

# Measurement of Plutonium Ratios for CRM 137A Recertification



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Chemical Sciences Division

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February 2023

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## ABBREVIATIONS

|           |   |
|-----------|---|
| CRM       | certified reference material                                    |
| GUM       | guide to the expression of uncertainty in measurement           |
| LLNL      | Lawrence Livermore National Laboratory                          |
| MB        | Mass Bias standard  |
| MC-ICP-MS | multiple collector inductively coupled plasma–mass spectrometry |
| MTE       | modified total evaporation                                      |
| NBL-PO    | New Brunswick Laboratory Program Office                         |
| NIST      | National Institute of Standards and Technology                  |
| ORNL      | Oak Ridge National Laboratory                                   |
| QC        | quality control   |
| RSD       | relative standard deviation                                     |
| RSE       | relative standard error   |
| TE        | total evaporation   |
| TIMS      | thermal ionization mass spectrometry                            |
| WRM       | working reference material                                      |



## 1. INTRODUCTION

This report documents the analytical methodologies used by the Chemical and Isotopes Mass Spectrometry (CIMS) Group at the US Department of Energy's Oak Ridge National Laboratory (ORNL) for plutonium isotopic ratio characterizations on purified ~1 mg units prepared by Lawrence Livermore National Laboratory (LLNL) from a mother solution created from an existing 250 mg unit of certified reference material (CRM) 137. The analytical processes described are designed to maintain traceability of the final certified attributes and to eliminate sources of systematic bias for the measurements described. The measurands for certification are the plutonium isotope ratios:  $^{238}\text{Pu}/^{239}\text{Pu}$ ,  $^{240}\text{Pu}/^{239}\text{Pu}$ ,  $^{241}\text{Pu}/^{239}\text{Pu}$ , and  $^{242}\text{Pu}/^{239}\text{Pu}$ . The preparation and analytical process included the following activities:

- Preparation of reference materials to be used as calibrants to establish traceability to the SI unit of mass for the isotopic analyses and quality controls. For the plutonium isotopic analyses, CRM 128 (a CRM comprising equal atoms of  $^{239}\text{Pu}$  and  $^{242}\text{Pu}$ ) was used as the primary calibrant.
- Each CRM 137A unit was reconstituted using dilute high-purity  $\text{HNO}_3$ . From each, seven replicates were distributed for the isotopic characterizations by thermal ionization mass spectrometry (TIMS) using the total evaporation (TE) method for isotope ratio measurements and MC-ICP-MS using a dynamic peak hooping method for secondary isotope ratio measurements.
- Due to time delay in the analyses from the last purification of the original CRM 137 mother solution by LLNL, an aliquot of the three provided plutonium units was purified using Eichrom TEVA separation methods to remove americium in-growth and uranium impurities.
- Minimally corrected data were reported from each analysis using reporting templates provided by the New Brunswick Laboratory Program Office (NBL PO) for the specific methods used for isotopic measurements. In addition, a copy of the instrument exports, Excel templates for isotopic data corrections, and the uncertainty budgets completed with the GUM Workbench software package were submitted to NBL PO.

**Table 1. Summary of isotopic data**

| Instrument | Vial | $^{238}\text{Pu}/^{239}\text{Pu}$ |                           | $^{240}\text{Pu}/^{239}\text{Pu}$ |                           | $^{241}\text{Pu}/^{239}\text{Pu}$ |                           | $^{242}\text{Pu}/^{239}\text{Pu}$ |                           |
|------------|------|-----------------------------------|---------------------------|-----------------------------------|---------------------------|-----------------------------------|---------------------------|-----------------------------------|---------------------------|
|            |      | Value                             | Uncertainty (2 $\sigma$ ) | Value                             | Uncertainty (2 $\sigma$ ) | Value                             | Uncertainty (2 $\sigma$ ) | Value                             | Uncertainty (2 $\sigma$ ) |
| TIMS/TE    | 004  | 0.0026370                         | 0.0000053                 | 0.240626                          | 0.000077                  | 0.005099                          | 0.000034                  | 0.0155775                         | 0.0000067                 |
| MC-ICP-MS  | 004  | —                                 | —                         | 0.240631                          | 0.000072                  | 0.005105                          | 0.000037                  | 0.015573                          | 0.000042                  |
| TIMS/TE    | 052  | 0.0026440                         | 0.0000095                 | 0.240627                          | 0.000078                  | 0.005111                          | 0.000014                  | 0.0155771                         | 0.0000068                 |
| MC-ICP-MS  | 052  | —                                 | —                         | 0.240623                          | 0.000072                  | 0.005105                          | 0.000036                  | 0.015571                          | 0.000043                  |
| TIMS/TE    | 113  | 0.0026482                         | 0.000019                  | 0.240626                          | 0.000076                  | 0.005121                          | 0.000031                  | 0.015578                          | 0.000067                  |
| MC-ICP-MS  | 113  | —                                 | —                         | 0.240635                          | 0.000072                  | 0.005086                          | 0.000040                  | 0.015585                          | 0.000044                  |

## 2. SAMPLE PREPARATION

### 2.1 RECEIVED UNITS

ORNL received three units of C137A from LLNL into Lab R139 in Building 4500S (Figure 1). Units received had identifiers of 004, 052, and 113. Each unit contained 1 mg of a plutonium dry nitrate that appeared as a solid light brown residue from the evaporation process that occurred at LLNL (Figure 2). ORNL also received CRM 128 from NBL PO at the Y-12 National Security Complex; the unit identifier was #313.



Figure 1. Three units of C137A in Mylar bags. ORNL received units 004, 052, and 113.

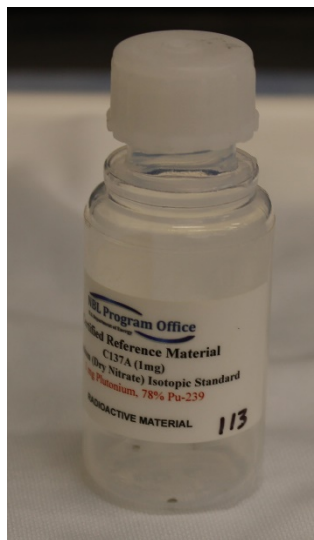


Figure 2. C137A (Unit 113) in 30 mL Teflon bottle with light brown plutonium nitrate residue in the bottom of the vial.

## **2.2 DISSOLUTION**

To dissolve the plutonium nitrate, a 10 mL portion of 4 M HNO<sub>3</sub> + 0.05 M HF was added to each C137A unit, one unit of CRM 128, and a process blank. The acid was prepared from Optima HNO<sub>3</sub> (Lot: 1221120) and Optima HF (Lot: 5217040) purchased from Fisher Scientific, diluted with ASTM Type I water. C137A dissolved after 1 hour on a hot plate set to 60 °C, whereas CRM 128 required 2 hours to dissolve.

### **2.2.1 Sampling**

Each time sampling occurred, a 100 µL aliquot (to provide 10 µg Pu) of each C137A solution and the CRM 128 solution was pipetted into a perfluoroalkoxy vial and transferred to Building 1060 Lab 104 for separation. Triplicate aliquots were pulled from the process blank.

### 3. SEPARATION

#### 3.1 REAGENTS AND MATERIALS

All acids ( $\text{HNO}_3$ ,  $\text{HCl}$ , and  $\text{HF}$ ) and  $\text{H}_2\text{O}_2$  (30%) were Optima grade, purchased from Fisher Scientific and used without further purification. Dilutions of acids were made using ASTM Type I water ( $>18.0 \text{ M}\Omega \cdot \text{cm}$ ) generated using a Thermo Scientific Barnstead GenPure xCAD Plus water purification system. Iron(II) sulfate heptahydrate (Puratronic, 99.999%, metal basis) and sodium nitrite (99.999%, metal basis) were purchased from Alfa Aesar and used without further purification. TEVA cartridges (1 mL, 50–100  $\mu\text{m}$ ) were purchased from Eichrom Technologies.

#### 3.2 METHOD

Plutonium was chemically purified from uranium and americium before isotopic analysis to ensure separation from isobaric interference at mass 239 (uranium hydride  $^{238}\text{UH}^+$ ) and mass 241 ( $^{241}\text{Pu}$  decays to  $^{241}\text{Am}$ ). This purification was accomplished via extraction chromatography with Eichrom TEVA 1 mL cartridges following an established analytical method (CSD-AM-CIMS-IN15<sup>1</sup>) using a vacuum box system inside a radiological hood, as shown in Figure 3. Before separation, samples were dried to remove trace HF and dissolved in 2 mL of 3 M  $\text{HNO}_3$ . The oxidation state of plutonium in the sample was adjusted to Pu(IV) with ferrous sulfate and sodium nitrite before loading on a preconditioned TEVA cartridge. After loading, the cartridge was rinsed with 38 mL of 3 M  $\text{HNO}_3$ , converted to the chloride form with 3 mL of 9 M  $\text{HCl}$ , and plutonium was eluted from the resin with 10 mL of 0.1 M  $\text{HCl}$ –0.06 M  $\text{HF}$ . The samples were dried and treated twice with a 1:1 v/v mixture of 8 M  $\text{HNO}_3$  and  $\text{H}_2\text{O}_2$  (30%) to remove any residual column organics. Before the solution were ready for TIMS loading, 20–50  $\mu\text{L}$  8 M  $\text{HNO}_3$  were added to the samples.

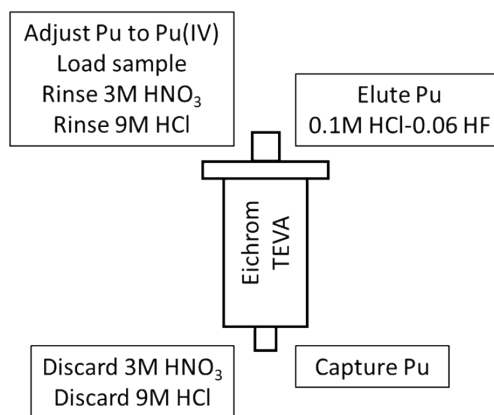


Figure 3. Separation scheme for the purification of plutonium.

## 4. ANALYSIS

### 4.1 PLUTONIUM ISOTOPIC COMPOSITION BY TIMS

The isotopic characterizations were performed utilizing the TE method. For this method, approximately 50 ng of plutonium solution was loaded onto a zone-refined double filament. This method is outlined in the following subsections, as described in ASTM 1672<sup>2</sup>. Any method deviation was recorded. Dr. Cole Hexel was previously qualified on the TE method by Dr. K. J. Mathew at the NBL labs on the Argonne National Laboratory campus when the facility was still in operation.

#### 4.1.1 Filament Preparation

High-purity zone-refined rhenium filaments were used for all analyses. The filaments were made by MasCom (Breman, Germany), and purchased from Thermo Fisher Scientific, part number 4062350. The filaments were welded in a double-filament geometry. Before sample loading, the filaments were degassed to condition the filament surface and remove contamination. Table 2 outlines the filament degassing program. No filament background signal was observed from the degassed filament.

Table 2. Filament degassing program

| <b>ParameterC</b> | <b>Program</b>       |           |
|-------------------|----------------------|-----------|
| Limit 1           | $1.0 \times 10^{-5}$ |           |
| Limit 2           | $9.0 \times 10^{-6}$ |           |
| C1 (Ioni)         | Wait 1               | 1 min     |
|                   | Slope                | +1 A/min  |
|                   | I1                   | 4.7 A     |
|                   | Wait 2               | 30 min    |
|                   | Slope 2              | -10 A/min |
| C2 (Evap)         | Wait 1               | 40 min    |
|                   | Slope                | +1 A/min  |
|                   | I1                   | 4.7 A     |
|                   | Wait 2               | 30 min    |
|                   | Slope 2              | -10 A/min |
| C1 + C2           | Wait 1               | 40 min    |
|                   | Slope                | +50 A/min |
|                   | I1                   | 5.0 A     |
|                   | Wait 2               | 15 s      |
|                   | Slope 2              | -50 A/min |

#### 4.1.2 Filament Loading Method

Conditioned filaments were aged for a minimum of 25 days before use. No filaments were aged longer than 30 days. Initially, a filament was heated to 1.6 A, and the edge of a parafilm strip created a hydrophobic dam. This hydrophobic barrier did not perturb the plutonium isotopic analysis but did prevent the sample from skating across the filament surface. After applying the barrier, the filament was cooled to 0 A for loading. Approximately 50 ng of plutonium solution was loaded in 1-0.5  $\mu$ L application. The droplet was

then dried at 0.6 A to evaporate the liquid without causing sample splattering. Once the sample was dry, the amperage was increased to 1 A for 60 s then to 1.5 A for 5 s, and finally to 2 A for 5 s. Next, the filaments were returned to 0 A and loaded onto the turret. Sample filaments and the corresponding ionization filaments were immediately installed on the sample turret along with the extraction plate. All extraction plates were new and placed in the same orientation on the sample turret. Appendix A includes the original filament loading sheets.

#### 4.1.3 Filament Position on Sample Turret

Three turrets were analyzed during a 1 week period. Samples were randomly distributed on each turret. Each sample vial was analyzed using seven replicates. Any sample filament that did not run was added to the third turret to maintain a total of seven replicates. The sample filament distribution can be found in Table 3.

**Table 3. TIMS plutonium isotopic composition turret analysis scheme**

| <b>Turret Position</b> | <b>Turret 1</b>      | <b>Turret 2</b>      | <b>Turret 3</b>      |
|------------------------|----------------------|----------------------|----------------------|
| Position 1             | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> |
| Position 2             | <i>NBL 137 (QC)</i>  | <i>NBL 137 (QC)</i>  | <i>NBL 137 (QC)</i>  |
| Position 3             | <i>NBL 136 (QC)</i>  | <i>NBL 136 (QC)</i>  | <i>NBL 136 (QC)</i>  |
| Position 4             | NBL PO 137A-1a       | NBL PO 137A-2a       | NBL PO 137A-2a       |
| Position 5             | NBL PO 137A-2a       | NBL PO 137A-3a       | NBL PO 137A-2a       |
| Position 6             | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> |
| Position 7             | NBL PO 137A-3a       | NBL PO 137A-1a       | NBL PO 137A-3a       |
| Position 8             | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> |
| Position 9             | <i>NBL 137 (QC)</i>  | <i>NBL 137 (QC)</i>  | <i>NBL 137 (QC)</i>  |
| Position 10            | NBL PO 137A-1b       | NBL PO 137A-2b       | NBL PO 137A-3a       |
| Position 11            | NBL PO 137A-2b       | NBL PO 137A-1b       | ORNL WRM 003         |
| Position 12            | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> |
| Position 13            | <i>NBL 136 (QC)</i>  | <i>NBL 136 (QC)</i>  | <i>NBL 136 (QC)</i>  |
| Position 14            | NBL PO 137A-3b       | NBL PO 137A-3c       | NBL PO 137A-1a       |
| Position 15            | NBL PO 137A-1c       | NBL PO 137A-1c       | ORNL WRM 003         |
| Position 16            | NBL PO 137A-2c       | NBL PO 137A-1c       | ORNL WRM 003         |
| Position 17            | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> |
| Position 18            | NBL PO 137A-3c       | NBL PO 137A-2c       | ORNL WRM 003         |
| Position 19            | <i>NBL 137 (QC)</i>  | <i>NBL 137 (QC)</i>  | <i>NBL 137 (QC)</i>  |
| Position 20            | <i>NBL 136 (QC)</i>  | <i>NBL 136 (QC)</i>  | <i>NBL 136 (QC)</i>  |
| Position 21            | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> | <b>NBL C128 (MB)</b> |

Note: QC = quality control; MB = mass bias ; WRM = working reference material

#### 4.1.4 Detector Configuration, Amplifiers, and Calibration

The gain history was used to select the instrument amplifiers that had the lowest standard deviation. The lowest deviation amplifiers were used on mass,  $m/z$ , and the 241 faraday cup. Subsequently the 242, 244, 238, 240, and 239 faraday cup amplifiers were populated in that order (Table 4). The most stable amplifier was used for the least abundant isotope. Only the  $10^{11}$  amplifiers were selected for the TE method. The ORNL WRM 003 sample was used to verify that the detectors were coincident. No amplifier rotation was applied. The faraday detector gain was electronically determined for 3 h using a 0.3333334 gain calibration card. This calibration was performed before the three turrets were analyzed. The results were consistent with the gain history, and the values were within the historical deviation. After the gain calibration, a baseline was conducted for 1,800 s. A baseline was performed before each turret was analyzed. A beam of  $^{187}\text{Re}$  was placed on the center faraday cup to verify the faraday mass calibration. A mass calibration filament was loaded, and a full mass calibration was performed at the beginning of the project analysis. The instrument was calibrated at lithium, sodium, strontium, neodymium, rhenium, uranium, plutonium, and UO masses. Before each filament analysis, rhenium and plutonium were recalibrated. No instrument drift was observed.

**Table 4. Historical gain from the instrument’s history log**

| Timestamp        | Amp 1                | Amp 2              | Amp 3                | Amp 4                | Amp 5                | Amp 6                | Amp 7                | Amp 8                |
|------------------|----------------------|--------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| 10/4/2018 16:40  | 0.33222              | 0.33755            | 0.32926              | 0.32844              | 0.32988              | 0.33407              | 0.32777              | 0.33011              |
| 3/27/2020 12:55  | 0.33219              | 0.33757            | 0.32926              | 0.32845              | 0.32988              | 0.33408              | 0.32778              | 0.33012              |
| 8/25/2020 16:44  | 0.33212              | 0.33753            | 0.32921              | 0.32842              | 0.32983              | 0.33403              | 0.32773              | 0.33008              |
| 11/3/2020 11:28  | 0.33207              | 0.33749            | 0.32916              | 0.32836              | 0.32979              | 0.33399              | 0.32768              | 0.33003              |
| 1/14/2021 16:32  | 0.33207              | 0.33749            | 0.32915              | 0.32836              | 0.32978              | 0.33398              | 0.32767              | 0.33002              |
| 1/31/2021 14:57  | 0.33206              | 0.33749            | 0.32915              | 0.32836              | 0.32978              | 0.33397              | 0.32766              | 0.33002              |
| 2/5/2021 19:08   | 0.33205              | 0.33749            | 0.32915              | 0.32836              | 0.32978              | 0.33398              | 0.32765              | 0.33002              |
| 2/23/2021 12:04  | 0.33205              | 0.33749            | 0.32914              | 0.32834              | 0.32976              | 0.33397              | 0.32764              | 0.33                 |
| 3/9/2021 16:13   | 0.33207              | 0.33751            | 0.32916              | 0.32837              | 0.32978              | 0.33398              | 0.32766              | 0.33003              |
| 3/10/2021 17:01  | 0.33217              | 0.33744            | 0.32895              | 0.3285               | 0.32978              | 0.33397              | 0.32777              | 0.32968              |
| 5/10/2021 22:39  | 0.33203              | 0.33746            | 0.32911              | 0.32833              | 0.32974              | 0.33394              | 0.32762              | 0.32998              |
| 6/17/2021 23:33  | 0.33198              | 0.33743            | 0.32908              | 0.3283               | 0.32972              | 0.33391              | 0.32759              | 0.32996              |
| 7/21/2021 22:29  | 0.332                | 0.33745            | 0.32909              | 0.32831              | 0.32972              | 0.33392              | 0.32759              | 0.32997              |
| 8/1/2021 23:07   | 0.33207              | 0.33754            | 0.32912              | 0.32837              | 0.32974              | 0.33397              | 0.32759              | 0.33                 |
| 10/19/2021 4:43  | 0.33208              | 0.33755            | 0.32912              | 0.32836              | 0.32975              | 0.33396              | 0.3276               | 0.32999              |
| 11/23/2021 0:13  | 0.33206              | 0.33752            | 0.32912              | 0.32835              | 0.32975              | 0.33395              | 0.3276               | 0.32999              |
| 12/7/2021 6:00   | 0.33205              | 0.33751            | 0.32911              | 0.32833              | 0.32975              | 0.33395              | 0.3276               | 0.32998              |
| 1/28/2022 2:55   | 0.33203              | 0.33748            | 0.3291               | 0.32832              | 0.32973              | 0.33394              | 0.32759              | 0.32997              |
| 6/16/2022 14:22  | 0.33196              | 0.33741            | 0.32905              | 0.32825              | 0.32967              | 0.33388              | 0.32755              | 0.32991              |
| 8/11/2022 19:11  | 0.33192              | 0.33738            | 0.32902              | 0.32823              | 0.32966              | 0.33385              | 0.32754              | 0.3299               |
| 10/20/2022 16:48 | 0.3319               | 0.33736            | 0.32901              | 0.32821              | 0.32964              | 0.33384              | 0.32753              | 0.32988              |
| 10/24/2022 11:16 | 0.3319               | 0.33736            | 0.32901              | 0.32821              | 0.32964              | 0.33384              | 0.32752              | 0.32988              |
| Avg              | 0.33205              | 0.33748            | 0.32911              | 0.32834              | 0.32975              | 0.33395              | 0.32763              | 0.32998              |
| Std dev          | $8.4 \times 10^{-5}$ | $6 \times 10^{-5}$ | $7.7 \times 10^{-5}$ | $7.3 \times 10^{-5}$ | $6.5 \times 10^{-5}$ | $6.4 \times 10^{-5}$ | $7.7 \times 10^{-5}$ | $9.3 \times 10^{-5}$ |
| % RSD            | 0.0252%              | 0.0178%            | 0.0235%              | 0.0224%              | 0.0198%              | 0.0191%              | 0.0235%              | 0.0282%              |
| Mass             |                      | 241                | 244                  | 239                  | 240                  | 242                  | 238                  |                      |

#### 4.1.5 Sample Analysis Method

TIMS startup, tuning, and initial setup was conducted according to the standard operating procedure for the plutonium isotope ratios ( $^{238}\text{Pu}/^{239}\text{Pu}$ ,  $^{240}\text{Pu}/^{239}\text{Pu}$ ,  $^{241}\text{Pu}/^{239}\text{Pu}$ ,  $^{242}\text{Pu}/^{239}\text{Pu}$ ,  $^{244}\text{Pu}/^{239}\text{Pu}$ ). A sample isotopic survey was performed before the sample turret was analyzed, and no  $^{244}\text{Pu}$  was observed via the faraday cup. The instrument optimized the ionization filament to yield a rhenium signal of 160 mA or to a filament current of about 5,100 mA. A filament tune and a mass calibration on  $^{187}\text{Re}$  was completed at this heating step. The evaporator current was increased, and the TE analysis started. The filament current was increased to yield a summed total ion current of 3 V and run to exhaustion. The sample mass bias was corrected using an exponential correction model based on the average  $^{242}\text{Pu}/^{239}\text{Pu}$  ratio in the CRM 128 comparator sample filaments. The method and heat profile are shown in Figure 4.

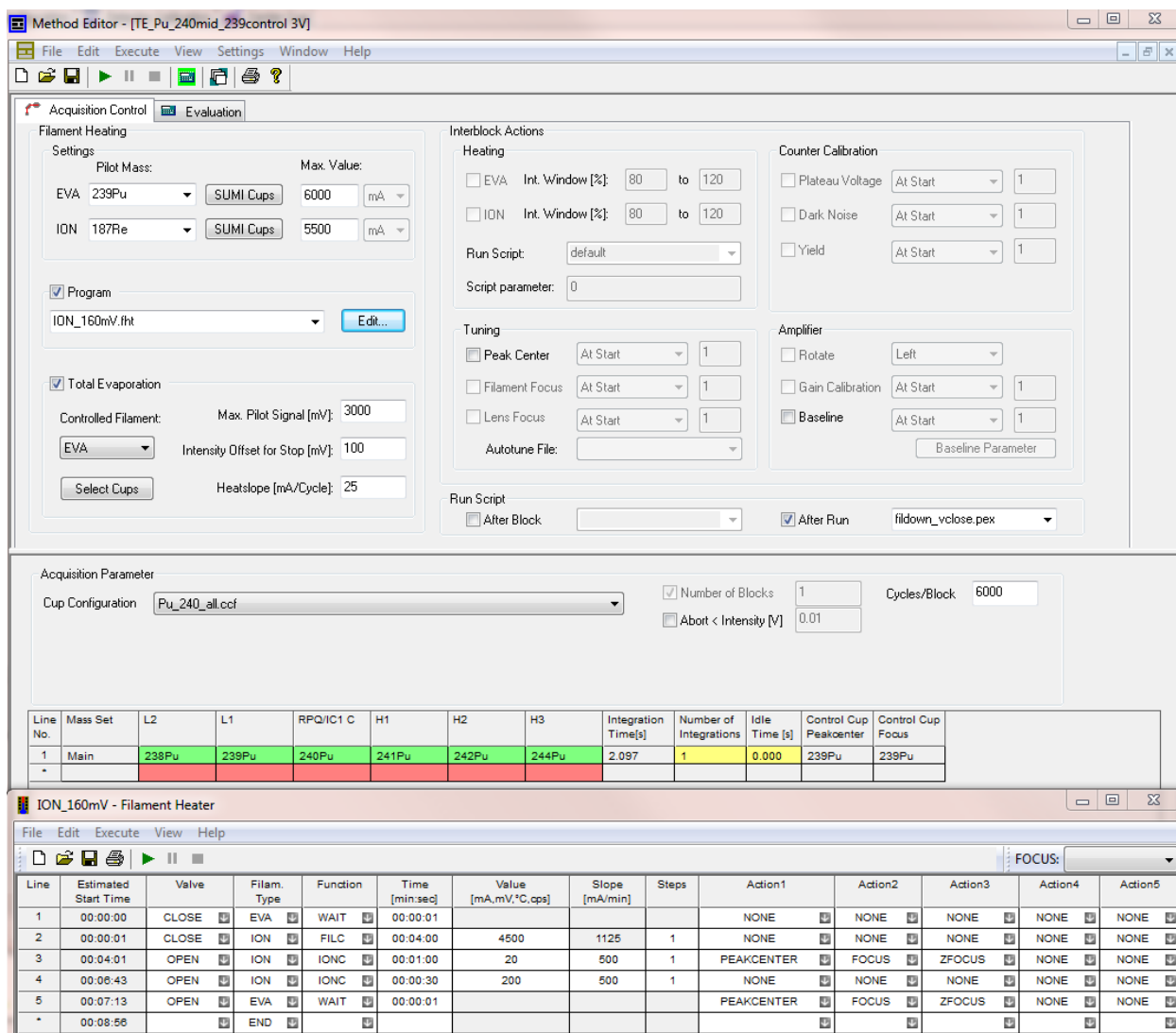


Figure 4. The total evaporation method used for the isotopic analysis by TIMS. The heat profile is included with the method.



## 4.2 PU ANALYSIS USING MC-ICP-MS

### 4.2.1 MC-ICP-MS Analysis Sequence

The plutonium isotopic characterizations were performed via multiple collector inductively coupled plasma–mass spectrometry (MC-ICP-MS). The samples were analyzed in a single sequence spanning about 20 h. Within the sample sequence, each vial was analyzed non-sequentially seven times. The sequence was constructed using a standard bracketing method with quality control (QC) samples bracketing the unknown C137A samples (Figure 5). A hydride sample (“H”) was analyzed at the beginning and the end of the sequence, and the hydride ratio was averaged across the run. The control samples have the “C” designation, and “M” signifies mass bias or comparator. A wash time of 200 s was used to eliminate washout effects. The washout solutions were 5% HNO<sub>3</sub> + 0.01M HF, and the blank correction 2% HNO<sub>3</sub>. The washout and blanks both had an uptake time of 100 s to minimize memory effect before the sample. The samples, QC, and comparator samples had an uptake time of 100 s. This time considers a signal stability time of about 45 s, which is common for standard ICP-MS introduction systems. The method and acquisition parameters can be found in Figure 5.

The screenshot displays the software interface for setting up an MC-ICP-MS analysis sequence. The metadata section includes:

- Sequence Name: Pu\_Iso\_Apex\_Plus\_EHM DHS 11252019 29
- Start at Run Number: 1
- Date: 17 January 2023 10:10
- Operator: All
- Instrument: Neptune Plus
- Directory To Evaluate: c:\Neptune\User\Neptune\Data\PU\_Iso\_Apex\_P

Below the metadata is a table with 10 columns: Run Number, Sample Type, Sample ID, Filename, Description (Comments), Method File, Tune Parameter, Status, Rack Pos, Vial Pos, and Takeup Time. The table lists 48 runs, alternating between sample types (BLK, SMP, STD) and various sample IDs (e.g., 001\_BLK, 002\_BLK, 2M128Pul, 003\_2M128Pul, etc.). Each row includes a dropdown menu for the sample type and a status icon (e.g., Done, Error).

Figure 5. MC-ICP-MS sequence template for plutonium analysis.

## 4.2.2 Detector Configuration, Amplifiers, and Calibration

The baseline history was used to select the instrument amplifiers with the lowest standard deviation. The lowest deviation amplifier was used on the 241 faraday cup, and then 242, 244, 238, 240, and 239 faraday cup amplifiers were populated in that order. A mix of  $10^{11}$  and  $10^{13}$  amplifiers was selected for the MC-ICP-MS method. No amplifier rotation was applied. The faraday detector gain was electronically determined for 2.5 h using a 0.3333334 gain calibration card. This calibration was performed before the project sequences. The results were compared to the gain history to determine whether the values were within the history deviation. After the gain calibration, a baseline was conducted for 1,800 s. The baseline measurements were completed before each sequence. A mass calibration solution was run to complete a full mass calibration at the beginning of the project analyses (Figure 6). The instrument was calibrated using masses for lithium, sodium, iron, strontium, neodymium, hafnium, lead, uranium, UO, and UO<sub>2</sub>. During each sample analysis, plutonium was recalibrated.

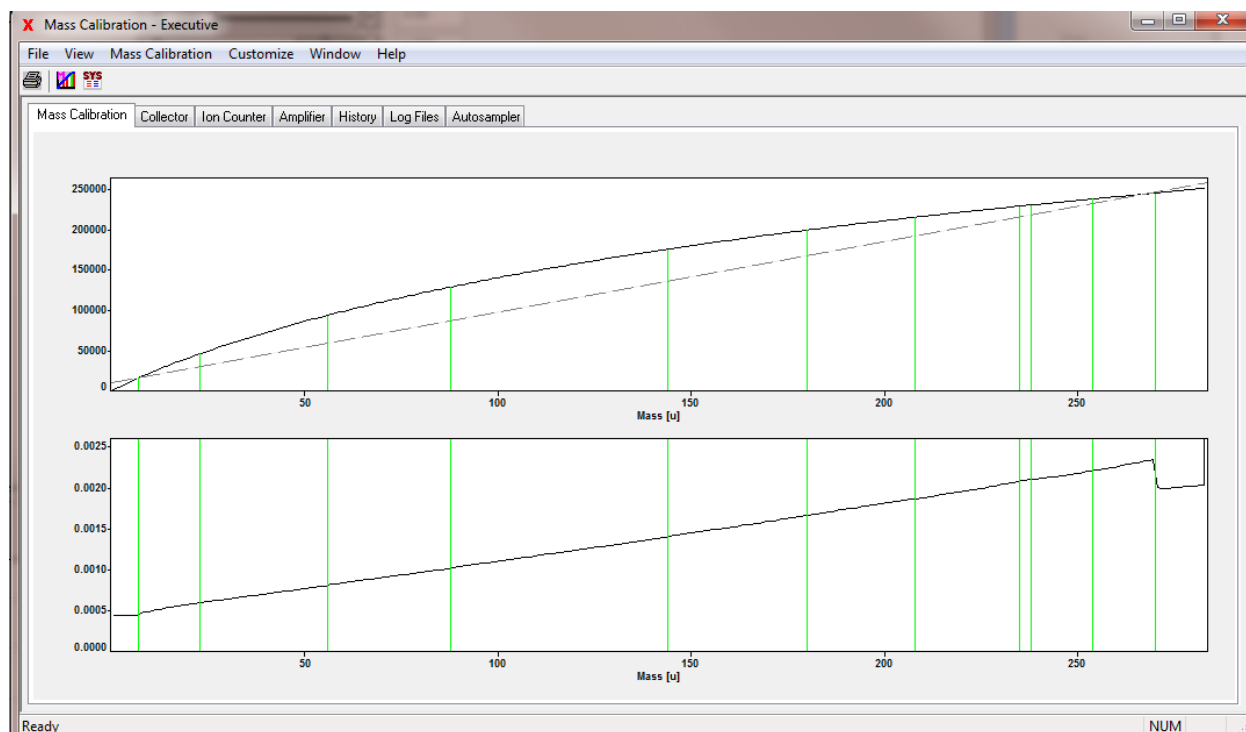


Figure 6. Mass calibration Neptune Plus.

## 4.2.3 Sample Analysis Method

Plutonium isotope ratios ( $^{238}\text{Pu}/^{239}\text{Pu}$ ,  $^{240}\text{Pu}/^{239}\text{Pu}$ ,  $^{241}\text{Pu}/^{239}\text{Pu}$ ,  $^{242}\text{Pu}/^{239}\text{Pu}$ ,  $^{244}\text{Pu}/^{239}\text{Pu}$ ) were measured via MC-ICP-MS. An aliquot from the purified stock solution was used to create a 4 ng solution with a volume of 2 mL. Using CRM 137 decay-corrected ratios as an example, total ion current of 4 V should yield 7 mV of mass 238, 1 V of mass 240, 16 mV of mass 241, and 46 mV of mass 242. These signal intensities should all be large enough to be placed on the faraday detector without needing a secondary electron multiplier. A 4 V 239 signal should yield a count rate of  $5 \times 10^{-6}$  V. This correction will be made with the secondary electron multiplier and by measuring  $^{241}\text{Pu}$  in two lines using the IC1 B and the center Faraday cup. The analyses were set up in two lines with five integrations on the first line and one integration on the second line. The integration time was set to 16.777 s. Each line was run in an alternating pattern making up one cycle and 10 cycles were run. Outliers were rejected based on two standard deviations of the individual

cycles. The sample mass bias was corrected using an exponential correction model based on the average  $^{242}\text{Pu}/^{239}\text{Pu}$  ratio in the CRM 128 comparator sample filaments.

### 4.3 PLUTONIUM ANALYSIS USING ALPHA SPECTROMETRY

#### 4.3.1 Sample Analysis Method

The activities of  $^{238}\text{Pu}$  and  $^{239+240}\text{Pu}$  were determined in the three units of C137A by means of direct coprecipitation of the plutonium with  $\text{CeF}_3$ . Because samples were pure plutonium ( $^{241}\text{Am}$  had recently been separated from  $^{241}\text{Pu}$ , as described in Section 3), an additional separation was not required. The  $\text{CeF}_3$  precipitation was prepared by spiking 10 mL of a 0.1 M HCl + 0.05 M HF + 0.05 M  $\text{TiCl}_3$  solution with 100  $\mu\text{L}$  of sample and 0.02 mL of  $^{242}\text{Pu}$  standard NIST 4334J-E (used as a tracer to monitor chemical recovery). To this solution, 50  $\mu\text{L}$  of Ce carrier (1000 mg/L) and 2 mL of concentrated HF was added, mixed, and allowed to sit for about 15 min. The precipitate was quantitatively transferred and filtered onto an Eichrom Resolve filter (preconditioned with EtOH). The filter was dried under vacuum and transferred to a stainless steel planchette for further drying under a heat lamp for about 15 min. Samples were taken to a count room for counting via alpha spectrometry.

The main purpose of the alpha spectrometry was to provide supporting data for the mass spectrometry measurements. The activity ratio of  $^{238}\text{Pu}$  isotope with respect to  $^{239}\text{Pu}$  was calculated and used to support the mass spectrometry measurements.

In addition to determining the plutonium isotope activities, the  $\text{CeF}_3$  direct precipitation method used precipitated all actinide elements. Thus, any potential actinide impurities present could have been determined. No actinides, other than plutonium, were present in the samples. This information can be used to help assign impurity values in the C137A standard.

#### 4.3.2 Quality Assurance

The alpha spectrometer detectors were calibrated using a mixed-energy alpha source from NIST-certified sources. The energy range was calibrated from 3 to 8 MeV. Efficiency calibrations for the detectors used the same NIST mixed-energy source. The detectors were passivated implanted planar silicon detectors. The counting efficiency of these detectors ranged from approximately 12% to 15%. The detectors are housed in an ORTEC DUO chamber within the ORTEC Ensemble, which is an integrated alpha spectrometer. ORTEC's AlphaVision software performed the data acquisition and analysis. The alpha detectors were checked using a pulsar to ensure proper working conditions, and the backgrounds were performed weekly.

## 5. RESULTS

### 5.1 ISOTOPIC DATA

Four turrets were analyzed on four separate days. The first three turrets were analyzed in November. At that time a bias in the  $^{241}\text{Pu}/^{239}\text{Pu}$  ratio was observed between vial 113 and the other two vials. A second sample fraction was pulled and purified to verify the ratio. The second sample solution did not display the same isotopic value. This observation was verified via MC-ICP-MS. The fourth turret was loaded with four additional vial 04 filaments, and eight additional vial 113 filaments along with CRM 128 and CRM 137 served as mass comparator and quality assurance samples. This analysis provided better results for the  $^{241}\text{Pu}/^{239}\text{Pu}$  ratio. No other ratios were perturbed, and all analysis results have been included.

Table 5 displays the 11 replicates TIMS measured for all ratios in vial 004. Table 6 displays the seven replicates MC-ICP-MS measured for all ratios in vial 004. The average  $^{240}\text{Pu}/^{239}\text{Pu}$  TIMS value was

0.240626 ± 0.000077 (2σ), and the average  $^{240}\text{Pu}/^{239}\text{Pu}$  MC-ICP-MS value was 0.240631 ± 0.000072 (2σ). The ratio plots of all replicates for each isotopes system are shown in Figure 7 through Figure 10. The analyzed values are plotted against the decay-corrected values for CRM 137. The guide to the expression of uncertainty in measurement (GUM) models and budgets are given in Appendix B. No  $^{238}\text{Pu}/^{239}\text{Pu}$  ratio was collected with MC-ICP-MS, due to the background of  $^{238}\text{U}$  in the system. Replicates 1-7, which corresponds to analysis dates October 25<sup>th</sup> - October 28<sup>th</sup>, were separated on October 12<sup>th</sup>, 2022, and replicates 8 -11 were separated on January 11<sup>th</sup>, 2023, and subsequently analyzed January 24<sup>th</sup>, 2023.

**Table 5. The isotopic values for vial 004 from all TIMS analyses**

| TIMS isotopic data      |           |                                   |                                   |                                   |                                   |                                   |               |
|-------------------------|-----------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|---------------|
| Replicate               | Sample ID | $^{238}\text{Pu}/^{239}\text{Pu}$ | $^{240}\text{Pu}/^{239}\text{Pu}$ | $^{241}\text{Pu}/^{239}\text{Pu}$ | $^{242}\text{Pu}/^{239}\text{Pu}$ | $^{244}\text{Pu}/^{239}\text{Pu}$ | Analysis date |
| 1                       | 202201875 | 0.0026347                         | 0.240611                          | 0.005108                          | 0.015573                          | 0.0000003                         | 10/25/2022    |
| 2                       | 202201875 | 0.0026353                         | 0.240631                          | 0.005106                          | 0.015578                          | 0.0000047                         | 10/25/2022    |
| 3                       | 202201875 | 0.0026362                         | 0.240662                          | 0.005107                          | 0.015585                          | 0.0000011                         | 10/25/2022    |
| 4                       | 202201875 | 0.0026398                         | 0.240614                          | 0.005180                          | 0.015573                          | 0.0000017                         | 10/26/2022    |
| 5                       | 202201875 | 0.0026369                         | 0.240641                          | 0.005105                          | 0.015577                          | 0.0000011                         | 10/26/2022    |
| 6                       | 202201875 | 0.0026350                         | 0.240576                          | 0.005110                          | 0.015565                          | 0.0000019                         | 10/28/2022    |
| 7                       | 202201875 | 0.0026529                         | 0.240595                          | 0.005194                          | 0.015578                          | 0.0000028                         | 10/28/2022    |
| 8                       | 202201875 | 0.0026342                         | 0.240633                          | 0.005047                          | 0.015579                          | -0.0000009                        | 1/24/2023     |
| 9                       | 202201875 | 0.0026331                         | 0.240636                          | 0.005054                          | 0.015579                          | -0.0000044                        | 1/24/2023     |
| 10                      | 202201875 | 0.0026345                         | 0.240640                          | 0.005040                          | 0.015581                          | -0.0000063                        | 1/24/2023     |
| 11                      | 202201875 | 0.0026346                         | 0.240649                          | 0.005042                          | 0.015586                          | -0.0000032                        | 1/24/2023     |
| <b>Average</b>          |           | 0.0026370                         | 0.240626                          | 0.005099                          | 0.0155776                         | -0.0000001                        | —             |
| <b>Uncertainty (2σ)</b> |           | 0.0000053                         | 0.000077                          | 0.000034                          | 0.0000067                         | 0.0000033                         | —             |

**Table 6. The isotopic values for vial 004 from all MC-ICP-MS analyses**

| MC-ICP-MS isotopic data |              |                                   |                                   |                                   |                                   |                                   | Analysis date |
|-------------------------|--------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|---------------|
| Replicate               | Sample ID    | $^{238}\text{Pu}/^{239}\text{Pu}$ | $^{240}\text{Pu}/^{239}\text{Pu}$ | $^{241}\text{Pu}/^{239}\text{Pu}$ | $^{242}\text{Pu}/^{239}\text{Pu}$ | $^{244}\text{Pu}/^{239}\text{Pu}$ | Analysis date |
| 12                      | 009_21875PuI | —                                 | 0.2406307                         | 0.005071437                       | 0.015596134                       | $-6.6207 \times 10^{-6}$          | 11/22/2022    |
| 13                      | 015_21875PuI | —                                 | 0.240608131                       | 0.005110372                       | 0.015576855                       | $1.07696 \times 10^{-5}$          | 11/22/2022    |
| 14                      | 018_21875PuI | —                                 | 0.240640078                       | 0.005089841                       | 0.015556068                       | $-2.3424 \times 10^{-5}$          | 11/22/2022    |
| 15                      | 024_21875PuI | —                                 | 0.240637052                       | 0.005115536                       | 0.015576865                       | $6.43469 \times 10^{-7}$          | 11/22/2022    |
| 16                      | 027_21875PuI | —                                 | 0.240630755                       | 0.005117414                       | 0.015552021                       | $1.25449 \times 10^{-8}$          | 11/22/2022    |
| 17                      | 033_21875PuI | —                                 | 0.240620868                       | 0.005114397                       | 0.015577411                       | $9.1276 \times 10^{-6}$           | 11/22/2022    |
| 18                      | 042_21875PuI | —                                 | 0.240649037                       | 0.005114528                       | 0.015572375                       | $-3.4938 \times 10^{-7}$          | 11/22/2022    |
| <b>Average</b>          |              | —                                 | 0.240631                          | 0.005105                          | 0.015573                          | -0.0000014                        | —             |
| <b>Uncertainty (2σ)</b> |              | —                                 | 0.000072                          | 0.000037                          | 0.000042                          | 0.0000114                         | —             |

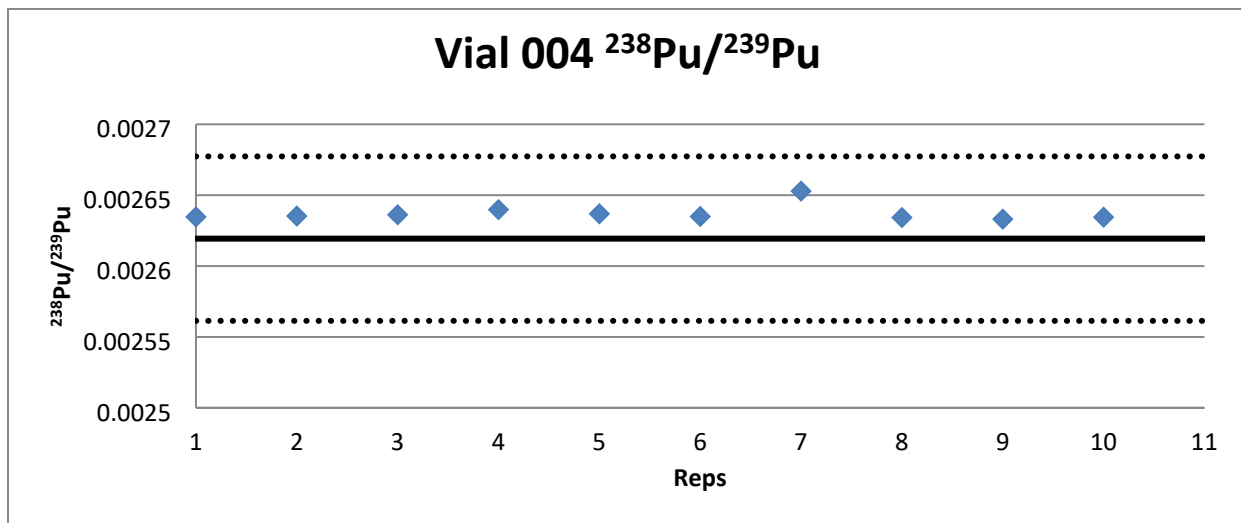


Figure 7. Replicate values of  $^{238}\text{Pu}/^{239}\text{Pu}$  in vial 004 using TIMS, plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.

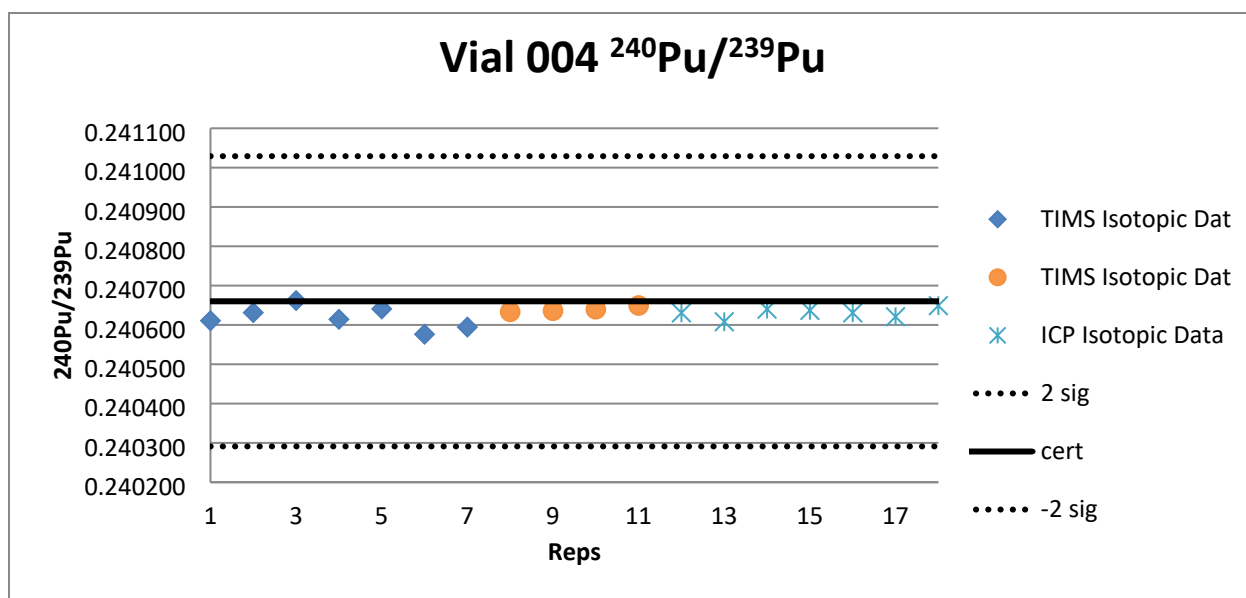


Figure 8. Replicate values of  $^{240}\text{Pu}/^{239}\text{Pu}$  in vial 004 using TIMS and MC-ICP-MS, plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.

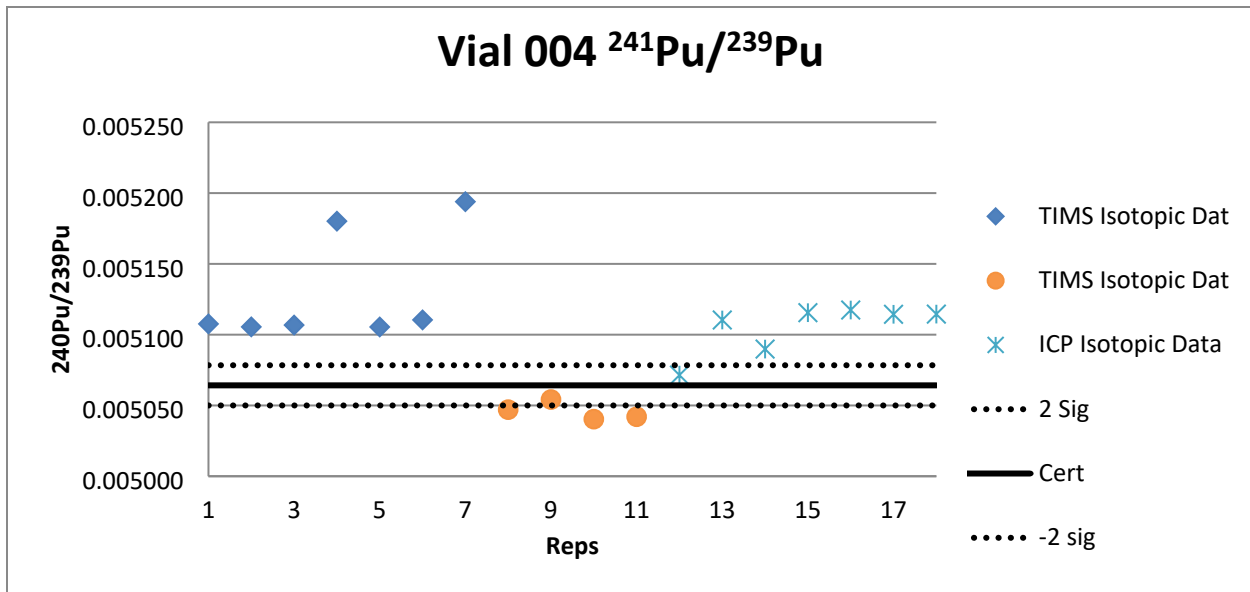


Figure 9. Replicate values of  $^{241}\text{Pu}/^{239}\text{Pu}$  in vial 004 using TIMS and MC-ICP-MS, plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.

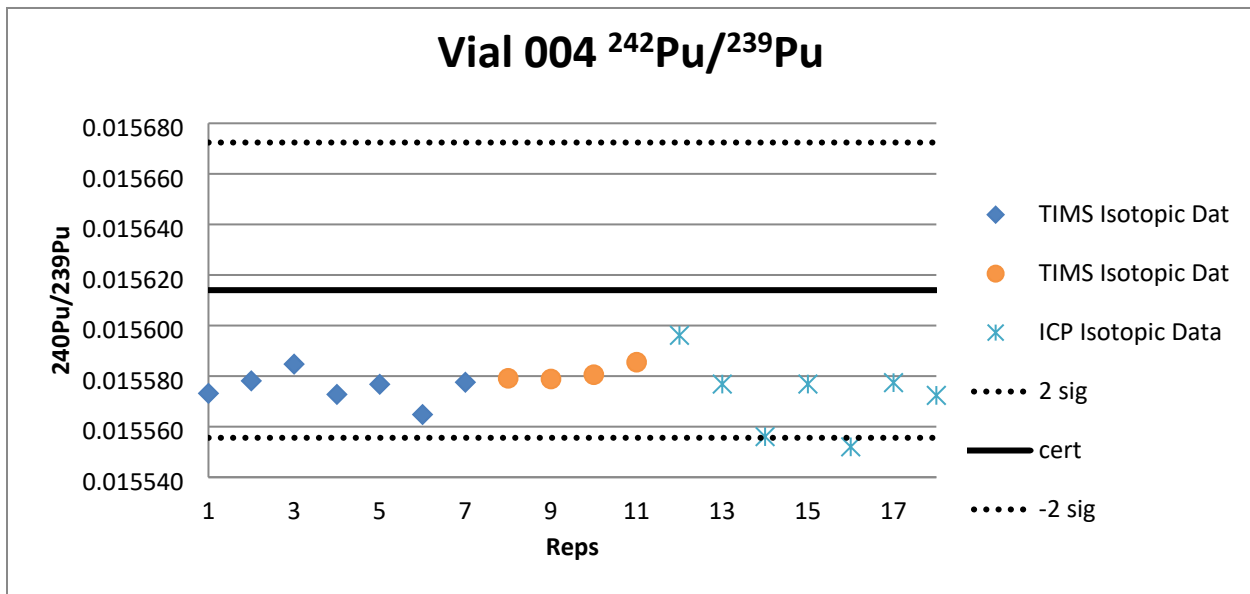


Figure 10. Replicate values of  $^{242}\text{Pu}/^{239}\text{Pu}$  in vial 004 using TIMS and MC-ICP-MS, plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.

Table 7 displays the seven replicates TIMS measured for all ratios in vial 052. Table 8 displays the seven replicates MC-ICP-MS measured for all ratios in vial 052. The average  $^{240}\text{Pu}/^{239}\text{Pu}$  TIMS value was  $0.240627 \pm 0.000078$  ( $2\sigma$ ), and the average  $^{240}\text{Pu}/^{239}\text{Pu}$  MC-ICP-MS value was  $0.240623 \pm 0.000072$  ( $2\sigma$ ). The ratio plots of all replicates for each isotopes system are shown in Figure 11 through Figure 14. The analyzed values are plotted against the decay-corrected values for CRM 137. The GUM models and budgets are given in Appendix C. Replicates 1-7, which corresponds to analysis dates October 25<sup>th</sup> - October 28<sup>th</sup>, were separated on October 12<sup>th</sup>, 2022

**Table 7. The isotopic values for vial 052 from all TIMS analyses**

| TIMS isotopic data      |           |                                      |                                      |                                      |                                      |                                      |               |
|-------------------------|-----------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Replicate               | Sample ID | <sup>238</sup> Pu/ <sup>239</sup> Pu | <sup>240</sup> Pu/ <sup>239</sup> Pu | <sup>241</sup> Pu/ <sup>239</sup> Pu | <sup>242</sup> Pu/ <sup>239</sup> Pu | <sup>244</sup> Pu/ <sup>239</sup> Pu | Analysis date |
| 1                       | 202201876 | 0.0026458                            | 0.240627                             | 0.005113                             | 0.0155755                            | $4.7111 \times 10^{-7}$              | 10/25/2022    |
| 2                       | 202201876 | 0.0026572                            | 0.240621                             | 0.005112                             | 0.0155782                            | $2.17145 \times 10^{-7}$             | 10/25/2022    |
| 3                       | 202201876 | 0.0026337                            | 0.240620                             | 0.005108                             | 0.0155758                            | $4.14565 \times 10^{-7}$             | 10/25/2022    |
| 4                       | 202201876 | 0.0026346                            | 0.240592                             | 0.005110                             | 0.0155684                            | $5.03829 \times 10^{-7}$             | 10/26/2022    |
| 5                       | 202201876 | 0.0026342                            | 0.240677                             | 0.005108                             | 0.0155850                            | $-1.03829 \times 10^{-7}$            | 10/26/2022    |
| 6                       | 202201876 | 0.0026414                            | 0.240631                             | 0.005114                             | 0.0155781                            | $2.00646 \times 10^{-6}$             | 10/28/2022    |
| 7                       | 202201876 | 0.0026611                            | 0.240623                             | 0.005111                             | 0.0155789                            | $1.32822 \times 10^{-6}$             | 10/28/2022    |
| <b>Average</b>          |           | 0.0026440                            | 0.240627                             | 0.005111                             | 0.0155771                            | 0.00000069                           | —             |
| <b>Uncertainty (2σ)</b> |           | 0.0000095                            | 0.000078                             | 0.000014                             | 0.0000068                            | 0.00000072                           | —             |

**Table 8. The isotopic values for vial 052 from all MC-ICP-MS analyses**

| ICP Isotopic Data       |              |                                      |                                      |                                      |                                      |                                      |               |
|-------------------------|--------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Replicate               | Sample ID    | <sup>238</sup> Pu/ <sup>239</sup> Pu | <sup>240</sup> Pu/ <sup>239</sup> Pu | <sup>241</sup> Pu/ <sup>239</sup> Pu | <sup>242</sup> Pu/ <sup>239</sup> Pu | <sup>244</sup> Pu/ <sup>239</sup> Pu | Analysis Date |
| 8                       | 045_21876PuI | —                                    | 0.240640                             | 0.005106                             | 0.015564                             | $9.43223 \times 10^{-6}$             | 11/22/2022    |
| 9                       | 051_21876PuI | —                                    | 0.240596                             | 0.005103                             | 0.015551                             | $-2.27107 \times 10^{-5}$            | 11/22/2022    |
| 10                      | 054_21876PuI | —                                    | 0.240609                             | 0.005099                             | 0.015570                             | $-6.43841 \times 10^{-8}$            | 11/22/2022    |
| 11                      | 060_21876PuI | —                                    | 0.240628                             | 0.005118                             | 0.015597                             | $1.40812 \times 10^{-5}$             | 11/22/2022    |
| 12                      | 063_21876PuI | —                                    | 0.240639                             | 0.005125                             | 0.015585                             | $-2.25803 \times 10^{-5}$            | 11/22/2022    |
| 13                      | 072_21876PuI | —                                    | 0.240631                             | 0.005091                             | 0.015586                             | $8.79275 \times 10^{-6}$             | 11/22/2022    |
| 14                      | 078_21876PuI | —                                    | 0.240619                             | 0.005097                             | 0.015546                             | $7.86452 \times 10^{-6}$             | 11/22/2022    |
| <b>Average</b>          |              | —                                    | 0.240623                             | 0.005105                             | 0.015571                             | -0.000001                            | —             |
| <b>Uncertainty (2σ)</b> |              | —                                    | 0.000072                             | 0.000036                             | 0.000043                             | 0.000016                             | —             |

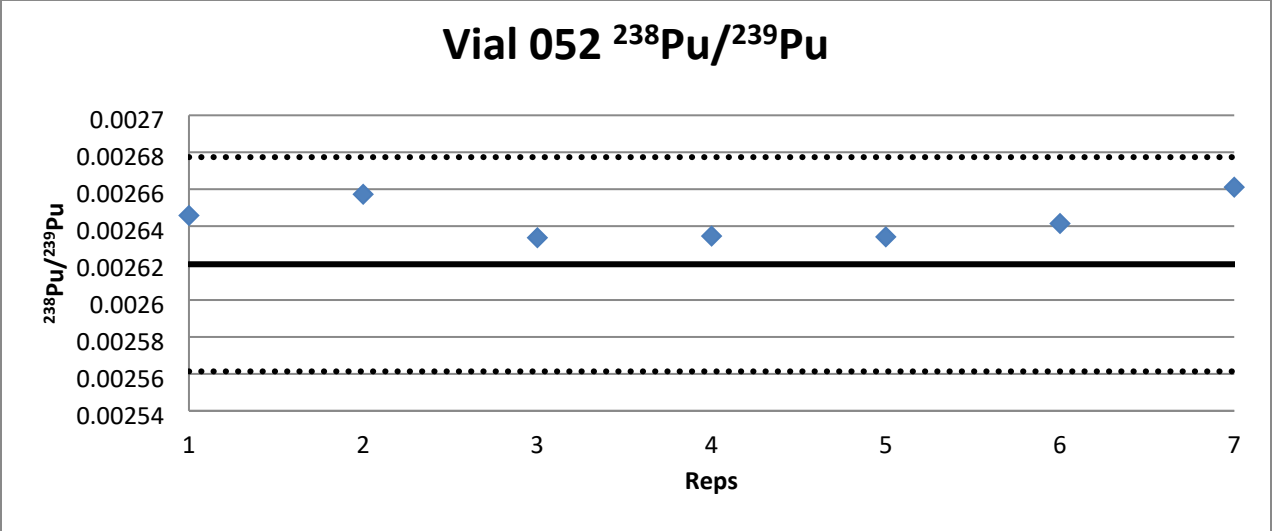


Figure 11. Replicate values of  $^{238}\text{Pu}/^{239}\text{Pu}$  in vial 052 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.

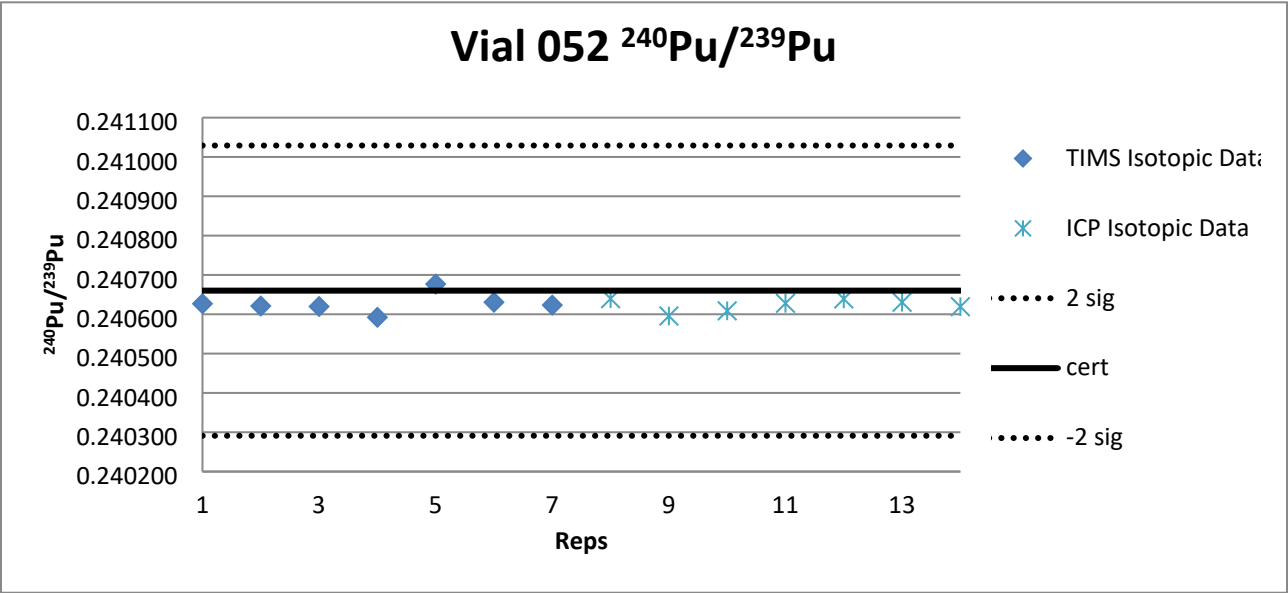
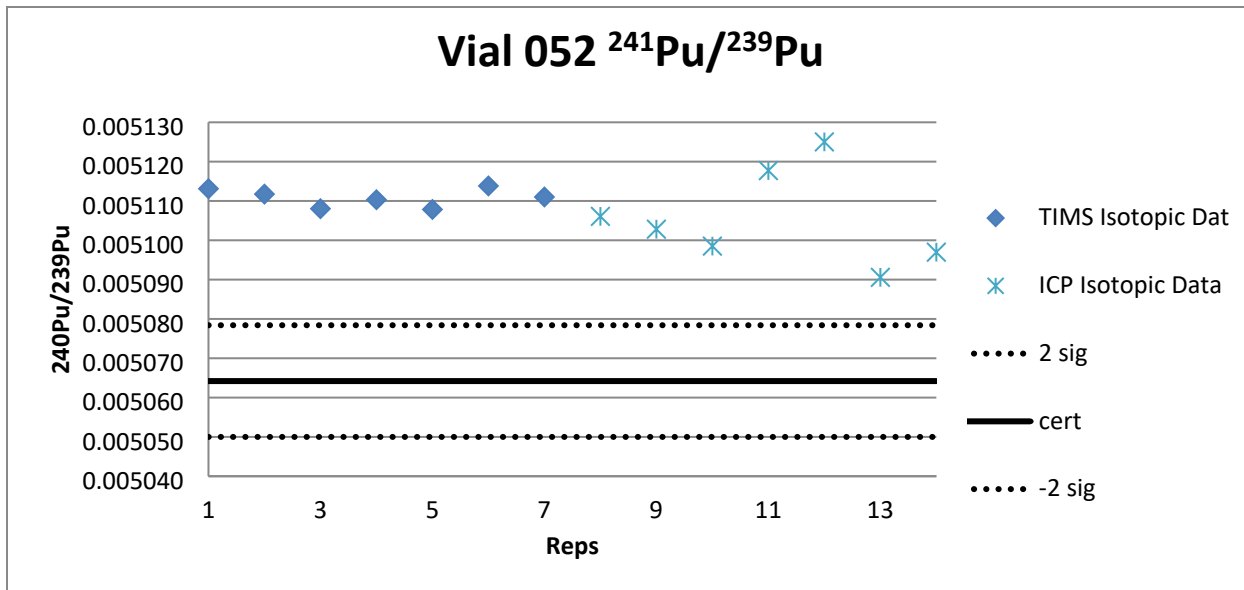
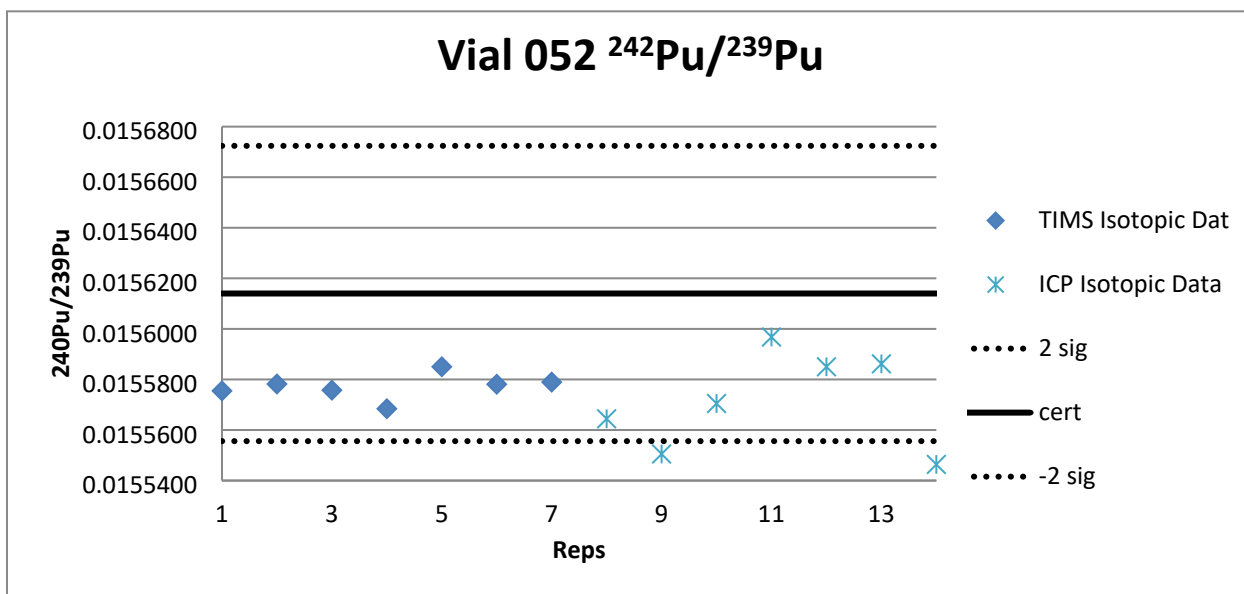


Figure 12. Replicate values of  $^{240}\text{Pu}/^{239}\text{Pu}$  in vial 052 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.





**Figure 13. Replicate values of  $^{241}\text{Pu}/^{239}\text{Pu}$  in vial 052 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.**



**Figure 14. Replicate values of  $^{242}\text{Pu}/^{239}\text{Pu}$  in vial 052 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.**

Table 9 displays the 15 replicates TIMS measured for all ratios in vial 113. Table 10 displays the seven replicates MC-ICP-MS measured for all ratios in vial 113. The average  $^{240}\text{Pu}/^{239}\text{Pu}$  TIMS value was  $0.240626 \pm 0.000076$  ( $2\sigma$ ), and the average  $^{240}\text{Pu}/^{239}\text{Pu}$  MC-ICP-MS value was  $0.240635 \pm 0.000072$  ( $2\sigma$ ). The ratio plots of all replicates for each isotopes system are shown in Figure 15 through Figure 18. The analyzed values are plotted against the decay-corrected values for CRM 137. The GUM models and budgets are given in Appendix D. Replicates 1-7, which corresponds to analysis dates October 25<sup>th</sup> - October 28<sup>th</sup>, were separated on October 12<sup>th</sup>, 2022. While the other replicates were separated on January 11<sup>th</sup>, 2023, and subsequently analyzed January 24<sup>th</sup>, 2023.

**Table 9. The isotopic values for vial 113 from all TIMS analyses**

| TIMS isotopic data      |           |                                      |                                      |                                      |                                      |                                      |               |
|-------------------------|-----------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Replicate               | Sample ID | <sup>238</sup> Pu/ <sup>239</sup> Pu | <sup>240</sup> Pu/ <sup>239</sup> Pu | <sup>241</sup> Pu/ <sup>239</sup> Pu | <sup>242</sup> Pu/ <sup>239</sup> Pu | <sup>244</sup> Pu/ <sup>239</sup> Pu | Analysis date |
| 1                       | 202201877 | 0.002640                             | 0.240615                             | 0.005180                             | 0.015573                             | 1.65257 × 10 <sup>-6</sup>           | 10/25/2022    |
| 2                       | 202201877 | 0.002637                             | 0.240618                             | 0.005170                             | 0.015570                             | -8.60144 × 10 <sup>-7</sup>          | 10/25/2022    |
| 3                       | 202201877 | 0.002634                             | 0.240617                             | 0.005167                             | 0.015573                             | -8.88115E-07                         | 10/25/2022    |
| 4                       | 202201877 | 0.002644                             | 0.240614                             | 0.005180                             | 0.015573                             | 1.65256 × 10 <sup>-6</sup>           | 10/26/2022    |
| 5                       | 202201877 | 0.002660                             | 0.240641                             | 0.005162                             | 0.015578                             | -8.04512 × 10 <sup>-7</sup>          | 10/26/2022    |
| 6                       | 202201877 | 0.002643                             | 0.240620                             | 0.005182                             | 0.015576                             | 5.03829 × 10 <sup>-7</sup>           | 10/26/2022    |
| 7                       | 202201877 | 0.002777                             | 0.240612                             | 0.005193                             | 0.015576                             | 2.64673 × 10 <sup>-6</sup>           | 10/28/2022    |
| 8                       | 202201877 | 0.002632                             | 0.240589                             | 0.005075                             | 0.015569                             | 1.37884 × 10 <sup>-6</sup>           | 1/24/2023     |
| 9                       | 202201877 | 0.002638                             | 0.240639                             | 0.005076                             | 0.015576                             | -8.59367 × 10 <sup>-6</sup>          | 1/24/2023     |
| 10                      | 202201877 | 0.002634                             | 0.240626                             | 0.005075                             | 0.015581                             | -4.07069 × 10 <sup>-6</sup>          | 1/24/2023     |
| 11                      | 202201877 | 0.002634                             | 0.240641                             | 0.005074                             | 0.015580                             | -1.38997 × 10 <sup>-5</sup>          | 1/24/2023     |
| 12                      | 202201877 | 0.002643                             | 0.240632                             | 0.005074                             | 0.015577                             | -2.24508 × 10 <sup>-5</sup>          | 1/24/2023     |
| 13                      | 202201877 | 0.002632                             | 0.240615                             | 0.005070                             | 0.015577                             | -1.09625 × 10 <sup>-6</sup>          | 1/24/2023     |
| 14                      | 202201877 | 0.002641                             | 0.240644                             | 0.005069                             | 0.015595                             | -4.47132 × 10 <sup>-6</sup>          | 1/24/2023     |
| 15                      | 202201877 | 0.002634                             | 0.240660                             | 0.005075                             | 0.015589                             | -7.03564 × 10 <sup>-6</sup>          | 1/24/2023     |
| <b>Average</b>          |           | 0.002648                             | 0.240626                             | 0.005121                             | 0.015578                             | -0.0000038                           | —             |
| <b>Uncertainty (2σ)</b> |           | 0.000019                             | 0.000076                             | 0.000031                             | 0.000067                             | 0.0000069                            | —             |

**Table 10. The isotopic values for vial 113 from all MC-ICP-MS analyses**

| ICP isotopic data       |              |                                      |                                      |                                      |                                      |                                      |               |
|-------------------------|--------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Replicate               | Sample ID    | <sup>238</sup> Pu/ <sup>239</sup> Pu | <sup>240</sup> Pu/ <sup>239</sup> Pu | <sup>241</sup> Pu/ <sup>239</sup> Pu | <sup>242</sup> Pu/ <sup>239</sup> Pu | <sup>244</sup> Pu/ <sup>239</sup> Pu | Analysis date |
| 16                      | 081_21877PuI | —                                    | 0.240655                             | 0.005036                             | 0.015617                             | 2.43393 × 10 <sup>-5</sup>           | 11/22/2022    |
| 17                      | 087_21877PuI | —                                    | 0.240638                             | 0.005101                             | 0.015537                             | 2.0161 × 10 <sup>-5</sup>            | 11/22/2022    |
| 18                      | 090_21877PuI | —                                    | 0.240638                             | 0.005106                             | 0.015587                             | 3.63947 × 10 <sup>-6</sup>           | 11/22/2022    |
| 19                      | 096_21877PuI | —                                    | 0.240643                             | 0.005101                             | 0.015600                             | -1.33184 × 10 <sup>-5</sup>          | 11/22/2022    |
| 20                      | 099_21877PuI | —                                    | 0.240644                             | 0.005069                             | 0.015595                             | 3.80158 × 10 <sup>-6</sup>           | 11/22/2022    |
| 21                      | 105_21877PuI | —                                    | 0.240611                             | 0.005085                             | 0.015571                             | 1.60763 × 10 <sup>-6</sup>           | 11/22/2022    |
| 22                      | 108_21877PuI | —                                    | 0.240617                             | 0.005102                             | 0.015589                             | -2.21113 × 10 <sup>-5</sup>          | 11/22/2022    |
| <b>Average</b>          |              | —                                    | 0.240635                             | 0.005086                             | 0.015585                             | 0.0000026                            | —             |
| <b>Uncertainty (2σ)</b> |              | —                                    | 0.000072                             | 0.000040                             | 0.000044                             | 0.0000166                            | —             |

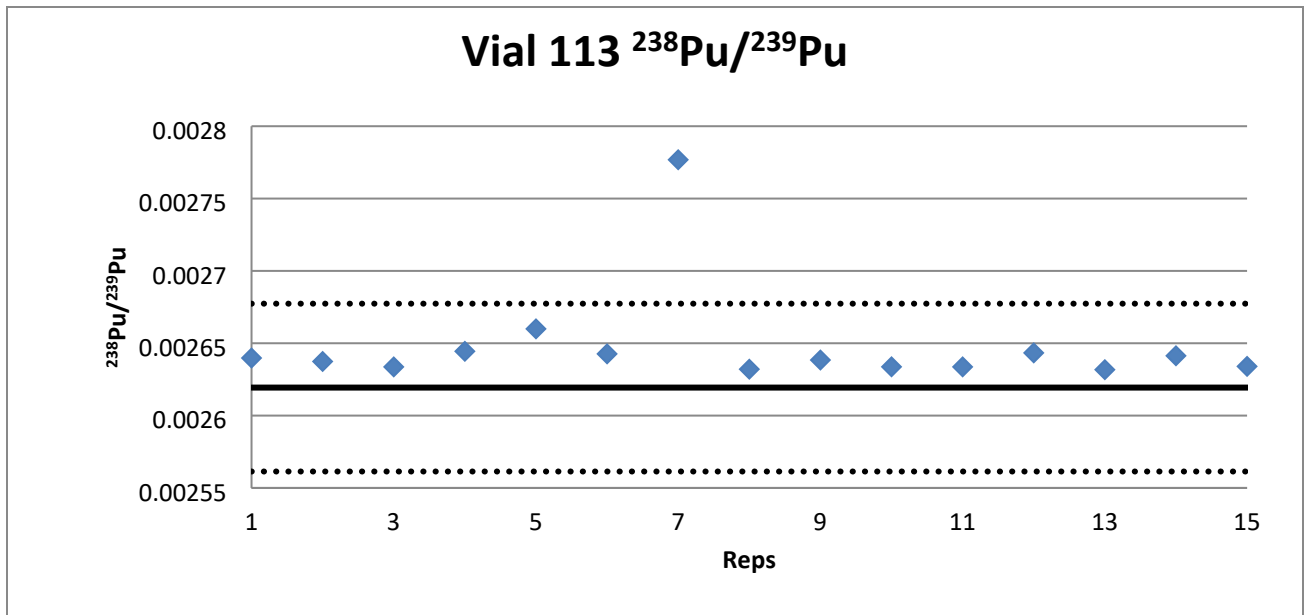


Figure 15. Replicate values of  $^{238}\text{Pu}/^{239}\text{Pu}$  in vial 113 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.

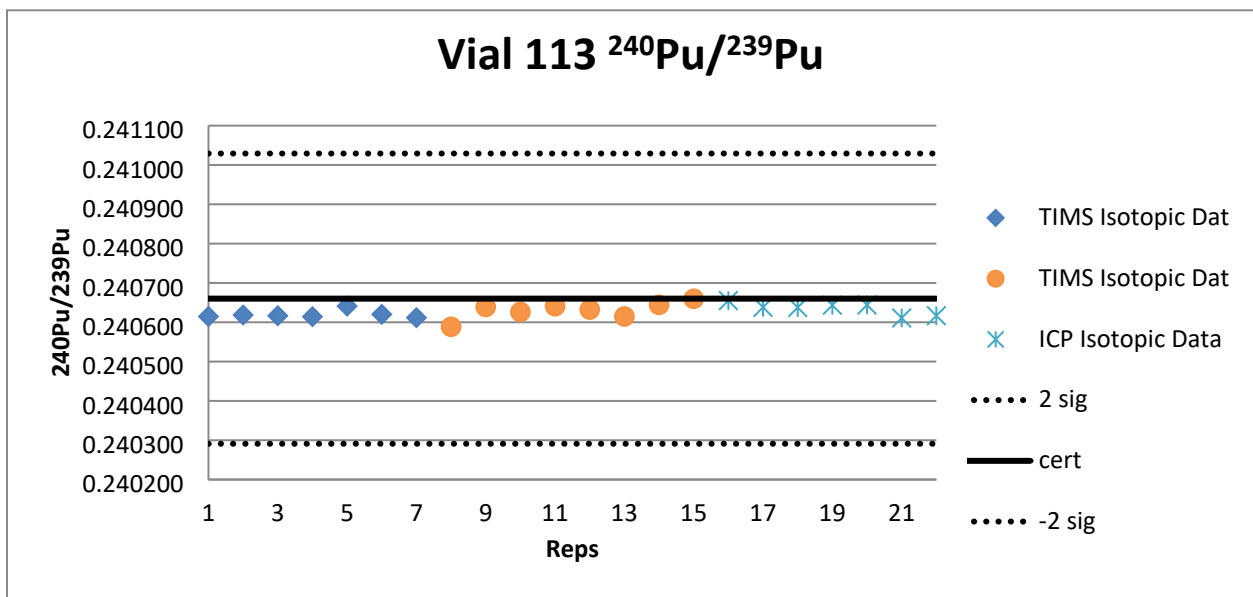
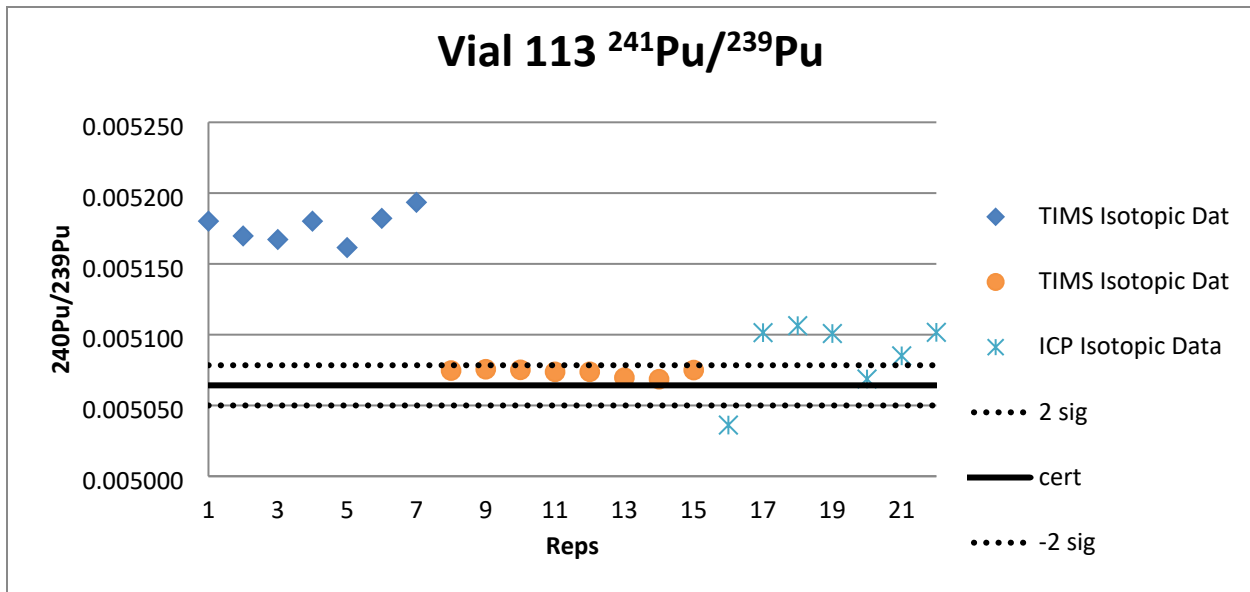
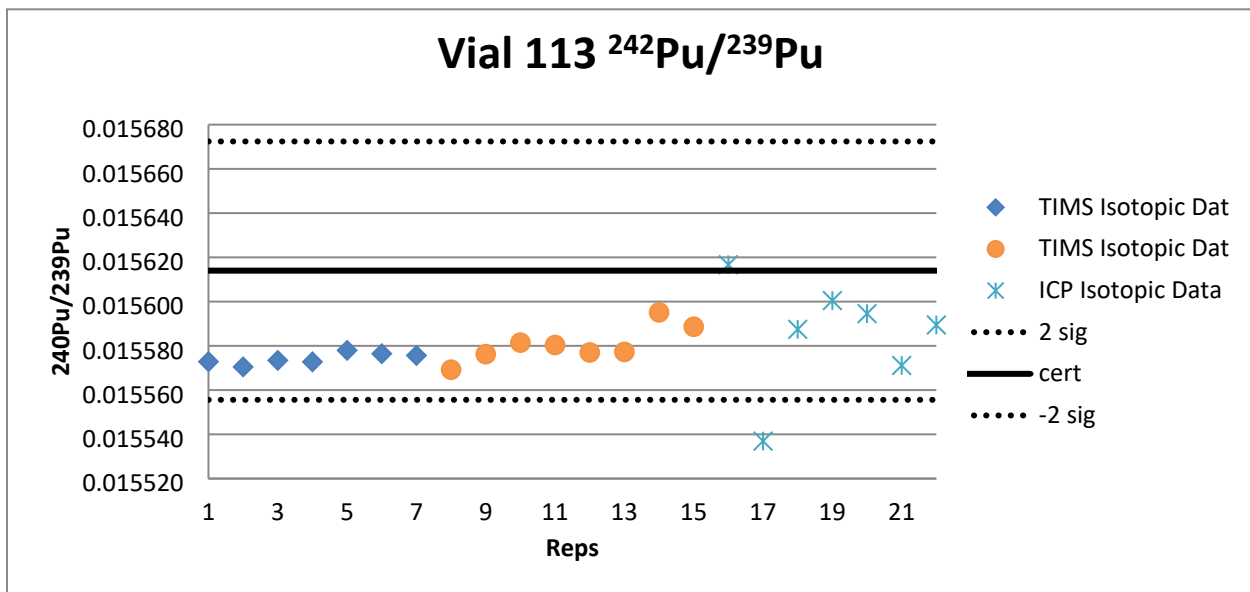


Figure 16. Replicate values of  $^{240}\text{Pu}/^{239}\text{Pu}$  in vial 113 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.



**Figure 17. Replicate values of  $^{241}\text{Pu}/^{239}\text{Pu}$  in vial 113 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.**



**Figure 18. Replicate values of  $^{242}\text{Pu}/^{239}\text{Pu}$  in vial 113 plotted against CRM 137 decay-corrected values. The dashed line represents the expanded uncertainty ( $k=2$ ) from the original certificate of analysis for CRM 137.**

Table 11 displays the all replicates measured by TIMS and MC-ICP-MS. The average  $^{240}\text{Pu}/^{239}\text{Pu}$  value was  $0.240628 \pm 0.000075$  ( $2\sigma$ ). The number of replicate measurements was 54. The GUM models and budgets are given in Appendix E.

**Table 11. The isotopic values for vials 004, 052, and 113 from all analyses**

| Replicate analysis for vials 004, 052, and 113 |               |                                      |                                      |                                      |                                      |                                      |               |
|--|---------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------|
| Replicate                                      | Sample ID     | <sup>238</sup> Pu/ <sup>239</sup> Pu | <sup>240</sup> Pu/ <sup>239</sup> Pu | <sup>241</sup> Pu/ <sup>239</sup> Pu | <sup>242</sup> Pu/ <sup>239</sup> Pu | <sup>244</sup> Pu/ <sup>239</sup> Pu | Analysis date |
| 1  | TIMS vial 04  | 0.002635                             | 0.240611                             | 0.005108                             | 0.015573                             | 0.000000                             | 10/25/2022    |
| 2  | TIMS vial 04  | 0.002635                             | 0.240631                             | 0.005106                             | 0.015578                             | 0.000005                             | 10/25/2022    |
| 3  | TIMS vial 04  | 0.002636                             | 0.240662                             | 0.005107                             | 0.015585                             | 0.000001                             | 10/25/2022    |
| 4  | TIMS vial 04  | 0.002640                             | 0.240614                             | 0.005180                             | 0.015573                             | 0.000002                             | 10/26/2022    |
| 5  | TIMS vial 04  | 0.002637                             | 0.240641                             | 0.005105                             | 0.015577                             | 0.000001                             | 10/26/2022    |
| 6  | TIMS vial 04  | 0.002635                             | 0.240576                             | 0.005110                             | 0.015565                             | 0.000002                             | 10/28/2022    |
| 7  | TIMS vial 04  | 0.002653                             | 0.240595                             | 0.005194                             | 0.015578                             | 0.000003                             | 10/28/2022    |
| 8  | TIMS vial 04  | 0.002634                             | 0.240633                             | 0.005047                             | 0.015579                             | -0.000001                            | 1/24/2023     |
| 9  | TIMS vial 04  | 0.002633                             | 0.240636                             | 0.005054                             | 0.015579                             | -0.000004                            | 1/24/2023     |
| 10   | TIMS vial 04  | 0.002634                             | 0.240640                             | 0.005040                             | 0.015581                             | -0.000006                            | 1/24/2023     |
| 11   | TIMS vial 04  | 0.002635                             | 0.240649                             | 0.005042                             | 0.015586                             | -0.000003                            | 1/24/2023     |
| 12   | TIMS vial 52  | 0.002646                             | 0.240627                             | 0.005113                             | 0.015575                             | 0.000000                             | 10/25/2022    |
| 13   | TIMS vial 52  | 0.002657                             | 0.240621                             | 0.005112                             | 0.015578                             | 0.000000                             | 10/25/2022    |
| 14   | TIMS vial 52  | 0.002634                             | 0.240620                             | 0.005108                             | 0.015576                             | 0.000000                             | 10/25/2022    |
| 15   | TIMS vial 52  | 0.002635                             | 0.240592                             | 0.005110                             | 0.015568                             | 0.000001                             | 10/26/2022    |
| 16   | TIMS vial 52  | 0.002634                             | 0.240677                             | 0.005108                             | 0.015585                             | 0.000000                             | 10/26/2022    |
| 17   | TIMS vial 52  | 0.002641                             | 0.240631                             | 0.005114                             | 0.015578                             | 0.000002                             | 10/28/2022    |
| 18   | TIMS vial 52  | 0.002661                             | 0.240623                             | 0.005111                             | 0.015579                             | 0.000001                             | 10/28/2022    |
| 19   | TIMS vial 113 | 0.002640                             | 0.240615                             | 0.005180                             | 0.015573                             | 0.000002                             | 10/25/2022    |
| 20   | TIMS vial 113 | 0.002637                             | 0.240618                             | 0.005170                             | 0.015570                             | -0.000001                            | 10/25/2022    |
| 21   | TIMS vial 113 | 0.002634                             | 0.240617                             | 0.005167                             | 0.015573                             | -0.000001                            | 10/25/2022    |
| 22   | TIMS vial 113 | 0.002644                             | 0.240614                             | 0.005180                             | 0.015573                             | 0.000002                             | 10/26/2022    |
| 23   | TIMS vial 113 | 0.002660                             | 0.240641                             | 0.005162                             | 0.015578                             | -0.000001                            | 10/26/2022    |
| 24   | TIMS vial 113 | 0.002643                             | 0.240620                             | 0.005182                             | 0.015576                             | 0.000001                             | 10/26/2022    |
| 25   | TIMS vial 113 | 0.002777                             | 0.240612                             | 0.005193                             | 0.015576                             | 0.000003                             | 10/28/2022    |
| 26   | TIMS vial 113 | 0.002632                             | 0.240589                             | 0.005075                             | 0.015569                             | 0.000001                             | 1/24/2023     |
| 27   | TIMS vial 113 | 0.002638                             | 0.240639                             | 0.005076                             | 0.015576                             | -0.000009                            | 1/24/2023     |
| 28   | TIMS vial 113 | 0.002634                             | 0.240626                             | 0.005075                             | 0.015581                             | -0.000004                            | 1/24/2023     |
| 29   | TIMS vial 113 | 0.002634                             | 0.240641                             | 0.005074                             | 0.015580                             | -0.000014                            | 1/24/2023     |
| 30   | TIMS vial 113 | 0.002643                             | 0.240632                             | 0.005074                             | 0.015577                             | -0.000022                            | 1/24/2023     |
| 31   | TIMS vial 113 | 0.002632                             | 0.240615                             | 0.005070                             | 0.015577                             | -0.000001                            | 1/24/2023     |
| 32   | TIMS vial 113 | 0.002641                             | 0.240644                             | 0.005069                             | 0.015595                             | -0.000004                            | 1/24/2023     |
| 33   | TIMS vial 113 | 0.002634                             | 0.240660                             | 0.005075                             | 0.015589                             | -0.000007                            | 1/24/2023     |
| 34   | ICP vial 04   |                                      | 0.240631                             | 0.005071                             | 0.015596                             | -0.000007                            | 11/22/2022    |

|                         |              |                 |                 |                 |                  |                  |
|-------------------------|--------------|-----------------|-----------------|-----------------|------------------|------------------|
| 35                      | ICP vial 04  | 0.240608        | 0.005110        | 0.015577        | 0.000011         | 11/22/2022       |
| 36                      | ICP vial 04  | 0.240640        | 0.005090        | 0.015556        | -0.000023        | 11/22/2022       |
| 37                      | ICP vial 04  | 0.240637        | 0.005116        | 0.015577        | 0.000001         | 11/22/2022       |
| 38                      | ICP vial 04  | 0.240631        | 0.005117        | 0.015552        | 0.000000         | 11/22/2022       |
| 39                      | ICP vial 04  | 0.240621        | 0.005114        | 0.015577        | 0.000009         | 11/22/2022       |
| 40                      | ICP vial 04  | 0.240649        | 0.005115        | 0.015572        | 0.000000         | 11/22/2022       |
| 41                      | ICP vial 52  | 0.240640        | 0.005106        | 0.015564        | 0.000009         | 11/22/2022       |
| 42                      | ICP vial 52  | 0.240596        | 0.005103        | 0.015551        | -0.000023        | 11/22/2022       |
| 43                      | ICP vial 52  | 0.240609        | 0.005099        | 0.015570        | 0.000000         | 11/22/2022       |
| 44                      | ICP vial 52  | 0.240628        | 0.005118        | 0.015597        | 0.000014         | 11/22/2022       |
| 45                      | ICP vial 52  | 0.240639        | 0.005125        | 0.015585        | -0.000023        | 11/22/2022       |
| 46                      | ICP vial 52  | 0.240631        | 0.005091        | 0.015586        | 0.000009         | 11/22/2022       |
| 47                      | ICP vial 52  | 0.240619        | 0.005097        | 0.015546        | 0.000008         | 11/22/2022       |
| 48                      | ICP vial 113 | 0.240655        | 0.005036        | 0.015617        | 0.000024         | 11/22/2022       |
| 49                      | ICP vial 113 | 0.240638        | 0.005101        | 0.015537        | 0.000020         | 11/22/2022       |
| 50                      | ICP vial 113 | 0.240638        | 0.005106        | 0.015587        | 0.000004         | 11/22/2022       |
| 51                      | ICP vial 113 | 0.240643        | 0.005101        | 0.015600        | -0.000013        | 11/22/2022       |
| 52                      | ICP vial 113 | 0.240644        | 0.005069        | 0.015595        | 0.000004         | 11/22/2022       |
| 53                      | ICP vial 113 | 0.240611        | 0.005085        | 0.015571        | 0.000002         | 11/22/2022       |
| 54                      | ICP vial 113 | 0.240617        | 0.005102        | 0.015589        | -0.000022        | 11/22/2022       |
| <b>Average</b>          |              | <i>0.002644</i> | <i>0.240628</i> | <i>0.005107</i> | <i>0.0155771</i> | <i>-0.000001</i> |
| <b>Uncertainty (2σ)</b> |              | <i>0.000010</i> | <i>0.000075</i> | <i>0.000017</i> | <i>0.0000067</i> | <i>0.000010</i>  |

## 5.2 ALPHA DATA

Alpha Counting was used as a secondary verification for the  $^{238}\text{Pu}/^{239}\text{Pu}$ . The separation and plate produce a clean  $^{238}\text{Pu}$  spectrum, measured against a combined 239+240 signal. The ratio data is corrected using the average  $^{240}\text{Pu}/^{239}\text{Pu}$  for each vial to calculate the  $^{238}\text{Pu}/^{239}\text{Pu}$  ratio. Table 9 displays the 7 replicates for each vial of the 238/239 ratio. The average  $^{238}\text{Pu}/^{239}\text{Pu}$  ratio by alpha counting was  $0.0260 \pm 0.00037$  for vial 004,  $0.0266 \pm 0.00034$  for vial 052, and  $0.0261 \pm 0.00038$  for vial 113. The total averaged value for  $^{238}\text{Pu}/^{239}\text{Pu}$   $0.00262 \pm 0.00034$ . This average was derived with the removal of replicate 7 in vial 113. The ratio plots of all replicates for  $^{238}\text{Pu}/^{239}\text{Pu}$  are shown in Figure 18. The analyzed values are plotted against the decay-corrected values for CRM 137. The GUM models and budgets are given in Appendix F. While the other replicates were separated on January 11<sup>th</sup>, 2023,

| Alpha Counting Data |             |                                   |                  |               |
|---------------------|-------------|-----------------------------------|------------------|---------------|
| 238Pu/239Pu Value   |             |                                   |                  |               |
| Vial                | Sample ID   | $^{238}\text{Pu}/^{239}\text{Pu}$ | Uncertainty (2σ) | Analysis date |
| Vial004             | 221278-001A | 0.00257                           | 0.00037          | 2/8/2023      |
| Vial004             | 221278-001B | 0.00259                           | 0.00036          | 2/8/2023      |
| Vial004             | 221278-001C | 0.00280                           | 0.00041          | 2/8/2023      |
| Vial004             | 221278-001D | 0.00245                           | 0.00034          | 2/8/2023      |
| Vial004             | 221278-001E | 0.00248                           | 0.00036          | 2/8/2023      |
| Vial004             | 221278-001F | 0.00267                           | 0.00038          | 2/8/2023      |

|         |             |         |         |          |
|---------|-------------|---------|---------|----------|
| Vial004 | 221278-001G | 0.00265 | 0.00037 | 2/8/2023 |
| Vial052 | 221278-002A | 0.00250 | 0.00031 | 2/8/2023 |
| Vial052 | 221278-002B | 0.00265 | 0.00034 | 2/8/2023 |
| Vial052 | 221278-002C | 0.00276 | 0.00034 | 2/8/2023 |
| Vial052 | 221278-002D | 0.00268 | 0.00034 | 2/8/2023 |
| Vial052 | 221278-002E | 0.00264 | 0.00035 | 2/8/2023 |
| Vial052 | 221278-002F | 0.00269 | 0.00034 | 2/8/2023 |
| Vial052 | 221278-002G | 0.00271 | 0.00038 | 2/8/2023 |
| Vial113 | 221278-003A | 0.00265 | 0.00039 | 2/8/2023 |
| Vial113 | 221278-003B | 0.00249 | 0.00035 | 2/8/2023 |
| Vial113 | 221278-003C | 0.00261 | 0.00038 | 2/8/2023 |
| Vial113 | 221278-003D | 0.00248 | 0.00036 | 2/8/2023 |
| Vial113 | 221278-003E | 0.00275 | 0.00040 | 2/8/2023 |
| Vial113 | 221278-003F | 0.00270 | 0.00038 | 2/8/2023 |
| Vial113 | 221278-003G | 0.00357 | 0.00038 | 2/8/2023 |

Table 12. Displays all replicates measured by alpha counting. The average  $^{238}\text{Pu}/^{239}\text{Pu}$  value was  $0.00262 \pm 0.00034$  ( $2\sigma$ ). The number of replicate measurements was 21.

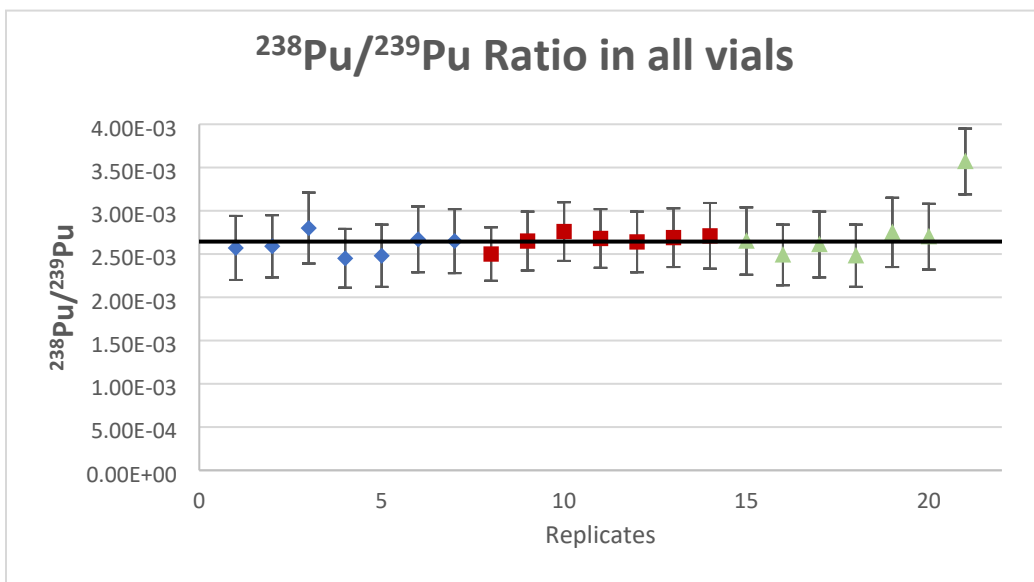


Figure 19. Replicate values of  $^{238}\text{Pu}/^{239}\text{Pu}$  by alpha counts for all the analyzed vials plotted against the average TIMS measured value.

## 6. REFERENCES

1. CSD-AM-CIMS-IN15, *Purification of U and/or Pu on 1-mL Eichrom UTEVA and/or TEVA Resin for Analysis by Mass Spectrometry*, Oak Ridge National Laboratory, Revision 1.
2. ASTM C1672-17, *Standard Test Method for Determination of Uranium or Plutonium Isotopic Composition or Concentration by the Total Evaporation Method Using a Thermal Ionization Mass Spectrometer*, 2017.





## **APPENDIX A. TIMS LOADING SHEETS**



### APPENDIX A. TIMS LOADING SHEETS

| Triton Loading Sheet |            |
|----------------------|------------|
| Date:                | 10/20/2022 |
| Turret #:            | Ø77        |
| Instrument           | SN630      |
| Operator:            | Hexel      |

| Turret Position | Sample ID | Element | Filament type (Re,W,Ta) (dbl single) | Loading Volume (uL) | Filament treatment                        |
|-----------------|-----------|---------|--------------------------------------|---------------------|---|
| ①               | 2M128P-I  | Pu      | Re, dbl                              | 0.9 uL              | Dry @ 0.6 A<br>14 sec, 1.5, 5 sec 2.0 sec |
| ②               | CRM 137   | ↓       | ↓                                    | ↓                   | ↓   |
| ③               | CRM 136   | ↓       | ↓                                    | ↓                   | ↓   |
| ④               | 1875      | ↓       | ↓                                    | ↓                   | ↓   |
| ⑤               | 202201876 |         |                                      |                     |   |
| ⑥               | 128       |         |                                      |                     |   |
| ⑦               | 202201877 |         |                                      |                     |   |
| ⑧               | 128       |         |                                      |                     |   |
| ⑨               | CRM 137   |         |                                      |                     |   |
| ⑩               | 202201875 |         |                                      |                     |   |
| ⑪               | 202201876 |         |                                      |                     | skate/SUS                                 |
| ⑫               | 128       |         |                                      |                     |   |
| ⑬               | CRM 136   |         |                                      |                     |   |
| ⑭               | 202201877 |         |                                      |                     |   |
| ⑮               | 202201875 |         |                                      |                     |   |
| ⑯               | 202201876 |         |                                      |                     |   |
| ⑰               | 128       |         |                                      |                     |   |
| ⑱               | 202201877 |         |                                      |                     |   |
| ⑲               | CRM 137   |         |                                      |                     |   |
| ⑳               | CRM 136   |         |                                      |                     |   |
| ㉑               | 128       |         |                                      |                     |   |

✓ 128, 6 → 1, 6, 8, 12, 17, 21  
 ✓ 137, 3 → 2, 9, 19  
 ✓ 136, 3 → 3, 13, 20  
 ✓ 202201875, 3 → 4, 10, 15  
 ✓ 202201876, 3 → 5, 11, 16  
 ✓ 202201877, 3 → 7, 14, 18

CRM 137A V113 = 3a = 202201877  
 CRM 137A V052 = 2a = 202201876  
 CRM 137A V004 = 1a = 202201875

| Triton Loading Sheet |            |
|----------------------|------------|
| Date:                | 10/25/2022 |
| Turret #:            | 077        |
| Instrument           | 630        |
| Operator:            | Hexel      |

| Turret Position | Sample ID | Element | Filament type (Re,W,Ta) (dbl single) | Loading Volume (uL) | Filament treatment |
|-----------------|-----------|---------|--------------------------------------|---------------------|--------------------|
| 1               | 2M128 PuI | Pu      | Re,dbl                               | 1uL                 | Load @ 1.5A, 5@ 2A |
| 2               | 2C137 PuI | ↓       | ↓                                    | 0.80                | ↓                  |
| 3               | 2C136 PuI | ↓       | ↓                                    | 0.9                 |                    |
| 4               | 202201876 |         |                                      | 0.70uL              |                    |
| 5               | 202201877 |         |                                      | 0.70uL              |                    |
| 6               | 2M128 PuI |         |                                      | 1uL                 |                    |
| 7               | 202201875 |         |                                      | 0.7uL               |                    |
| 8               | 2M128 PuI |         |                                      | 1uL                 |                    |
| 9               | 2C137 PuI |         |                                      | 0.80uL              |                    |
| 10              | 202201876 |         |                                      | 0.7                 |                    |
| 11              | 202201875 |         |                                      | 0.7                 |                    |
| 12              | 2M128 PuI |         |                                      | 1.0                 |                    |
| 13              | 2C136 PuI |         |                                      | 0.9                 |                    |
| 14              | 202201877 |         |                                      | 0.7                 |                    |
| 15              | 202201877 |         |                                      | 0.7                 |                    |
| 16              | 202201875 |         |                                      | 0.7                 |                    |
| 17              | 2M128 PuI |         |                                      | 1.0                 |                    |
| 18              | 2C137 PuI |         |                                      | 0.7                 |                    |
| 19              | 2C137 PuI |         |                                      | 1uL 0.80uL          |                    |
| 20              | 2C136 PuI |         |                                      | 0.9                 |                    |
| 21              | 2M128 PuI |         |                                      | 1.0                 |                    |

| Triton Loading Sheet |   |
|----------------------|---|
| Date:                | 10/27/2022  |
| Turret #:            | 077 <span style="border: 1px solid black; padding: 2px;">Day 3</span> |
| Instrument:          | Hexel 630   |
| Operator:            | Hexel   |

| Turret Position | Sample ID | Element | Filament type (Re, W, Ta) (dbl single) | Loading Volume (uL) | Filament treatment                        |
|-----------------|-----------|---------|--|---------------------|---|
| 1               | 2M128 PuI | Pu      | Re Dbl                                 | 1.0 uL              | Load 0.6 A<br>60 @ 1A, 50 @ 1.5A, 10 @ 2A |
| 2               | 2C137 PuI | ↓       | ↓                                      | 0.6 uL              | ↓   |
| 3               | 2C136 PuI | ↓       | ↓                                      | 0.9 uL              | ↓   |
| 4               | 202201877 | ↓       | ok                                     | 0.7 uL              | x 0.7 uL ↓                                |
| 5               | 202201877 |         |  | 0.7                 |   |
| 6               | 2M128 PuI |         |  | 1.0                 |   |
| 7               | 202201877 |         |  | 0.7                 |   |
| 8               | 2M128 PuI |         |  | 1.0                 |   |
| 9               | 2C137 PuI |         |  | 0.6                 |   |
| 10              | 202201876 |         |  | 0.4                 |   |
| 11              | WRM003    |         |  | 0.8                 |   |
| 12              | 2M128 PuI |         |  | 1.0                 |   |
| 13              | 2C136 PuI |         |  | 0.9                 |   |
| 14              | 202201875 |         |  | 0.6 uL              |   |
| 15              | 2C003 PuI |         |  | 0.8                 |   |
| 16              | 2C002 PuI |         |  | 0.8                 |   |
| 17              | 2M128 PuI |         |  | 1                   |   |
| 18              | 2C003 PuI |         |  | 0.8                 |   |
| 19              | 2C137 PuI |         |  | 0.6                 |   |
| 20              | 2C136 PuI |         |  | 0.9                 |   |
| 21              | 2M128 PuI |         |  | 1.0                 |   |

2M128 PuI (6, 1.0 uL) : 1, 6, 8, 12, 17, 21  
 2C137 PuI (3, 0.6 uL) : 2, 9, 19  
 2C136 PuI (3, 0.9 uL) : 3, 13, 20  
 2C003 PuI (4, 0.8 uL) : 11, 15, 16, 18  
 202201875 (1, 0.6 uL) : 14  
 202201876 (2, 0.4 uL) : 4, 10  
 202201877 (2, 0.7 uL) : 5, 7

| Triton Loading Sheet |          |
|----------------------|----------|
| Date:                | 01/23/20 |
| Turret #:            | Ø77      |
| Instrument           | SN 630   |
| Operator:            | Hexel    |

| Turret Position | Sample ID          | Element | Filament type (Re,W,Ta) (dbl single) | Loading Volume (uL) | Filament treatment                           |
|-----------------|--------------------|---------|--------------------------------------|---------------------|--|
| 1               | 3M128Pt            | Pt      | Re,dbl,Ta                            | 1 uL                | Dry @ 6.5 amp / 1100-600<br>ISA @ 55, 2AG 55 |
| 2               | 3M137Pt            | ↓       | ↓                                    | ↓                   | ↓  |
| 3               | 21875Pt            | ↓       | ↓                                    | ↓                   | ↓  |
| 4               | 21877Pt            | ↓       | ↓                                    | ↓                   | ↓  |
| 5               | 21877Pt            | ↓       | ↓                                    | ↓                   | ↓  |
| 6               | 3M128Pt            |         |                                      |                     |  |
| 7               | <del>3C137Pt</del> | 21877Pt |                                      |                     |  |
| 8               | 3C137Pt            |         |                                      |                     |  |
| 9               | 21875Pt            |         |                                      |                     |  |
| 10              | 21877Pt            |         |                                      |                     |  |
| 11              | 2M128Pt            |         |                                      |                     |  |
| 12              | 21875Pt            |         |                                      |                     |  |
| 13              | 3C137Pt            |         |                                      |                     |  |
| 14              | 21877Pt            |         |                                      |                     |  |
| 15              | 21877Pt            |         |                                      |                     |  |
| 16              | 3M128Pt            |         |                                      |                     |  |
| 17              | 21877Pt            |         |                                      |                     |  |
| 18              | 21875Pt            |         |                                      |                     |  |
| 19              | 21877Pt            |         |                                      |                     |  |
| 20              | 3C137Pt            |         |                                      |                     |  |
| 21              | 3M128Pt            |         |                                      |                     |  |

**APPENDIX B. VIAL 004 GUM WORKBENCH**





## APPENDIX B. VIAL 004 GUM WORKBENCH

### Pu Isotopic for recert 137A

Author: Cole R. Hexel

This Workbench is designed to evaluate the uncertainties in the plutonium isotopic abundance data obtained using the multiple collector mass spectrometer.

#### Model Equation:

*{GUM Uncertainty Calculations for Plutonium Isotopic (PuI) Characterization for a single sample.}*

*{TIMS Data}*

*{Pu 238/239 Ratio Data}*

$$R_{89} = R_{89corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq4};$$

*{Pu 240/239 Ratio Data}*

$$R_{09} = R_{09corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq};$$

*{Pu 241/239 Ratio Data}*

$$R_{19} = R_{19corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq2};$$

*{Pu 242/239 Ratio Data}*

$$R_{29} = R_{29corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq3};$$

*{ICP Data}*

*{Pu 240/239 Ratio Data}*

$$ICPR_{09} = ICPR_{09corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq};$$

*{Pu 241/239 Ratio Data}*

$$ICPR_{19} = ICPR_{19corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq2};$$

*{Pu 242/239 Ratio Data}*

$$ICPR_{29} = ICPR_{29corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq3};$$

**List of Quantities:**

| Quantity                      | Unit | Definition  |
|-------------------------------|------|---|
| $R_{89\text{corr}}$           |      | The corrected $^{238}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{09\text{corr}}$           |      | The corrected $^{240}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{19\text{corr}}$           |      | The corrected $^{241}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{29\text{corr}}$           |      | The corrected $^{242}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $\delta_{\text{Cert}}$        |      | Relative uncertainty associated with the decay-corrected certified $^{242}\text{Pu}/^{239}\text{Pu}$ ratio on the mass bias standard certificate. |
| $\delta_{\text{CFVar}}$       |      | Relative standard error associated with the mass bias measurements before and after the sample for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio    |
| $\delta_{\text{seq}}$         |      | Daily variability of each sequence run for the $^{240}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $\delta_{\text{seq}2}$        |      | Daily variability of each sequence run for the $^{241}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $\delta_{\text{seq}3}$        |      | Daily variability of each sequence run for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $\delta_{\text{seq}4}$        |      | Daily variability of each sequence run for the $^{238}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $R_{09}$                      |      | The final $^{240}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{19}$                      |      | The final $^{241}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{29}$                      |      | The final $^{242}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{89}$                      |      | The final $^{238}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $\text{ICPR}_{09\text{corr}}$ |      | The corrected $^{240}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\text{ICPR}_{19\text{corr}}$ |      | The corrected $^{241}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\text{ICPR}_{29\text{corr}}$ |      | The corrected $^{242}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\delta_{\text{ICPseq}}$      |      | Daily variability of each sequence run for the $^{240}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPseq}2}$     |      | Daily variability of each sequence run for the $^{241}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPseq}3}$     |      | Daily variability of each sequence run for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPCFVar}}$    |      | Relative standard error associated with the mass bias measurements before and after the sample for the $^{242}\text{Pu}/^{239}\text{Pu}$ Ratio    |
| $\text{ICPR}_{09}$            |      | The final $^{240}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |
| $\text{ICPR}_{19}$            |      | The final $^{241}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |
| $\text{ICPR}_{29}$            |      | The final $^{242}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |

**Input Correlation**

|                     |                     |                     |                     |                     |
|---------------------|---------------------|---------------------|---------------------|---------------------|
|                     | $R_{89\text{corr}}$ | $R_{09\text{corr}}$ | $R_{19\text{corr}}$ | $R_{29\text{corr}}$ |
| $R_{89\text{corr}}$ | 1                   | -0.4174             | 0.7846              | -0.0471             |
| $R_{09\text{corr}}$ | -0.4174             | 1                   | -0.5457             | 0.8651              |
| $R_{19\text{corr}}$ | 0.7846              | -0.5457             | 1                   | -0.4151             |
| $R_{29\text{corr}}$ | -0.0471             | 0.8651              | -0.4151             | 1                   |

|                        |                        |                        |                        |
|------------------------|------------------------|------------------------|------------------------|
|                        | ICPR <sub>09corr</sub> | ICPR <sub>19corr</sub> | ICPR <sub>29corr</sub> |
| ICPR <sub>09corr</sub> | 1                      | -0.0809                | -0.2334                |
| ICPR <sub>19corr</sub> | -0.0809                | 1                      | -0.4418                |
| ICPR <sub>29corr</sub> | -0.2334                | -0.4418                | 1                      |

### Uncertainty Budgets:

#### R<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>09corr</sub>     | 0.24062618 | $7.54 \times 10^{-6}$ | normal       | 1.0                     | $7.5 \times 10^{-6}$     | 3.9%  |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 66.4% |
| $\delta_{\text{CFVar}}$ | 1.0000000  | $76.4 \times 10^{-6}$ | normal       | 0.24                    | $18 \times 10^{-6}$      | 22.9% |
| $\delta_{\text{seq}}$   | 0.0        | $10.0 \times 10^{-6}$ | normal       | 1.0                     | $10 \times 10^{-6}$      | 6.8%  |
| R <sub>09</sub>         | 0.2406262  | $38.4 \times 10^{-6}$ |              |                         |                          |       |

#### R<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value                   | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|-------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>19corr</sub>     | $5.0994 \times 10^{-3}$ | $15.8 \times 10^{-6}$ | normal       | 1.0                     | $16 \times 10^{-6}$      | 84.2% |
| $\delta_{\text{Cert}}$  | 1.000000                | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $660 \times 10^{-9}$     | 0.1%  |
| $\delta_{\text{CFVar}}$ | 1.0000000               | $76.4 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $390 \times 10^{-9}$     | 0.0%  |
| $\delta_{\text{seq2}}$  | 0.0                     | $6.80 \times 10^{-6}$ | normal       | 1.0                     | $6.8 \times 10^{-6}$     | 15.6% |
| R <sub>19</sub>         | $5.0994 \times 10^{-3}$ | $17.2 \times 10^{-6}$ |              |                         |                          |       |

#### R<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>29corr</sub>     | 0.01557764 | $1.76 \times 10^{-6}$ | normal       | 1.0                     | $1.8 \times 10^{-6}$     | 27.8% |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 36.6% |
| $\delta_{\text{CFVar}}$ | 1.0000000  | $76.4 \times 10^{-6}$ | normal       | 0.016                   | $1.2 \times 10^{-6}$     | 12.7% |
| $\delta_{\text{seq3}}$  | 0.0        | $1.60 \times 10^{-6}$ | normal       | 1.0                     | $1.6 \times 10^{-6}$     | 22.9% |
| R <sub>29</sub>         | 0.01557764 | $3.35 \times 10^{-6}$ |              |                         |                          |       |

**R<sub>89</sub>: The final <sup>238</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>89corr</sub>     | $2.63702 \times 10^{-3}$ | $1.67 \times 10^{-6}$ | normal       | 1.0                     | $1.7 \times 10^{-6}$     | 40.3% |
| $\delta_{\text{Cert}}$  | 1.000000                 | $130 \times 10^{-6}$  | normal       | $2.6 \times 10^{-3}$    | $340 \times 10^{-9}$     | 1.7%  |
| $\delta_{\text{CFVar}}$ | 1.0000000                | $76.4 \times 10^{-6}$ | normal       | $2.6 \times 10^{-3}$    | $200 \times 10^{-9}$     | 0.6%  |
| $\delta_{\text{seq4}}$  | 0.0                      | $2.00 \times 10^{-6}$ | normal       | 1.0                     | $2.0 \times 10^{-6}$     | 57.4% |
| R <sub>89</sub>         | $2.63702 \times 10^{-3}$ | $2.64 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 76.3% |
| ICPR <sub>09corr</sub>     | 0.24063095 | $5.05 \times 10^{-6}$ | normal       | 1.0                     | $5.0 \times 10^{-6}$     | 2.0%  |
| $\delta_{\text{ICPseq}}$   | 0.0        | $12.4 \times 10^{-6}$ | normal       | 1.0                     | $12 \times 10^{-6}$      | 12.0% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000  | $46.3 \times 10^{-6}$ | normal       | 0.24                    | $11 \times 10^{-6}$      | 9.7%  |
| ICPR <sub>09</sub>         | 0.2406309  | $35.8 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000                 | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $660 \times 10^{-9}$     | 0.1%  |
| ICPR <sub>19corr</sub>     | $5.10479 \times 10^{-3}$ | $6.60 \times 10^{-6}$ | normal       | 1.0                     | $6.6 \times 10^{-6}$     | 12.4% |
| $\delta_{\text{ICPseq2}}$  | 0.0                      | $17.5 \times 10^{-6}$ | normal       | 1.0                     | $18 \times 10^{-6}$      | 87.4% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000                | $46.3 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $240 \times 10^{-9}$     | 0.0%  |
| ICPR <sub>19</sub>         | $5.1048 \times 10^{-3}$  | $18.7 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 0.9%  |
| ICPR <sub>29corr</sub>     | 0.01557253 | $5.59 \times 10^{-6}$ | normal       | 1.0                     | $5.6 \times 10^{-6}$     | 7.2%  |
| $\delta_{\text{ICPseq3}}$  | 0.0        | $19.9 \times 10^{-6}$ | normal       | 1.0                     | $20 \times 10^{-6}$      | 91.7% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000  | $46.3 \times 10^{-6}$ | normal       | 0.016                   | $720 \times 10^{-9}$     | 0.1%  |
| ICPR <sub>29</sub>         | 0.0155725  | $20.8 \times 10^{-6}$ |              |                         |                          |       |

**Results:**

| Quantity           | Value                   | Expanded uncertainty | Coverage factor | Coverage     |
|--------------------|-------------------------|----------------------|-----------------|--------------|
| R <sub>09</sub>    | 0.240626                | $77 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>19</sub>    | $5.099 \times 10^{-3}$  | $34 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>29</sub>    | 0.0155776               | $6.7 \times 10^{-6}$ | 2.00            | 95% (normal) |
| R <sub>89</sub>    | $2.6370 \times 10^{-3}$ | $5.3 \times 10^{-6}$ | 2.00            | 95% (normal) |
| ICPR <sub>09</sub> | 0.240631                | $72 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>19</sub> | $5.105 \times 10^{-3}$  | $37 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>29</sub> | 0.015573                | $42 \times 10^{-6}$  | 2.00            | 95% (normal) |

**Result Correlation:**

|                    | R <sub>09</sub> | R <sub>19</sub>      | R <sub>29</sub> | R <sub>89</sub>      | ICPR <sub>09</sub> | ICPR <sub>19</sub>   | ICPR <sub>29</sub>   |
|--------------------|-----------------|----------------------|-----------------|----------------------|--------------------|----------------------|----------------------|
| R <sub>09</sub>    | 1               | -0.0561              | 0.7533          | 0.0904               | 0.7120             | 0.0289               | 0.0794               |
| R <sub>19</sub>    | -0.0561         | 1                    | -0.1695         | 0.4636               | 0.0337             | $1.4 \times 10^{-3}$ | $3.8 \times 10^{-3}$ |
| R <sub>29</sub>    | 0.7533          | -0.1695              | 1               | 0.0900               | 0.5289             | 0.0215               | 0.0590               |
| R <sub>89</sub>    | 0.0904          | 0.4636               | 0.0900          | 1                    | 0.1135             | $4.6 \times 10^{-3}$ | 0.0127               |
| ICPR <sub>09</sub> | 0.7120          | 0.0337               | 0.5289          | 0.1135               | 1                  | 0.0309               | 0.0871               |
| ICPR <sub>19</sub> | 0.0289          | $1.4 \times 10^{-3}$ | 0.0215          | $4.6 \times 10^{-3}$ | 0.0309             | 1                    | -0.0380              |
| ICPR <sub>29</sub> | 0.0794          | $3.8 \times 10^{-3}$ | 0.0590          | 0.0127               | 0.0871             | -0.0380              | 1                    |



**APPENDIX C. VIAL 052 GUM WORKBENCH**





## APPENDIX C. VIAL 052 GUM WORKBENCH

### Pu Isotopic for recert 137A

Author: Cole R. Hexel

This Workbench is designed to evaluate the uncertainties in the plutonium isotopic abundance data obtained using the multiple collector mass spectrometer.

#### Model Equation:

*{GUM Uncertainty Calculations for Plutonium Isotopic (PuI) Characterization for a single sample.}*

*{TIMS Data}*

*{Pu 238/239 Ratio Data}*

$$R_{89} = R_{89corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq4};$$

*{Pu 240/239 Ratio Data}*

$$R_{09} = R_{09corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq};$$

*{Pu 241/239 Ratio Data}*

$$R_{19} = R_{19corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq2};$$

*{Pu 242/239 Ratio Data}*

$$R_{29} = R_{29corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq3};$$

*{ICP Data}*

*{Pu 240/239 Ratio Data}*

$$ICPR_{09} = ICPR_{09corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq};$$

*{Pu 241/239 Ratio Data}*

$$ICPR_{19} = ICPR_{19corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq2};$$

*{Pu 242/239 Ratio Data}*

$$ICPR_{29} = ICPR_{29corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq3};$$

**List of Quantities:**

| Quantity                      | Unit | Definition  |
|-------------------------------|------|---|
| $R_{89\text{corr}}$           |      | The corrected $^{238}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{09\text{corr}}$           |      | The corrected $^{240}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{19\text{corr}}$           |      | The corrected $^{241}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{29\text{corr}}$           |      | The corrected $^{242}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $\delta_{\text{Cert}}$        |      | Relative uncertainty associated with the decay-corrected certified $^{242}\text{Pu}/^{239}\text{Pu}$ ratio on the mass bias standard certificate. |
| $\delta_{\text{CFVar}}$       |      | Relative standard error associated with the mass bias measurements before and after the sample for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio    |
| $\delta_{\text{seq}}$         |      | day to day variability of each sequence run for the $^{240}\text{Pu}/^{239}\text{Pu}$ ratio   |
| $\delta_{\text{seq}2}$        |      | day to day variability of each sequence run for the $^{241}\text{Pu}/^{239}\text{Pu}$ ratio   |
| $\delta_{\text{seq}3}$        |      | day to day variability of each sequence run for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio   |
| $\delta_{\text{seq}4}$        |      | day to day variability of each sequence run for the $^{238}\text{Pu}/^{239}\text{Pu}$ ratio   |
| $R_{09}$                      |      | The final $^{240}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{19}$                      |      | The final $^{241}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{29}$                      |      | The final $^{242}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{89}$                      |      | The final $^{238}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $\text{ICPR}_{09\text{corr}}$ |      | The corrected $^{240}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\text{ICPR}_{19\text{corr}}$ |      | The corrected $^{241}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\text{ICPR}_{29\text{corr}}$ |      | The corrected $^{242}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\delta_{\text{ICPseq}}$      |      | Daily variability of each sequence run for the $^{240}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPseq}2}$     |      | Daily variability of each sequence run for the $^{241}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPseq}3}$     |      | Daily variability of each sequence run for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPCFVar}}$    |      | Relative standard error associated with the mass bias measurements before and after the sample for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio    |
| $\text{ICPR}_{09}$            |      | The final $^{240}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |
| $\text{ICPR}_{19}$            |      | The final $^{241}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |
| $\text{ICPR}_{29}$            |      | The final $^{242}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |

**Input Correlation**

|                     |                     |                     |                     |                     |
|---------------------|---------------------|---------------------|---------------------|---------------------|
|                     | $R_{89\text{corr}}$ | $R_{09\text{corr}}$ | $R_{19\text{corr}}$ | $R_{29\text{corr}}$ |
| $R_{89\text{corr}}$ | 1                   | -0.4174             | 0.7846              | -0.0471             |
| $R_{09\text{corr}}$ | -0.4174             | 1                   | -0.5457             | 0.8651              |
| $R_{19\text{corr}}$ | 0.7846              | -0.5457             | 1                   | -0.4151             |
| $R_{29\text{corr}}$ | -0.0471             | 0.8651              | -0.4151             | 1                   |

|                        |                        |                        |                        |
|------------------------|------------------------|------------------------|------------------------|
|                        | ICPR <sub>09corr</sub> | ICPR <sub>19corr</sub> | ICPR <sub>29corr</sub> |
| ICPR <sub>09corr</sub> | 1                      | -0.0809                | -0.2334                |
| ICPR <sub>19corr</sub> | -0.0809                | 1                      | -0.4418                |
| ICPR <sub>29corr</sub> | -0.2334                | -0.4418                | 1                      |

### Uncertainty Budgets:

#### R<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>09corr</sub>     | 0.24062720 | $9.51 \times 10^{-6}$ | normal       | 1.0                     | $9.5 \times 10^{-6}$     | 6.0%  |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 64.9% |
| $\delta_{\text{CFVar}}$ | 1.0000000  | $76.4 \times 10^{-6}$ | normal       | 0.24                    | $18 \times 10^{-6}$      | 22.4% |
| $\delta_{\text{seq}}$   | 0.0        | $10.0 \times 10^{-6}$ | normal       | 1.0                     | $10 \times 10^{-6}$      | 6.6%  |
| R <sub>09</sub>         | 0.2406272  | $38.8 \times 10^{-6}$ |              |                         |                          |       |

#### R<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value                     | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|---------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>19corr</sub>     | $5.110839 \times 10^{-3}$ | $874 \times 10^{-9}$  | normal       | 1.0                     | $870 \times 10^{-9}$     | 1.6%  |
| $\delta_{\text{Cert}}$  | 1.000000                  | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $660 \times 10^{-9}$     | 0.9%  |
| $\delta_{\text{CFVar}}$ | 1.0000000                 | $76.4 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $390 \times 10^{-9}$     | 0.3%  |
| $\delta_{\text{seq2}}$  | 0.0                       | $6.80 \times 10^{-6}$ | normal       | 1.0                     | $6.8 \times 10^{-6}$     | 97.1% |
| R <sub>19</sub>         | $5.11084 \times 10^{-3}$  | $6.90 \times 10^{-6}$ |              |                         |                          |       |

#### R<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>29corr</sub>     | 0.01557713 | $1.88 \times 10^{-6}$ | normal       | 1.0                     | $1.9 \times 10^{-6}$     | 30.4% |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 35.3% |
| $\delta_{\text{CFVar}}$ | 1.0000000  | $76.4 \times 10^{-6}$ | normal       | 0.016                   | $1.2 \times 10^{-6}$     | 12.2% |
| $\delta_{\text{seq3}}$  | 0.0        | $1.60 \times 10^{-6}$ | normal       | 1.0                     | $1.6 \times 10^{-6}$     | 22.1% |
| R <sub>29</sub>         | 0.01557713 | $3.41 \times 10^{-6}$ |              |                         |                          |       |

**R<sub>89</sub>: The final <sup>238</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>89corr</sub>     | $2.64401 \times 10^{-3}$ | $4.27 \times 10^{-6}$ | normal       | 1.0                     | $4.3 \times 10^{-6}$     | 81.4% |
| $\delta_{\text{Cert}}$  | 1.000000                 | $130 \times 10^{-6}$  | normal       | $2.6 \times 10^{-3}$    | $340 \times 10^{-9}$     | 0.5%  |
| $\delta_{\text{CFVar}}$ | 1.0000000                | $76.4 \times 10^{-6}$ | normal       | $2.6 \times 10^{-3}$    | $200 \times 10^{-9}$     | 0.2%  |
| $\delta_{\text{seq4}}$  | 0.0                      | $2.00 \times 10^{-6}$ | normal       | 1.0                     | $2.0 \times 10^{-6}$     | 17.8% |
| R <sub>89</sub>         | $2.64401 \times 10^{-3}$ | $4.73 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 75.6% |
| ICPR <sub>09corr</sub>     | 0.24062296 | $6.13 \times 10^{-6}$ | normal       | 1.0                     | $6.1 \times 10^{-6}$     | 2.9%  |
| $\delta_{\text{ICPseq}}$   | 0.0        | $12.4 \times 10^{-6}$ | normal       | 1.0                     | $12 \times 10^{-6}$      | 11.9% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000  | $46.3 \times 10^{-6}$ | normal       | 0.24                    | $11 \times 10^{-6}$      | 9.6%  |
| ICPR <sub>09</sub>         | 0.2406230  | $36.0 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000                 | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $660 \times 10^{-9}$     | 0.1%  |
| ICPR <sub>19corr</sub>     | $5.10539 \times 10^{-3}$ | $4.58 \times 10^{-6}$ | normal       | 1.0                     | $4.6 \times 10^{-6}$     | 6.4%  |
| $\delta_{\text{ICPseq2}}$  | 0.0                      | $17.5 \times 10^{-6}$ | normal       | 1.0                     | $18 \times 10^{-6}$      | 93.4% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000                | $46.3 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $240 \times 10^{-9}$     | 0.0%  |
| ICPR <sub>19</sub>         | $5.1054 \times 10^{-3}$  | $18.1 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 0.9%  |
| ICPR <sub>29corr</sub>     | 0.01557139 | $7.17 \times 10^{-6}$ | normal       | 1.0                     | $7.2 \times 10^{-6}$     | 11.4% |
| $\delta_{\text{ICPseq3}}$  | 0.0        | $19.9 \times 10^{-6}$ | normal       | 1.0                     | $20 \times 10^{-6}$      | 87.6% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000  | $46.3 \times 10^{-6}$ | normal       | 0.016                   | $720 \times 10^{-9}$     | 0.1%  |
| ICPR <sub>29</sub>         | 0.0155714  | $21.3 \times 10^{-6}$ |              |                         |                          |       |

**Results:**

| Quantity           | Value                   | Expanded uncertainty | Coverage factor | Coverage     |
|--------------------|-------------------------|----------------------|-----------------|--------------|
| R <sub>09</sub>    | 0.240627                | $78 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>19</sub>    | $5.111 \times 10^{-3}$  | $14 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>29</sub>    | 0.0155771               | $6.8 \times 10^{-6}$ | 2.00            | 95% (normal) |
| R <sub>89</sub>    | $2.6440 \times 10^{-3}$ | $9.5 \times 10^{-6}$ | 2.00            | 95% (normal) |
| ICPR <sub>09</sub> | 0.240623                | $72 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>19</sub> | $5.105 \times 10^{-3}$  | $36 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>29</sub> | 0.015571                | $43 \times 10^{-6}$  | 2.00            | 95% (normal) |

**Result Correlation:**

|                    | R <sub>09</sub> | R <sub>19</sub>      | R <sub>29</sub> | R <sub>89</sub>      | ICPR <sub>09</sub> | ICPR <sub>19</sub>   | ICPR <sub>29</sub>   |
|--------------------|-----------------|----------------------|-----------------|----------------------|--------------------|----------------------|----------------------|
| R <sub>09</sub>    | 1               | 0.0875               | 0.7614          | -0.0136              | 0.7007             | 0.0295               | 0.0767               |
| R <sub>19</sub>    | 0.0875          | 1                    | 0.0480          | 0.0991               | 0.0837             | $3.5 \times 10^{-3}$ | $9.2 \times 10^{-3}$ |
| R <sub>29</sub>    | 0.7614          | 0.0480               | 1               | 0.0346               | 0.5170             | 0.0218               | 0.0566               |
| R <sub>89</sub>    | -0.0136         | 0.0991               | 0.0346          | 1                    | 0.0631             | $2.7 \times 10^{-3}$ | $6.9 \times 10^{-3}$ |
| ICPR <sub>09</sub> | 0.7007          | 0.0837               | 0.5170          | 0.0631               | 1                  | 0.0324               | 0.0799               |
| ICPR <sub>19</sub> | 0.0295          | $3.5 \times 10^{-3}$ | 0.0218          | $2.7 \times 10^{-3}$ | 0.0324             | 1                    | -0.0338              |
| ICPR <sub>29</sub> | 0.0767          | $9.2 \times 10^{-3}$ | 0.0566          | $6.9 \times 10^{-3}$ | 0.0799             | -0.0338              | 1                    |



**APPENDIX D. VIAL 113 GUM WORKBENCH**





## APPENDIX D. VIAL 113 GUM WORKBENCH

### Pu Isotopic for recert 137A

Author: Cole R. Hexel

This Workbench is designed to evaluate the uncertainties in the plutonium isotopic abundance data obtained using the multiple collector mass spectrometer.

#### Model Equation:

*{GUM Uncertainty Calculations for Plutonium Isotopic (PuI) Characterization for a single sample.}*

*{TIMS Data}*

*{Pu 238/239 Ratio Data}*

$$R_{89} = R_{89corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq4};$$

*{Pu 240/239 Ratio Data}*

$$R_{09} = R_{09corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq};$$

*{Pu 241/239 Ratio Data}*

$$R_{19} = R_{19corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq2};$$

*{Pu 242/239 Ratio Data}*

$$R_{29} = R_{29corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq3};$$

*{ICP Data}*

*{Pu 240/239 Ratio Data}*

$$ICPR_{09} = ICPR_{09corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq};$$

*{Pu 241/239 Ratio Data}*

$$ICPR_{19} = ICPR_{19corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq2};$$

*{Pu 242/239 Ratio Data}*

$$ICPR_{29} = ICPR_{29corr} * \delta_{Cert} * \delta_{ICPCFVar} + \delta_{ICPseq3};$$

**List of Quantities:**

| Quantity                      | Unit | Definition  |
|-------------------------------|------|---|
| $R_{89\text{corr}}$           |      | The corrected $^{238}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{09\text{corr}}$           |      | The corrected $^{240}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{19\text{corr}}$           |      | The corrected $^{241}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $R_{29\text{corr}}$           |      | The corrected $^{242}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs.   |
| $\delta_{\text{Cert}}$        |      | Relative uncertainty associated with the decay-corrected certified $^{242}\text{Pu}/^{239}\text{Pu}$ ratio on the mass bias standard certificate. |
| $\delta_{\text{CFVar}}$       |      | Relative standard error associated with the mass bias measurements before and after the sample for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio    |
| $\delta_{\text{seq}}$         |      | Daily variability of each sequence run for the $^{240}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $\delta_{\text{seq}2}$        |      | Daily variability of each sequence run for the $^{241}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $\delta_{\text{seq}3}$        |      | Daily variability of each sequence run for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $\delta_{\text{seq}4}$        |      | Daily variability of each sequence run for the $^{238}\text{Pu}/^{239}\text{Pu}$ ratio  |
| $R_{09}$                      |      | The final $^{240}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{19}$                      |      | The final $^{241}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{29}$                      |      | The final $^{242}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $R_{89}$                      |      | The final $^{238}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty   |
| $\text{ICPR}_{09\text{corr}}$ |      | The corrected $^{240}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\text{ICPR}_{19\text{corr}}$ |      | The corrected $^{241}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\text{ICPR}_{29\text{corr}}$ |      | The corrected $^{242}\text{Pu}/^{239}\text{Pu}$ ratio data from OakLimbs MC-ICP-MS  |
| $\delta_{\text{ICPseq}}$      |      | Daily variability of each sequence run for the $^{240}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPseq}2}$     |      | Daily variability of each sequence run for the $^{241}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPseq}3}$     |      | Daily variability of each sequence run for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio on ICP   |
| $\delta_{\text{ICPCFVar}}$    |      | Relative standard error associated with the mass bias measurements before and after the sample for the $^{242}\text{Pu}/^{239}\text{Pu}$ ratio    |
| $\text{ICPR}_{09}$            |      | The final $^{240}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |
| $\text{ICPR}_{19}$            |      | The final $^{241}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |
| $\text{ICPR}_{29}$            |      | The final $^{242}\text{Pu}/^{239}\text{Pu}$ ratio and uncertainty from ICP  |

**Input Correlation**

|                     |                     |                     |                     |                     |
|---------------------|---------------------|---------------------|---------------------|---------------------|
|                     | $R_{89\text{corr}}$ | $R_{09\text{corr}}$ | $R_{19\text{corr}}$ | $R_{29\text{corr}}$ |
| $R_{89\text{corr}}$ | 1                   | -0.4174             | 0.7846              | -0.0471             |
| $R_{09\text{corr}}$ | -0.4174             | 1                   | -0.5457             | 0.8651              |
| $R_{19\text{corr}}$ | 0.7846              | -0.5457             | 1                   | -0.4151             |
| $R_{29\text{corr}}$ | -0.0471             | 0.8651              | -0.4151             | 1                   |

|                        |                        |                        |                        |
|------------------------|------------------------|------------------------|------------------------|
|                        | ICPR <sub>09corr</sub> | ICPR <sub>19corr</sub> | ICPR <sub>29corr</sub> |
| ICPR <sub>09corr</sub> | 1                      | -0.0809                | -0.2334                |
| ICPR <sub>19corr</sub> | -0.0809                | 1                      | -0.4418                |
| ICPR <sub>29corr</sub> | -0.2334                | -0.4418                | 1                      |

### Uncertainty Budgets:

#### R<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>09corr</sub>     | 0.24062551 | $4.53 \times 10^{-6}$ | normal       | 1.0                     | $4.5 \times 10^{-6}$     | 1.4%  |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 68.1% |
| $\delta_{\text{CFVar}}$ | 1.0000000  | $76.4 \times 10^{-6}$ | normal       | 0.24                    | $18 \times 10^{-6}$      | 23.5% |
| $\delta_{\text{seq}}$   | 0.0        | $10.0 \times 10^{-6}$ | normal       | 1.0                     | $10 \times 10^{-6}$      | 7.0%  |
| R <sub>09</sub>         | 0.2406255  | $37.9 \times 10^{-6}$ |              |                         |                          |       |

#### R<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value                   | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|-------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>19corr</sub>     | $5.1214 \times 10^{-3}$ | $13.9 \times 10^{-6}$ | normal       | 1.0                     | $14 \times 10^{-6}$      | 80.4% |
| $\delta_{\text{Cert}}$  | 1.000000                | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $670 \times 10^{-9}$     | 0.2%  |
| $\delta_{\text{CFVar}}$ | 1.0000000               | $76.4 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $390 \times 10^{-9}$     | 0.0%  |
| $\delta_{\text{seq2}}$  | 0.0                     | $6.80 \times 10^{-6}$ | normal       | 1.0                     | $6.8 \times 10^{-6}$     | 19.3% |
| R <sub>19</sub>         | $5.1214 \times 10^{-3}$ | $15.5 \times 10^{-6}$ |              |                         |                          |       |

#### R<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>29corr</sub>     | 0.01557766 | $1.75 \times 10^{-6}$ | normal       | 1.0                     | $1.8 \times 10^{-6}$     | 27.5% |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 36.8% |
| $\delta_{\text{CFVar}}$ | 1.0000000  | $76.4 \times 10^{-6}$ | normal       | 0.016                   | $1.2 \times 10^{-6}$     | 12.7% |
| $\delta_{\text{seq3}}$  | 0.0        | $1.60 \times 10^{-6}$ | normal       | 1.0                     | $1.6 \times 10^{-6}$     | 23.0% |
| R <sub>29</sub>         | 0.01557766 | $3.34 \times 10^{-6}$ |              |                         |                          |       |

**R<sub>89</sub>: The final <sup>238</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>89corr</sub>     | $2.64820 \times 10^{-3}$ | $9.37 \times 10^{-6}$ | normal       | 1.0                     | $9.4 \times 10^{-6}$     | 95.5% |
| $\delta_{\text{Cert}}$  | 1.000000                 | $130 \times 10^{-6}$  | normal       | $2.6 \times 10^{-3}$    | $340 \times 10^{-9}$     | 0.1%  |
| $\delta_{\text{CFVar}}$ | 1.0000000                | $76.4 \times 10^{-6}$ | normal       | $2.6 \times 10^{-3}$    | $200 \times 10^{-9}$     | 0.0%  |
| $\delta_{\text{seq4}}$  | 0.0                      | $2.00 \times 10^{-6}$ | normal       | 1.0                     | $2.0 \times 10^{-6}$     | 4.3%  |
| R <sub>89</sub>         | $2.64820 \times 10^{-3}$ | $9.59 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 75.7% |
| ICPR <sub>09corr</sub>     | 0.24063514 | $5.95 \times 10^{-6}$ | normal       | 1.0                     | $6.0 \times 10^{-6}$     | 2.7%  |
| $\delta_{\text{ICPseq}}$   | 0.0        | $12.4 \times 10^{-6}$ | normal       | 1.0                     | $12 \times 10^{-6}$      | 11.9% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000  | $46.3 \times 10^{-6}$ | normal       | 0.24                    | $11 \times 10^{-6}$      | 9.6%  |
| ICPR <sub>09</sub>         | 0.2406351  | $35.9 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000                 | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $660 \times 10^{-9}$     | 0.1%  |
| ICPR <sub>19corr</sub>     | $5.08573 \times 10^{-3}$ | $9.64 \times 10^{-6}$ | normal       | 1.0                     | $9.6 \times 10^{-6}$     | 23.2% |
| $\delta_{\text{ICPseq2}}$  | 0.0                      | $17.5 \times 10^{-6}$ | normal       | 1.0                     | $18 \times 10^{-6}$      | 76.6% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000                | $46.3 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $240 \times 10^{-9}$     | 0.0%  |
| ICPR <sub>19</sub>         | $5.0857 \times 10^{-3}$  | $20.0 \times 10^{-6}$ |              |                         |                          |       |

**ICPR<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty from ICP**

| Quantity                   | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|----------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| $\delta_{\text{Cert}}$     | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 0.8%  |
| ICPR <sub>29corr</sub>     | 0.01558524 | $9.59 \times 10^{-6}$ | normal       | 1.0                     | $9.6 \times 10^{-6}$     | 18.7% |
| $\delta_{\text{ICPseq3}}$  | 0.0        | $19.9 \times 10^{-6}$ | normal       | 1.0                     | $20 \times 10^{-6}$      | 80.4% |
| $\delta_{\text{ICPCFVar}}$ | 1.0000000  | $46.3 \times 10^{-6}$ | normal       | 0.016                   | $720 \times 10^{-9}$     | 0.1%  |
| ICPR <sub>29</sub>         | 0.0155852  | $22.2 \times 10^{-6}$ |              |                         |                          |       |

**Results:**

| Quantity           | Value                  | Expanded uncertainty | Coverage factor | Coverage     |
|--------------------|------------------------|----------------------|-----------------|--------------|
| R <sub>09</sub>    | 0.240626               | $76 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>19</sub>    | $5.121 \times 10^{-3}$ | $31 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>29</sub>    | 0.0155777              | $6.7 \times 10^{-6}$ | 2.00            | 95% (normal) |
| R <sub>89</sub>    | $2.648 \times 10^{-3}$ | $19 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>09</sub> | 0.240635               | $72 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>19</sub> | $5.086 \times 10^{-3}$ | $40 \times 10^{-6}$  | 2.00            | 95% (normal) |
| ICPR <sub>29</sub> | 0.015585               | $44 \times 10^{-6}$  | 2.00            | 95% (normal) |

**Result Correlation:**

|                    | R <sub>09</sub>       | R <sub>19</sub>      | R <sub>29</sub>      | R <sub>89</sub>       | ICPR <sub>09</sub> | ICPR <sub>19</sub>   | ICPR <sub>29</sub>   |
|--------------------|-----------------------|----------------------|----------------------|-----------------------|--------------------|----------------------|----------------------|
| R <sub>09</sub>    | 1                     | -0.0107              | 0.7278               | $-8.9 \times 10^{-3}$ | 0.7182             | 0.0273               | 0.0753               |
| R <sub>19</sub>    | -0.0107               | 1                    | -0.1601              | 0.6897                | 0.0375             | $1.4 \times 10^{-3}$ | $3.9 \times 10^{-3}$ |
| R <sub>29</sub>    | 0.7278                | -0.1601              | 1                    | $5.2 \times 10^{-3}$  | 0.5280             | 0.0201               | 0.0554               |
| R <sub>89</sub>    | $-8.9 \times 10^{-3}$ | 0.6897               | $5.2 \times 10^{-3}$ | 1                     | 0.0312             | $1.2 \times 10^{-3}$ | $3.3 \times 10^{-3}$ |
| ICPR <sub>09</sub> | 0.7182                | 0.0375               | 0.5280               | 0.0312                | 1                  | 0.0260               | 0.0728               |
| ICPR <sub>19</sub> | 0.0273                | $1.4 \times 10^{-3}$ | 0.0201               | $1.2 \times 10^{-3}$  | 0.0260             | 1                    | -0.0886              |
| ICPR <sub>29</sub> | 0.0753                | $3.9 \times 10^{-3}$ | 0.0554               | $3.3 \times 10^{-3}$  | 0.0728             | -0.0886              | 1                    |



**APPENDIX E. VIAL 4, 52, 113 COMBINED GUM WORKBENCH**





## APPENDIX E. VIAL 004, 052, 113 COMBINED GUM WORKBENCH

### Pu Isotopic for recert 137A

Author: Cole R. Hexel

This Workbench is designed to evaluate the uncertainties in the plutonium isotopic abundance data obtained using the multicollector inductively coupled plasma–mass spectrometer.

#### Model Equation:

*{GUM Uncertainty Calculations for Plutonium Isotopic (PuI) Characterization for a single sample.}*

*{Pu 238/239 Ratio Data}*

$$R_{89} = R_{89corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq4};$$

*{Pu 240/239 Ratio Data}*

$$R_{09} = R_{09corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq2};$$

*{Pu 241/239 Ratio Data}*

$$R_{19} = R_{19corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq2};$$

*{Pu 242/239 Ratio Data}*

$$R_{29} = R_{29corr} * \delta_{Cert} * \delta_{CFVar} + \delta_{seq3};$$

#### List of Quantities:

| Quantity            | Unit | Definition   |
|---------------------|------|--|
| R <sub>89corr</sub> |      | The corrected <sup>238</sup> Pu/ <sup>239</sup> Pu ratio data from OakLimbs.   |
| R <sub>09corr</sub> |      | The corrected <sup>240</sup> Pu/ <sup>239</sup> Pu ratio data from OakLimbs.   |
| R <sub>19corr</sub> |      | The corrected <sup>241</sup> Pu/ <sup>239</sup> Pu ratio data from OakLimbs.   |
| R <sub>29corr</sub> |      | The corrected <sup>242</sup> Pu/ <sup>239</sup> Pu ratio data from OakLimbs.   |
| δ <sub>Cert</sub>   |      | Relative uncertainty associated with the decay-corrected certified <sup>242</sup> Pu/ <sup>239</sup> Pu ratio on the mass bias standard certificate. |
| δ <sub>CFVar</sub>  |      | Relative standard error associated with the mass bias measurements before and after the sample for the <sup>242</sup> Pu/ <sup>239</sup> Pu ratio    |
| δ <sub>seq</sub>    |      | Daily variability of each sequence run for the <sup>240</sup> Pu/ <sup>239</sup> Pu ratio  |
| δ <sub>seq2</sub>   |      | Daily variability of each sequence run for the <sup>241</sup> Pu/ <sup>239</sup> Pu ratio  |
| δ <sub>seq3</sub>   |      | Daily variability of each sequence run for the <sup>242</sup> Pu/ <sup>239</sup> Pu ratio  |
| δ <sub>seq4</sub>   |      | Daily variability of each sequence run for the <sup>238</sup> Pu/ <sup>239</sup> Pu ratio  |
| R <sub>09</sub>     |      | The final <sup>240</sup> Pu/ <sup>239</sup> Pu ratio and uncertainty   |
| R <sub>19</sub>     |      | The final <sup>241</sup> Pu/ <sup>239</sup> Pu ratio and uncertainty   |
| R <sub>29</sub>     |      | The final <sup>242</sup> Pu/ <sup>239</sup> Pu ratio and uncertainty   |
| R <sub>89</sub>     |      | The final <sup>238</sup> Pu/ <sup>239</sup> Pu ratio and uncertainty   |

**R<sub>89corr</sub>:**

Type A

Method of observation: Direct

Number of observations: 33

| No. | Observation | No. | Observation | No. | Observation |
|-----|-------------|-----|-------------|-----|-------------|
| 1   | 0.002635    | 12  | 0.002646    | 23  | 0.002660    |
| 2   | 0.002635    | 13  | 0.002657    | 24  | 0.002643    |
| 3   | 0.002636    | 14  | 0.002634    | 25  | 0.002777    |
| 4   | 0.002640    | 15  | 0.002635    | 26  | 0.002632    |
| 5   | 0.002637    | 16  | 0.002634    | 27  | 0.002638    |
| 6   | 0.002635    | 17  | 0.002641    | 28  | 0.002634    |
| 7   | 0.002653    | 18  | 0.002661    | 29  | 0.002634    |
| 8   | 0.002634    | 19  | 0.002640    | 30  | 0.002643    |
| 9   | 0.002633    | 20  | 0.002637    | 31  | 0.002632    |
| 10  | 0.002634    | 21  | 0.002634    | 32  | 0.002641    |
| 11  | 0.002635    | 22  | 0.002644    | 33  | 0.002634    |

Arithmetic mean:  $2.64358 \times 10^{-3}$

Standard deviation:  $25 \times 10^{-6}$

Standard uncertainty:  $4.39 \times 10^{-6}$

Degrees of freedom: 32

**R<sub>09corr</sub>:**

Type A

Method of observation: Direct

Number of observations: 54

| No. | Observation | No. | Observation | No. | Observation |
|-----|-------------|-----|-------------|-----|-------------|
| 1   | 0.240611    | 19  | 0.240615    | 37  | 0.240637    |
| 2   | 0.240631    | 20  | 0.240618    | 38  | 0.240631    |
| 3   | 0.240662    | 21  | 0.240617    | 39  | 0.240621    |
| 4   | 0.240614    | 22  | 0.240614    | 40  | 0.240649    |
| 5   | 0.240641    | 23  | 0.240641    | 41  | 0.240640    |
| 6   | 0.240576    | 24  | 0.240620    | 42  | 0.240596    |
| 7   | 0.240595    | 25  | 0.240612    | 43  | 0.240609    |
| 8   | 0.240633    | 26  | 0.240589    | 44  | 0.240628    |
| 9   | 0.240636    | 27  | 0.240639    | 45  | 0.240639    |
| 10  | 0.240640    | 28  | 0.240626    | 46  | 0.240631    |
| 11  | 0.240649    | 29  | 0.240641    | 47  | 0.240619    |
| 12  | 0.240627    | 30  | 0.240632    | 48  | 0.240655    |
| 13  | 0.240621    | 31  | 0.240615    | 49  | 0.240638    |
| 14  | 0.240620    | 32  | 0.240644    | 50  | 0.240638    |
| 15  | 0.240592    | 33  | 0.240660    | 51  | 0.240643    |
| 16  | 0.240677    | 34  | 0.240631    | 52  | 0.240644    |
| 17  | 0.240631    | 35  | 0.240608    | 53  | 0.240611    |
| 18  | 0.240623    | 36  | 0.240640    | 54  | 0.240617    |

Arithmetic mean: 0.24062754

Standard deviation:  $19 \times 10^{-6}$

Standard uncertainty:  $2.59 \times 10^{-6}$

Degrees of freedom: 53

The calculated  $^{240}\text{Pu}/^{239}\text{Pu}$  ratio, Standard Deviation, and number of “Good Points” imported from OakLimbs.

**R<sub>19corr</sub>:**

Type A

Method of observation: Direct

Number of observations: 54

| No. | Observation | No. | Observation | No. | Observation |
|-----|-------------|-----|-------------|-----|-------------|
| 1   | 0.005108    | 19  | 0.005180    | 37  | 0.005116    |
| 2   | 0.005106    | 20  | 0.005170    | 38  | 0.005117    |
| 3   | 0.005107    | 21  | 0.005167    | 39  | 0.005114    |
| 4   | 0.005180    | 22  | 0.005180    | 40  | 0.005115    |
| 5   | 0.005105    | 23  | 0.005162    | 41  | 0.005106    |
| 6   | 0.005110    | 24  | 0.005182    | 42  | 0.005103    |
| 7   | 0.005194    | 25  | 0.005193    | 43  | 0.005099    |
| 8   | 0.005047    | 26  | 0.005075    | 44  | 0.005118    |
| 9   | 0.005054    | 27  | 0.005076    | 45  | 0.005125    |
| 10  | 0.005040    | 28  | 0.005075    | 46  | 0.005091    |
| 11  | 0.005042    | 29  | 0.005074    | 47  | 0.005097    |
| 12  | 0.005113    | 30  | 0.005074    | 48  | 0.005036    |
| 13  | 0.005112    | 31  | 0.005070    | 49  | 0.005101    |
| 14  | 0.005108    | 32  | 0.005069    | 50  | 0.005106    |
| 15  | 0.005110    | 33  | 0.005075    | 51  | 0.005101    |
| 16  | 0.005108    | 34  | 0.005071    | 52  | 0.005069    |
| 17  | 0.005114    | 35  | 0.005110    | 53  | 0.005085    |
| 18  | 0.005111    | 36  | 0.005090    | 54  | 0.005102    |

Arithmetic mean:  $5.10672 \times 10^{-3}$

Standard deviation:  $39 \times 10^{-6}$

Standard uncertainty:  $5.33 \times 10^{-6}$

Degrees of freedom: 53

The calculated <sup>241</sup>Pu/<sup>239</sup>Pu ratio, Standard Deviation, and number of “Good Points” imported from OakLimbs.

**R<sub>29corr</sub>:**

Type A

Method of observation: Direct

Number of observations: 54

| No. | Observation | No. | Observation | No. | Observation |
|-----|-------------|-----|-------------|-----|-------------|
| 1   | 0.015573    | 19  | 0.015573    | 37  | 0.015577    |
| 2   | 0.015578    | 20  | 0.015570    | 38  | 0.015552    |
| 3   | 0.015585    | 21  | 0.015573    | 39  | 0.015577    |
| 4   | 0.015573    | 22  | 0.015573    | 40  | 0.015572    |
| 5   | 0.015577    | 23  | 0.015578    | 41  | 0.015564    |
| 6   | 0.015565    | 24  | 0.015576    | 42  | 0.015551    |
| 7   | 0.015578    | 25  | 0.015576    | 43  | 0.015570    |
| 8   | 0.015579    | 26  | 0.015569    | 44  | 0.015597    |
| 9   | 0.015579    | 27  | 0.015576    | 45  | 0.015585    |
| 10  | 0.015581    | 28  | 0.015581    | 46  | 0.015586    |
| 11  | 0.015586    | 29  | 0.015580    | 47  | 0.015546    |
| 12  | 0.015575    | 30  | 0.015577    | 48  | 0.015617    |
| 13  | 0.015578    | 31  | 0.015577    | 49  | 0.015537    |
| 14  | 0.015576    | 32  | 0.015595    | 50  | 0.015587    |
| 15  | 0.015568    | 33  | 0.015589    | 51  | 0.015600    |
| 16  | 0.015585    | 34  | 0.015596    | 52  | 0.015595    |
| 17  | 0.015578    | 35  | 0.015577    | 53  | 0.015571    |
| 18  | 0.015579    | 36  | 0.015556    | 54  | 0.015589    |

Arithmetic mean: 0.01557700

Standard deviation:  $13 \times 10^{-6}$

Standard uncertainty:  $1.81 \times 10^{-6}$

Degrees of freedom: 53

The calculated <sup>242</sup>Pu/<sup>239</sup>Pu ratio, Standard Deviation, and number of “Good Points” imported from OakLimbs.

$\delta_{\text{Cert}}$ :

Type B normal distribution

Value: 1

Expanded uncertainty:  $2.6 \times 10^{-4}$

Coverage factor: 2

The uncertainty of the decay-corrected  $^{240}\text{Pu}/^{239}\text{Pu}$  on the certificate used as the mass bias standard. This value will be found in OakLimbs → Common → Support Data → Standards → “look up the  $^{240}\text{Pu}/^{239}\text{Pu}$  ratio” with the ID Code used in the mass bias “M” sample.

Example 3M126PuI “M” equals mass bias ID Code is “126”

The decay-corrected  $^{242}\text{Pu}/^{239}\text{Pu}$  value is  $1.00016 \pm 0.00026$

$0.00026/1.00016 = 2.6 \times 10^{-4}$

$\delta_{\text{CFvar}}$ :

Type B normal distribution

Value: 1

Expanded uncertainty: 0.0000764

Coverage factor: 1

Uncertainty in the mass bias factor estimated from the variability in the mass bias measurements across the sequences Since each sample is bracket corrected for mass fractionation throughout a run, the multiplicative correction factor is assumed to be 1. However, uncertainties are assigned to this correction factor based on the relative standard uncertainty of the mass bias measurements across a run. The Std Err on the  $^{240}\text{Pu}/^{239}\text{Pu}$  measurements of the comparator in each sequence

Sequence Average R  $^{242}\text{Pu}/^{239}\text{Pu}$  Std Err % RSE (Comparator)

Average %RSE for the fractionation correction factor =  $1.66961 \times 10^{-7}/\sqrt{21} =$

$^{242}\text{Pu}/^{239}\text{Pu}$  1 CRM 128 1.0017011 2 CRM 128 1.0017348 3 CRM 128 1.0018845 4 CRM 128 1.0014960  
5 CRM 128 1.0015396 6 CRM 128 1.0015440 7 CRM 128 1.0016944 8 CRM 128 1.0017292 9 CRM  
128 1.0016014 10 CRM 128 1.0016866 11 CRM 128 1.0015384 12 CRM 128 1.0015404 13 CRM 128  
1.0016134 14 CRM 128 1.0015081 15 CRM 128 1.0021248 16 CRM 128 1.0014634 17 CRM 128  
1.0016042 18 CRM 128 1.0020550 19 CRM 128 1.0004350 20 CRM 128 1.0019940 21 CRM 128  
1.0021628 Average 1.0016501 Std Dev 0.0003503 %RSD 0.035% SE 0.0000764 %RSE 0.008%

$\delta_{\text{seq}}$ :

Type B normal distribution

Value: 0

Expanded uncertainty: 0.000010

Coverage factor: 1

Normalized sequence variation obtained from first control analyzed for  $^{240}\text{Pu}/^{239}\text{Pu}$  divided by the number of points in the control chart ( $N$ ). Therefore, normalized sequence variation is sequence variation/sqrt( $N$ ) = (standard uncertainty)

$^{240}\text{Pu}/^{239}\text{Pu}$  0.240659 0.240672 0.240659 0.240692 0.240659 0.240706 0.240641 0.240641 0.240629  
0.240632 0.240585 0.240595 0.240648 0.000035 0.015% 0.000010 0.0042%

$\delta_{seq2}$ :

Type B normal distribution

Value: 0

Expanded uncertainty: 0.0000068

Coverage factor: 1

Normalized sequence variation obtained from first control analyzed for  $^{241}\text{Pu}/^{239}\text{Pu}$  divided by the number of points in the control chart ( $N$ ). Therefore, normalized sequence variation is sequence variation/ $\sqrt{N}$  = (standard uncertainty)

$^{241}\text{Pu}/^{239}\text{Pu}$  0.0051793 0.0051876 0.0051872 0.0051708 0.0051891 0.0051407 0.0051749 0.0051749 0.0051343 0.0051323 0.0051311 0.0051459 0.0051623 0.0000235 0.45% 0.0000068 0.13%

$\delta_{seq3}$ :

Type B normal distribution

Value: 0

Expanded uncertainty: 0.0000016

Coverage factor: 1

Normalized sequence variation obtained from first control analyzed for  $^{242}\text{Pu}/^{239}\text{Pu}$  divided by the number of points in the control chart ( $N$ ). Therefore, normalized sequence variation is sequence variation/ $\sqrt{N}$  = (standard uncertainty)

$^{242}\text{Pu}/^{239}\text{Pu}$  0.0155814 0.0155810 0.0155813 0.0155885 0.0155795 0.0155926 0.0155800 0.0155800 0.0155780 0.0155768 0.0155734 0.0155723 0.0155804 0.0000056 0.036% 0.0000016 0.010%

$\delta_{seq4}$ :

Type B normal distribution

Value: 0

Expanded uncertainty: 0.0000020

Coverage factor: 1

Normalized sequence variation obtained from first control analyzed for  $^{238}\text{Pu}/^{239}\text{Pu}$  divided by the number of points in the control chart ( $N$ ). Therefore, normalized sequence variation is sequence variation/ $\sqrt{N}$  = (standard uncertainty)

Rep STD  $^{238}\text{Pu}/^{239}\text{Pu}$  1 CRM 137 0.0026357 2 CRM 137 0.0026352 3 CRM 137 0.0026575 4 CRM 137 0.0026372 5 CRM 137 0.0026358 6 CRM 137 0.0026432 7 CRM 137 0.0026389 8 CRM 137 0.0026388 9 CRM 137 0.0026323 10 CRM 137 0.0026310 11 CRM 137 0.0026337 12 CRM 137 0.0026344 Average 0.0026378 Std Dev 0.0000070 %RSD 0.27% SE 0.0000020 %RSE 0.077%

### Input Correlation

|                     | $R_{89\text{corr}}$ | $R_{09\text{corr}}$ | $R_{19\text{corr}}$ | $R_{29\text{corr}}$ |
|---------------------|---------------------|---------------------|---------------------|---------------------|
| $R_{89\text{corr}}$ | 1                   | -0.4174             | 0.7846              | -0.0471             |
| $R_{09\text{corr}}$ | -0.4174             | 1                   | -0.5457             | 0.8651              |
| $R_{19\text{corr}}$ | 0.7846              | -0.5457             | 1                   | -0.4151             |
| $R_{29\text{corr}}$ | -0.0471             | 0.8651              | -0.4151             | 1                   |



**Uncertainty Budgets:**

**R<sub>09</sub>: The final <sup>240</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>09corr</sub>     | 0.24062754 | $2.59 \times 10^{-6}$ | normal       | 1.0                     | $2.6 \times 10^{-6}$     | 0.5%  |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.24                    | $31 \times 10^{-6}$      | 68.8% |
| $\delta_{\text{CFVar}}$ | 1.000000   | $76.4 \times 10^{-6}$ | normal       | 0.24                    | $18 \times 10^{-6}$      | 23.7% |
| $\delta_{\text{seq}}$   | 0.0        | $10.0 \times 10^{-6}$ | normal       | 1.0                     | $10 \times 10^{-6}$      | 7.0%  |
| R <sub>09</sub>         | 0.2406275  | $37.7 \times 10^{-6}$ |              |                         |                          |       |

**R<sub>19</sub>: The final <sup>241</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>19corr</sub>     | $5.10672 \times 10^{-3}$ | $5.33 \times 10^{-6}$ | normal       | 1.0                     | $5.3 \times 10^{-6}$     | 37.8% |
| $\delta_{\text{Cert}}$  | 1.000000                 | $130 \times 10^{-6}$  | normal       | $5.1 \times 10^{-3}$    | $660 \times 10^{-9}$     | 0.6%  |
| $\delta_{\text{CFVar}}$ | 1.000000                 | $76.4 \times 10^{-6}$ | normal       | $5.1 \times 10^{-3}$    | $390 \times 10^{-9}$     | 0.2%  |
| $\delta_{\text{seq2}}$  | 0.0                      | $6.80 \times 10^{-6}$ | normal       | 1.0                     | $6.8 \times 10^{-6}$     | 61.5% |
| R <sub>19</sub>         | $5.10672 \times 10^{-3}$ | $8.67 \times 10^{-6}$ |              |                         |                          |       |

**R<sub>29</sub>: The final <sup>242</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value      | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>29corr</sub>     | 0.01557700 | $1.81 \times 10^{-6}$ | normal       | 1.0                     | $1.8 \times 10^{-6}$     | 28.8% |
| $\delta_{\text{Cert}}$  | 1.000000   | $130 \times 10^{-6}$  | normal       | 0.016                   | $2.0 \times 10^{-6}$     | 36.2% |
| $\delta_{\text{CFVar}}$ | 1.000000   | $76.4 \times 10^{-6}$ | normal       | 0.016                   | $1.2 \times 10^{-6}$     | 12.5% |
| $\delta_{\text{seq3}}$  | 0.0        | $1.60 \times 10^{-6}$ | normal       | 1.0                     | $1.6 \times 10^{-6}$     | 22.6% |
| R <sub>29</sub>         | 0.01557700 | $3.37 \times 10^{-6}$ |              |                         |                          |       |

**R<sub>89</sub>: The final <sup>238</sup>Pu/<sup>239</sup>Pu ratio and uncertainty**

| Quantity                | Value                    | Standard uncertainty  | Distribution | Sensitivity coefficient | Uncertainty contribution | Index |
|-------------------------|--------------------------|-----------------------|--------------|-------------------------|--------------------------|-------|
| R <sub>89corr</sub>     | $2.64358 \times 10^{-3}$ | $4.39 \times 10^{-6}$ | normal       | 1.0                     | $4.4 \times 10^{-6}$     | 82.2% |
| $\delta_{\text{Cert}}$  | 1.000000                 | $130 \times 10^{-6}$  | normal       | $2.6 \times 10^{-3}$    | $340 \times 10^{-9}$     | 0.5%  |
| $\delta_{\text{CFVar}}$ | 1.000000                 | $76.4 \times 10^{-6}$ | normal       | $2.6 \times 10^{-3}$    | $200 \times 10^{-9}$     | 0.2%  |
| $\delta_{\text{seq4}}$  | 0.0                      | $2.00 \times 10^{-6}$ | normal       | 1.0                     | $2.0 \times 10^{-6}$     | 17.1% |
| R <sub>89</sub>         | $2.64358 \times 10^{-3}$ | $4.84 \times 10^{-6}$ |              |                         |                          |       |

**Results:**

| Quantity        | Value                   | Expanded uncertainty | Coverage factor | Coverage     |
|-----------------|-------------------------|----------------------|-----------------|--------------|
| R <sub>09</sub> | 0.240628                | $75 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>19</sub> | $5.107 \times 10^{-3}$  | $17 \times 10^{-6}$  | 2.00            | 95% (normal) |
| R <sub>29</sub> | 0.0155770               | $6.7 \times 10^{-6}$ | 2.00            | 95% (normal) |
| R <sub>89</sub> | $2.6436 \times 10^{-3}$ | $9.7 \times 10^{-6}$ | 2.00            | 95% (normal) |

**Result Correlation:**

|                 | R <sub>09</sub> | R <sub>19</sub> | R <sub>29</sub> | R <sub>89</sub> |
|-----------------|-----------------|-----------------|-----------------|-----------------|
| R <sub>09</sub> | 1               | 0.0624          | 0.7026          | 0.0532          |
| R <sub>19</sub> | 0.0624          | 1               | -0.0749         | 0.4445          |
| R <sub>29</sub> | 0.7026          | -0.0749         | 1               | 0.0345          |
| R <sub>89</sub> | 0.0532          | 0.4445          | 0.0345          | 1               |

## Appendix F. Representative Alpha Counting GUM WORKBENCH

### Pu 238/239 Alpha

Author: kt4

#### Model Equation:

*{Ratio}*

$$R = mol_{238} / mol_{239};$$

*{Convert back to mol}*

$$mol_{240} = G_{found240} / AW_{240};$$

$$mol_{239} = G_{found239} / AW_{239};$$

$$mol_{238} = G_{found238} / AW_{238};$$

*{Convert back to grams}*

$$G_{found240} = A_{meas240} / SA_{240};$$

$$G_{found239} = A_{meas239} / SA_{239};$$

$$G_{found238} = A_{meas238} / SA_{238};$$

*{Activity in measurement}*

$$A_{meas240} = (AcP_{240} * Ac_{240239}) / 1000 / 1000 / 1000 / 1000;$$

$$A_{meas239} = (AcP_{239} * Ac_{240239}) / 1000 / 1000 / 1000 / 1000;$$

$$A_{meas238} = Ac_{238} / 1000 / 1000 / 1000 / 1000;$$

*{Activity Percent}*

$$AcP_{240} = Ci_{240} / Ci_{total};$$

$$AcP_{239} = Ci_{239} / Ci_{total};$$

$$Ci_{total} = Ci_{240} + Ci_{239};$$

*{Ci ratio}*

$$Ci_{240} = g_{240} * SA_{240};$$

$$Ci_{239} = g_{239} * SA_{239};$$

$$g_{240} = AW_{240} * R_{09};$$

$$g_{239} = AW_{239}$$

#### List of Quantities:

| Quantity          | Unit   | Definition  |
|-------------------|--------|---|
| Ac <sub>238</sub> | pCi/mL | Alpha spec instrument response intensity of the combined Pu238 peak |

| Quantity       | Unit    | Definition  |
|----------------|---------|---|
| $Ac_{240/239}$ | pCi/mL  | Alpha spec instrument response intensity of the combined Pu239/240 peak |
| $AW_{238}$     | g/mol   | Atomic weight   |
| $AW_{239}$     | g/mol   | Atomic weight   |
| $AW_{240}$     | g/mol   | Atomic weight   |
| $R_{09}$       | mol:mol | Ratio of 239:240 from TIMS data   |
| $SA_{239}$     | Ci/g    | Specific activity of 239  |
| $SA_{240}$     | Ci/g    | Specific activity of 240  |
| $SA_{238}$     | Ci/g    | Specific activity of 338  |
| $mol_{238}$    | mol     | Conversion to mols for 238  |
| $mol_{239}$    | mol     | Conversion to mols for 239  |
| $G_{found240}$ | g       | Convert back to grams for mass 240                                      |
| $G_{found239}$ | g       | Convert back to grams for mass 239                                      |
| $G_{found238}$ | g       | Convert back to grams for mass 238                                      |
| $A_{meas240}$  | Ci/mL   | 240 activity in measured  |
| $A_{meas239}$  | Ci/mL   | 239 activity in measured  |
| $A_{meas238}$  | Ci/mL   | 238 activity in measured  |
| $AcP_{240}$    | %       | Ci:Ci activity fraction for 239:240 using TIMS data                     |
| $AcP_{239}$    | %       | Ci:Ci activity fraction for 239:240 using TIMS data                     |
| $Ci_{240}$     | Ci      | Curies of 240   |
| $Ci_{total}$   | Ci      | Sum of the Ci activity of 238, 239 & 240                                |
| $Ci_{239}$     | Ci      | Curies of 239   |
| $g_{240}$      | g       | Grams of 240  |
| $g_{239}$      | g       | Grams of 239  |
| $R$            | mol/mol | Final ratio mol:mol of 238:239  |
| $mol_{240}$    | mol     | Conversion to mols for 240  |

**$Ac_{238}$ :**

Type B normal distribution

Value:  $3.289 \cdot 10^{+3}$  pCi/mL

Expanded Uncertainty: 353.8 pCi/mL

Coverage Factor: 2

**$Ac_{240/239}$ :**

Type B normal distribution

Value:  $8.3580 \cdot 10^{+3}$  pCi/mL

Expanded Uncertainty: 780.8 pCi/mL

Coverage Factor: 2

**AW<sub>238</sub>:**

Type B normal distribution

Value: 238.049559 g/mol

Expanded Uncertainty: 0.0000019 g/mol

Coverage Factor: 2

**AW<sub>239</sub>:**

Type B normal distribution

Value: 239.0521636 g/mol

Expanded Uncertainty: .0000019 g/mol

Coverage Factor: 2

**AW<sub>240</sub>:**

Type B normal distribution

Value: 240.0538138 g/mol

Expanded Uncertainty: .0000019 g/mol

Coverage Factor: 2

**R<sub>09</sub>:**

Type B normal distribution

Value: 0.240626 mol:mol

Expanded Uncertainty: 0.0000076 mol:mol

Coverage Factor: 2

**SA<sub>239</sub>:**

Constant

Value:  $6.20400 \cdot 10^{-2}$  Ci/g**SA<sub>240</sub>:**

Constant

Value: 0.22696 Ci/g

**SA<sub>238</sub>:**

Constant

Value:  $1.7119 \cdot 10^{+1}$  Ci/g**Uncertainty Budgets:****R: Final ratio mol:mol of 238:239**

| Quantity          | Value       | Standard Uncertainty | Distribution | Sensitivity Coefficient | Uncertainty Contribution    | Index  |
|-------------------|-------------|----------------------|--------------|-------------------------|-----------------------------|--------|
| Ac <sub>238</sub> | 3289 pCi/mL | 177 pCi/mL           | normal       | $820 \cdot 10^{-9}$     | $150 \cdot 10^{-6}$ mol/mol | 56.9 % |

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| Quantity              | Value                          | Standard Uncertainty          | Distribution | Sensitivity Coefficient | Uncertainty Contribution      | Index  |
|-----------------------|--------------------------------|-------------------------------|--------------|-------------------------|-------------------------------|--------|
| Ac <sub>240239</sub>  | 8358 pCi/mL                    | 390 pCi/mL                    | normal       | -320·10 <sup>-9</sup>   | -130·10 <sup>-6</sup> mol/mol | 43.1 % |
| AW <sub>238</sub>     | 238.049559000 g/mol            | 950·10 <sup>-9</sup> g/mol    | normal       | -11·10 <sup>-6</sup>    | -11·10 <sup>-12</sup> mol/mol | 0.0 %  |
| AW <sub>239</sub>     | 239.052163600 g/mol            | 950·10 <sup>-9</sup> g/mol    | normal       | 6.0·10 <sup>-6</sup>    | 5.7·10 <sup>-12</sup> mol/mol | 0.0 %  |
| AW <sub>240</sub>     | 240.053813800 g/mol            | 950·10 <sup>-9</sup> g/mol    | normal       | 5.3·10 <sup>-6</sup>    | 5.0·10 <sup>-12</sup> mol/mol | 0.0 %  |
| R <sub>09</sub>       | 0.24062600 mol:mol             | 3.80·10 <sup>-6</sup> mol:mol | normal       | 5.3·10 <sup>-3</sup>    | 20·10 <sup>-9</sup> mol/mol   | 0.0 %  |
| SA <sub>239</sub>     | 0.06204 Ci/g                   |                               |              |                         |                               |        |
| SA <sub>240</sub>     | 0.22696 Ci/g                   |                               |              |                         |                               |        |
| SA <sub>238</sub>     | 17.119 Ci/g                    |                               |              |                         |                               |        |
| mol <sub>238</sub>    | 807.1·10 <sup>-15</sup> mol    | 43.4·10 <sup>-15</sup> mol    |              |                         |                               |        |
| mol <sub>239</sub>    | 299.1·10 <sup>-12</sup> mol    | 14.0·10 <sup>-12</sup> mol    |              |                         |                               |        |
| G <sub>found239</sub> | 71.51·10 <sup>-9</sup> g       | 3.34·10 <sup>-9</sup> g       |              |                         |                               |        |
| G <sub>found238</sub> | 192.1·10 <sup>-12</sup> g      | 10.3·10 <sup>-12</sup> g      |              |                         |                               |        |
| A <sub>meas239</sub>  | 4.436·10 <sup>-9</sup> Ci/mL   | 207·10 <sup>-12</sup> Ci/mL   |              |                         |                               |        |
| A <sub>meas238</sub>  | 3.289·10 <sup>-9</sup> Ci/mL   | 177·10 <sup>-12</sup> Ci/mL   |              |                         |                               |        |
| AcP <sub>239</sub>    | 0.53079488 %                   | 3.93·10 <sup>-6</sup> %       |              |                         |                               |        |
| Ci <sub>240</sub>     | 13.109933 Ci                   | 207·10 <sup>-6</sup> Ci       |              |                         |                               |        |
| Ci <sub>total</sub>   | 27.940730 Ci                   | 207·10 <sup>-6</sup> Ci       |              |                         |                               |        |
| Ci <sub>239</sub>     | 14.8307962297 Ci               | 58.9·10 <sup>-9</sup> Ci      |              |                         |                               |        |
| g <sub>240</sub>      | 57.763189 g                    | 912·10 <sup>-6</sup> g        |              |                         |                               |        |
| g <sub>239</sub>      | 239.052163600 g                | 950·10 <sup>-9</sup> g        |              |                         |                               |        |
| R                     | 2.698·10 <sup>-3</sup> mol/mol | 192·10 <sup>-6</sup> mol/mol  |              |                         |                               |        |

### Results:

| Quantity | Value                         | Expanded Uncertainty         | Coverage factor | Coverage     |
|----------|-------------------------------|------------------------------|-----------------|--------------|
| R        | 2.70·10 <sup>-3</sup> mol/mol | 380·10 <sup>-6</sup> mol/mol | 2.00            | 95% (normal) |

