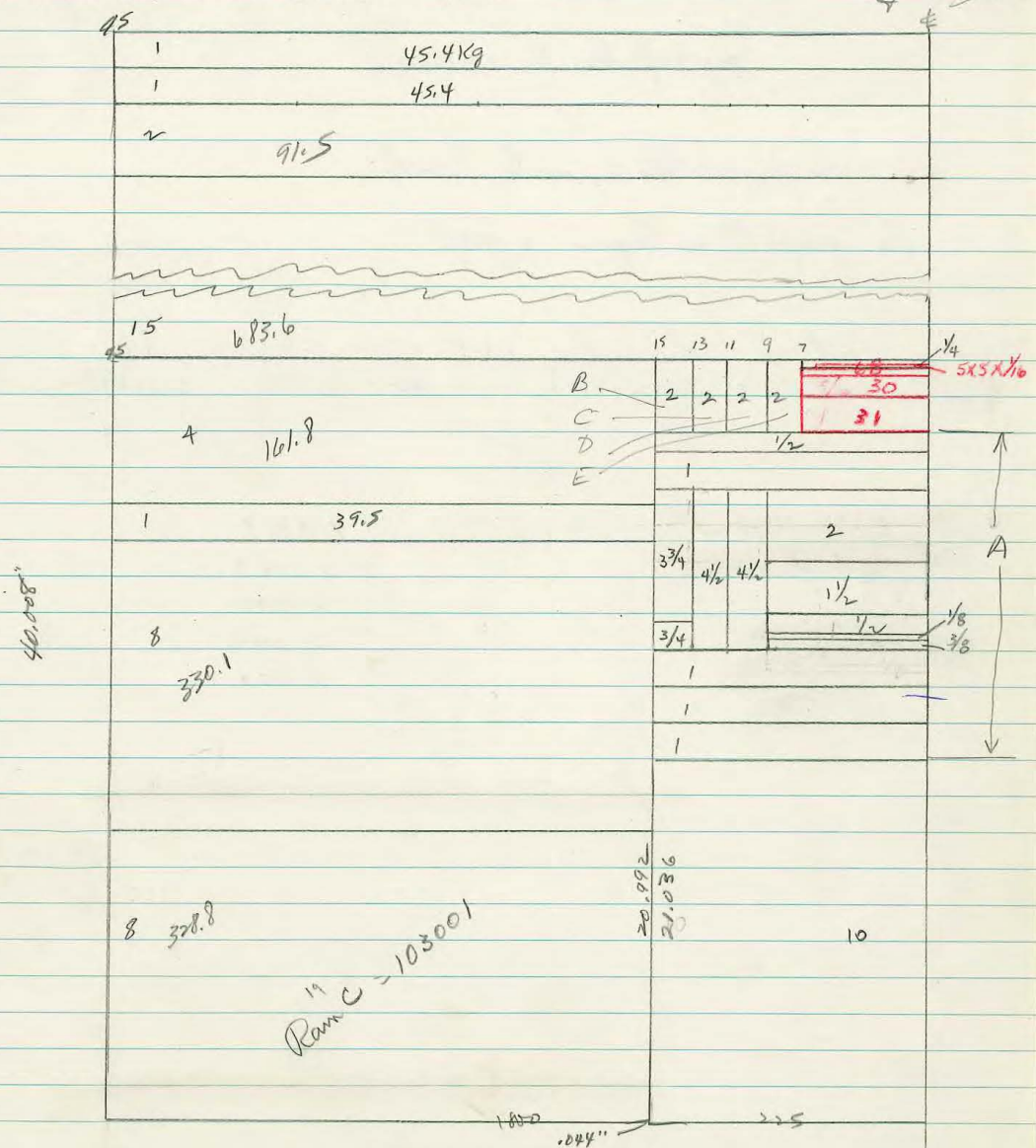
$$D = " " = 2.0000$$

$$E = " " = 2.0000$$

$$F = 0.881 - .880 - .880 - .878 - .880 = 0.8798$$

$$G = \text{Look Up} = 0.1250$$

146?
Pg 4-150


$$V_{\text{tot}} = 1067.9630 + 25.6049 = 1093.5679 \text{ cm}^3$$

MASS OF GRAPHITE: 1829.101 g ; $V = 1041625 \text{ cm}^3$; $\rho = 1.756 \text{ g/cc}$

$$(\sigma_D)^2 = 48.94867$$

9-7 Ring only $\pm 13''$ ref.

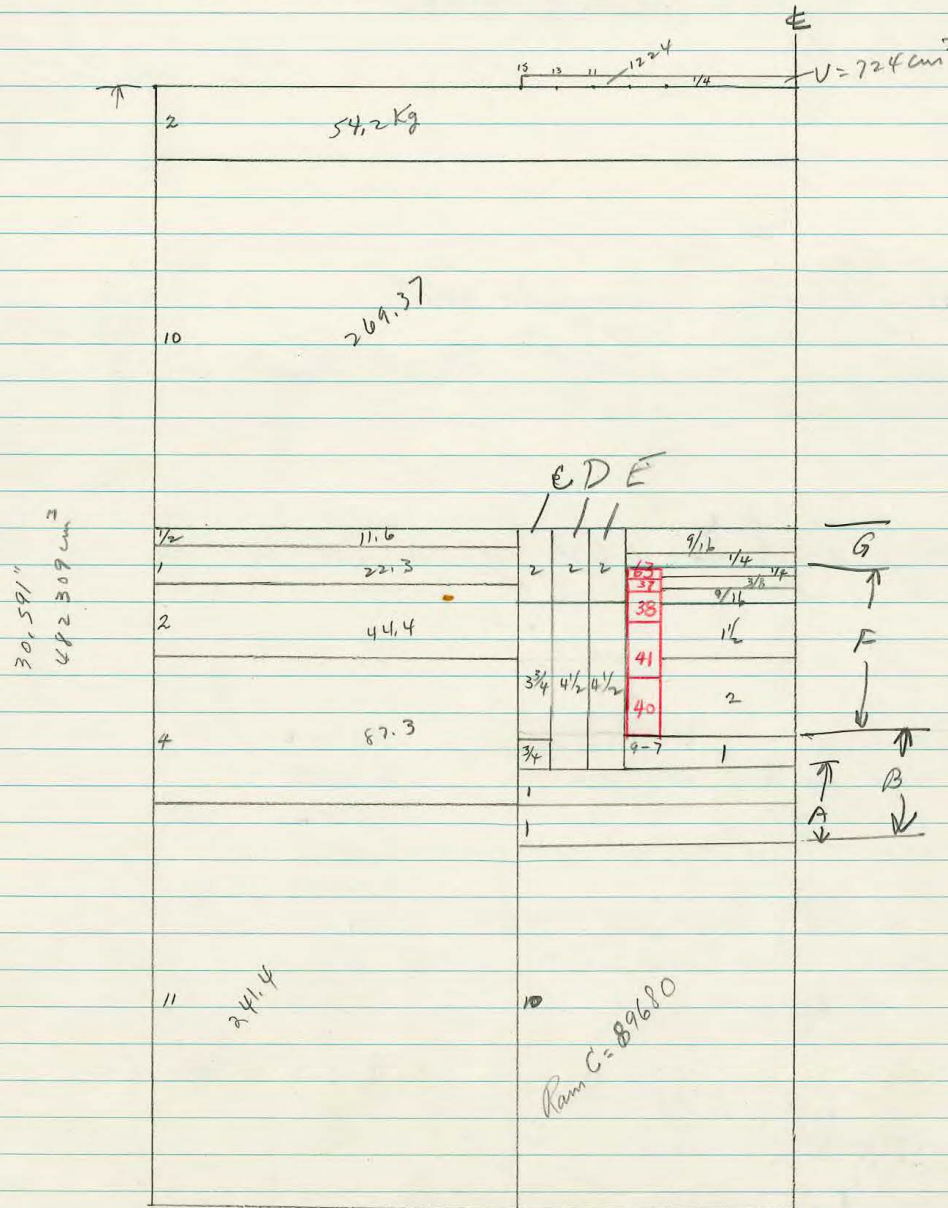
"Clean" Nom. Critical Ht. = $5\frac{7}{32}''$
reactivity = $+26.51\%$

$\frac{1}{32}''$ fuel value = 26.95% ✓ $.8624\%$ mil
all supports = 2.55%

fuel ht 9-7 = $5.225 - .225 - .225 - .226 - .226 - .225 = 5.2253$

A = Same as "A" 4-128	= 2.0022"
B = $3.003 - .004 - .003 - .004$	= 3.0035
C = Same as "C" 4-144	= 6.5202
D = Same as D 4-144	= 6.5022
E = Same as E 4-144	= 6.4997
F = Look up	= 0.2790

~~5.225~~
 ~~5.225~~
 ~~5.225~~
 5.225
 $- .225$
 $\hline 5.198$



MASS OF FUEL = 36135 gm
 $V_{\text{fuel}} = 1927.4673 \text{ cm}^3$
 $\rho = 18.7473 \text{ gm/cc}$

OD_{fuel} = 8.99624" (2) = 80.93233
 ID_{fuel} = 7.00268 (2) = 49.03752

Mass of C = 821,474 Kg
 $V_{\text{refl}} = 481106 \text{ cm}^3$
 $\rho = 1.707 \text{ gm/cc}$

AVG REFL = 13.013"

9-7 Ring only & 13" ref + Core

"Clean" Nom. 1st Critical = $4\frac{1}{16}"$
reactivity = -2.82%

51 mil ^{gap} (9" dia) $\frac{1}{16}"$ above fuel = 9.01%
 \therefore 13 mil void = 2.3%
 $\therefore \frac{1}{32}"$ fuel = 23.36% \checkmark $0.7475\%/mil$
all supports = 2.22%

Wt of 9-7 fuel = $4.695, .695, .696, .695, .697, .695, .695 = 4.6954$

A = Same as "A"	4-122	= 2.0022"
B = Same as "B"	4-122	= 3.0035
C = Same	"	= 6.5202
D =	"	= 6.5022
E =	"	= 6.4997
F =	$4.694, .692, .694, .693$	= 4.6932
G =	$0.815, .813, .813, .814$	= 0.8187

4.6954
+ 4.702

9.3974

7" dia cyl & 14" ref.

$$\text{Nom. Ht. Critical} = 7" \text{ dia} = 1\frac{13}{16} + 1(\frac{1}{16} \times 5 \times 5)$$

$$\text{reactivity} = +8.66\%$$

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$$1(\frac{1}{32} \times \frac{1}{2} \times \frac{1}{2}) = 20.64\%$$

$$\text{factor}(1.54)(20.64) = 31.79\% \times 4 \quad 4.07\%$$

$$\text{Ht. of fuel} = 1.816 - .816 - .817 - .817 - .816 - .8165 = 1.8164$$

not used 5x5

$$A = 4.008, .006, .007, .006 - .006 = 4.0066"$$

$$B = \text{Look Up} = 2.0043$$

$$C = " " = 2.0020$$

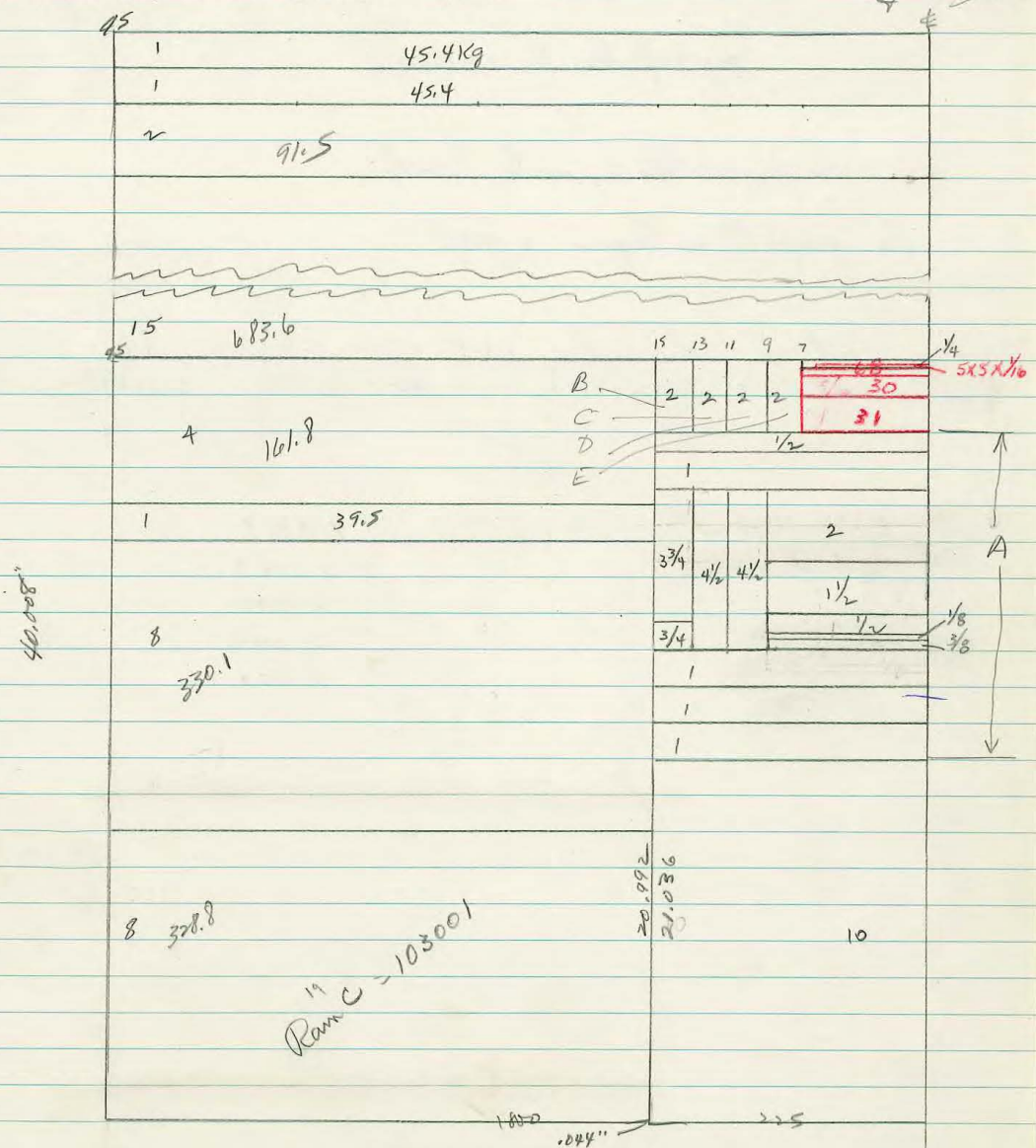
$$D = " " = 2.0000$$

$$E = " " = 2.0000$$

$$F = 0.881, .880, .880, .878 - .880 = 0.8798$$

$$G = \text{Look Up} = 0.1250$$

146?
Pg 4-150


$$V_{\text{tot}} = 1067.9630 + 25.6049 = 1093.5679 \text{ cm}^3$$

MASS OF GRAPHITE: 1829.101 g ; $V = 1041625 \text{ cm}^3$; $\rho = 1.756 \text{ g/cc}$

$$(\sigma_D)^2 = 48.94867$$

7" dia (solid) & 19" C. ref.

Nom. Ht. Critical = $1\frac{1}{16}" + 1(5 \times 5 \times 1/16)$ reactivity = ^{sub} close only

Top Ref has $\frac{1}{4}"$ excess

all supports = mil (0.001")

$\frac{1}{2}"$ graphite on Top = 3.93"

Ht. of 7" dia fuel = 1.695 - .695 - .695 - .695 - .696 - .6955 - .695.

NOT INCL (5X5)

← NOTE

= 1.6952 not incl 5X5

A = 9.035	- .027	- .033	- .032	= 9.037"
B = <i>Look Up</i>				= 2.0043
C = " "				= 2.0020
D = " "				= 2.0000
E = " "				= 2.0000

