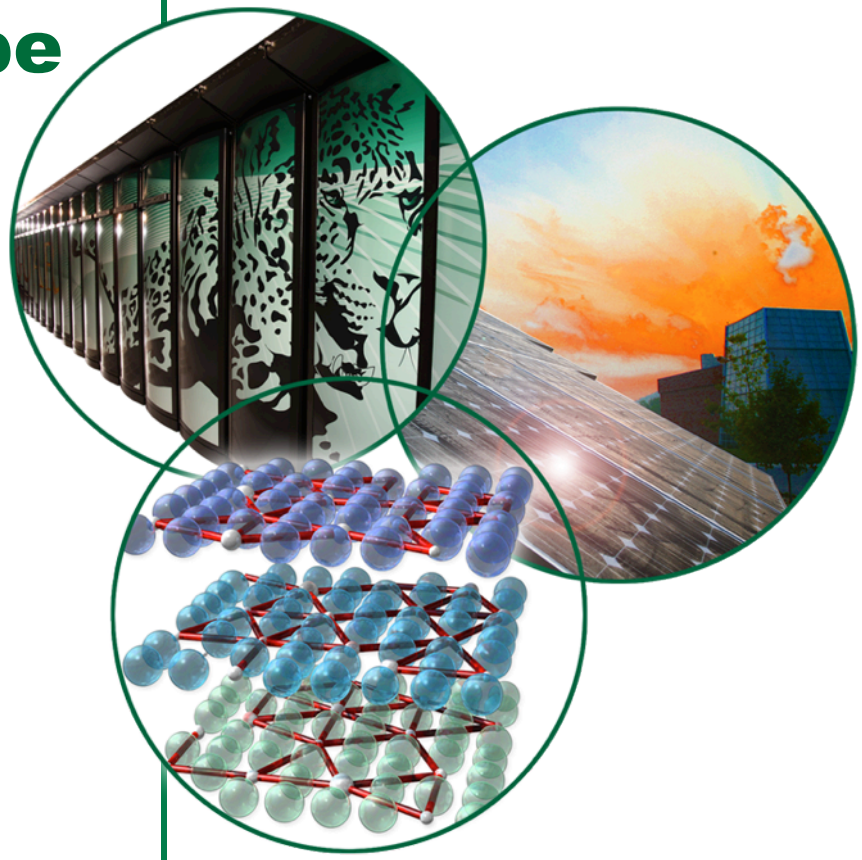
COMSOL Simulations for Steady State Thermal Hydraulics Analyses of ORNL's High Flux Isotope Reactor (HFIR)

COMSOL CONFERENCE BOSTON 2012



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October 03, 2012

U.S. DEPARTMENT OF ENERGY

RNSD Reactor and Nuclear Systems Division

HFIR

OAK RIDGE NATIONAL LABORATORY

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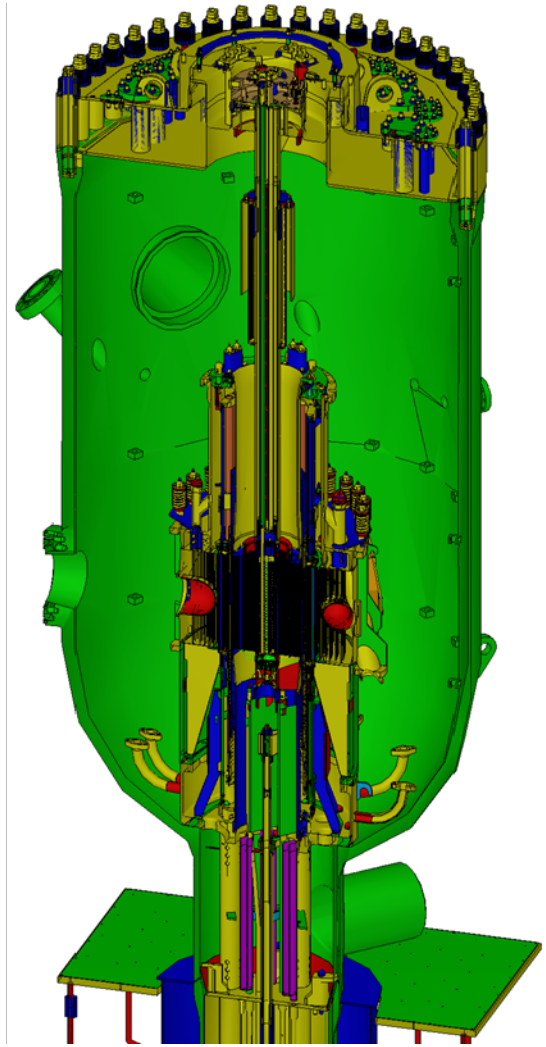
HFIR is a Multi-Purpose High-Performance Research Reactor

- Operated since 1966 with one of the world's highest thermal neutron fluxes ~2.5×10^{15} neutrons/(cm^2-s)
- Involute-shaped fuel plates, beryllium reflected, light water-cooled and –moderated, pressurized, flux-trap type research reactor
- Highly enriched uranium (~93% $^{235}U/U$) fuel embedded in aluminum-6061 clad
- Cold and thermal neutron scattering, materials irradiation, isotope production, neutron activation analysis



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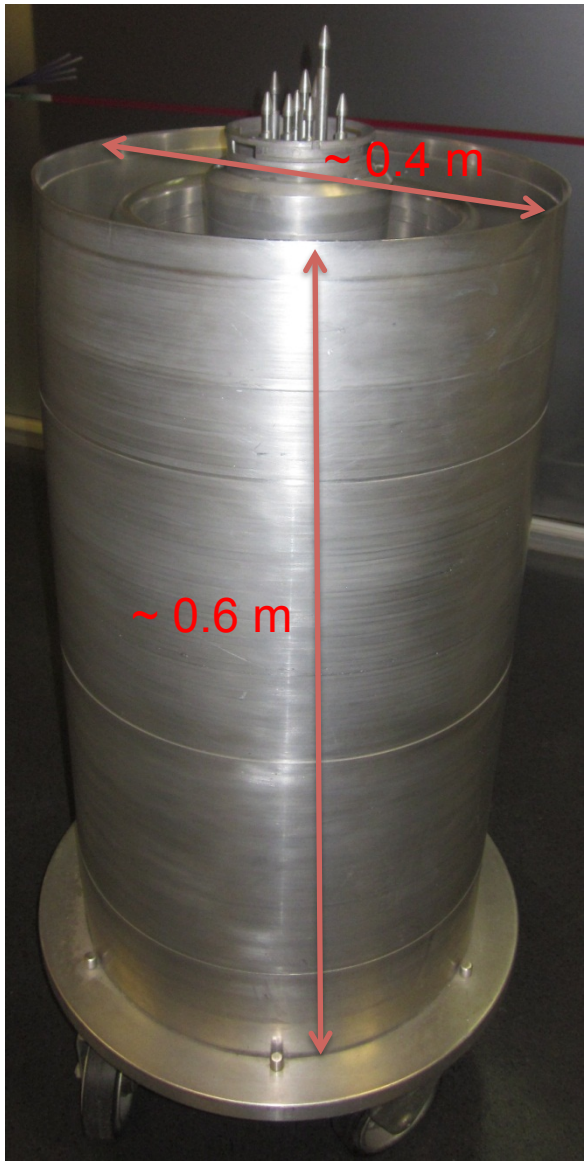
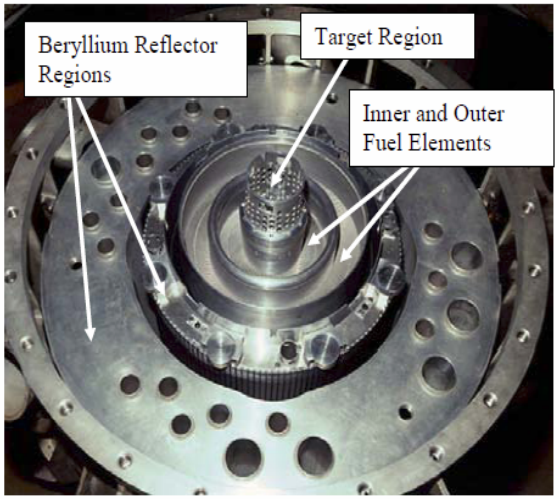
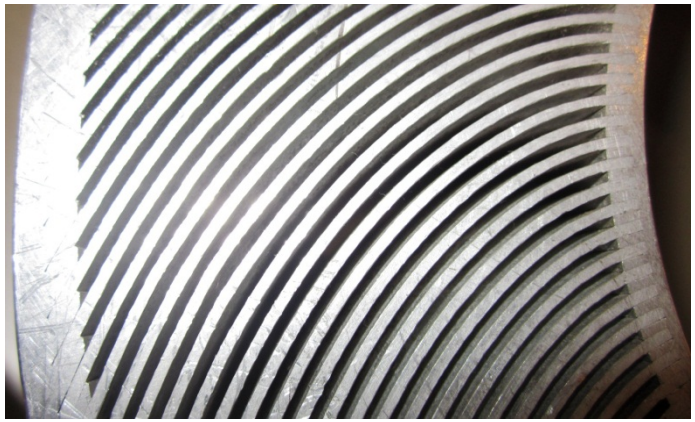
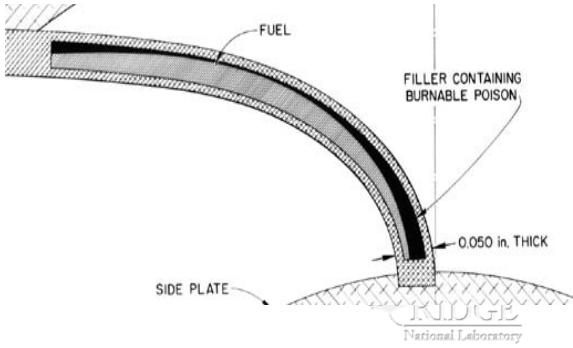
The HFIR Core









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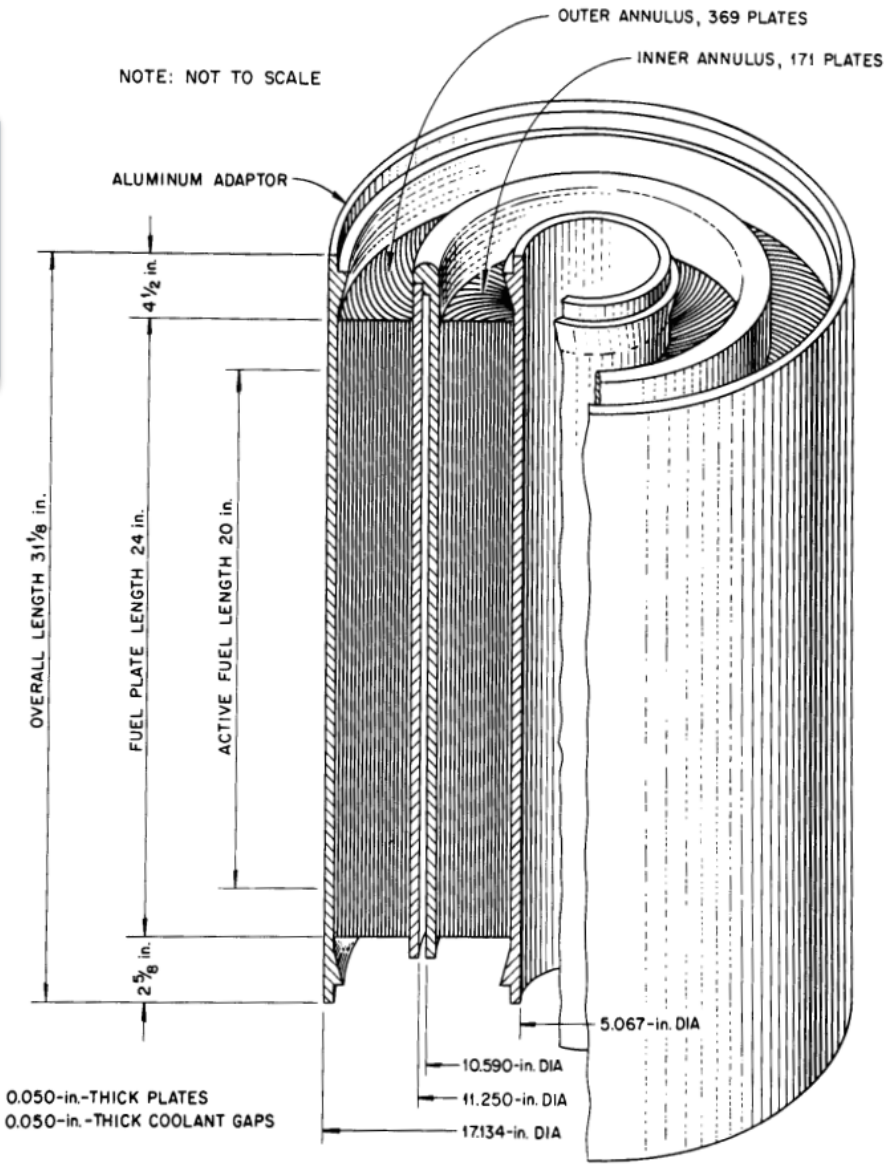
Physics of Interest for HFIR LEU Safety Analyses

- Reactor Physics
- Turbulent Flows
- Conjugate Heat Transfer
- Thermal Structural Interaction (TSI)
- Fluid Structural Interaction (FSI)

- <u>Unique features for HFIR modeling</u>
  - Multi-physics problem
  - Non-uniform spatial heat source distribution inside the fuel plates (fuel, mixture, clad, radial and axial variation)
  - Nonlinear material property variation (~f(T))
  - Very narrow flow channels
    - High aspect ratio = H/t = 24 inch/0.05 inch = 480
  - Desired high level of accuracy and fidelity because of impacts on nuclear safety



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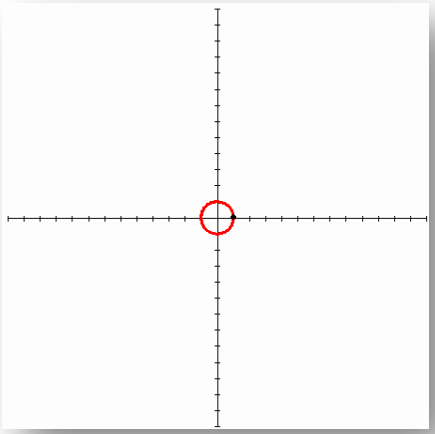
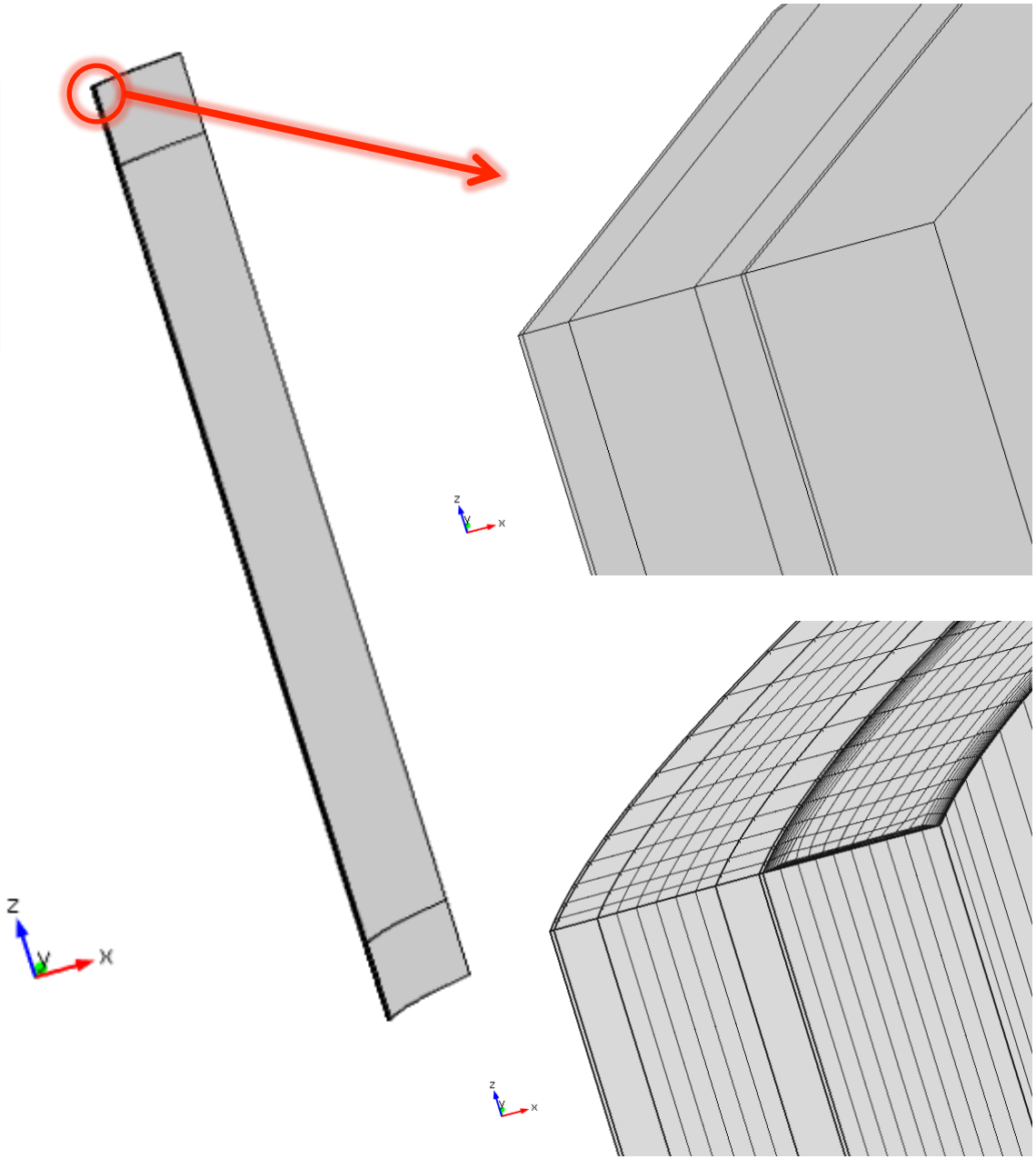
Parametric Geometry and Mapped Meshing

$$x(s) = R_{b_i}\left[sin(s) - s \cdot cos(s)\right],$$
$$y(s) = R_{b_i}\left[cos(s) + s \cdot sin(s)\right], \quad \text{where}$$
$$\theta_{\min} \leq s \leq \theta_{\max},$$
R_{b_i} = base radius of the involute, and
$\theta_{\min}$ = angle for the starting point of the involute, and
$\theta_{\max}$ = angle for the end point of the involute.



Equation of the involute of a circle



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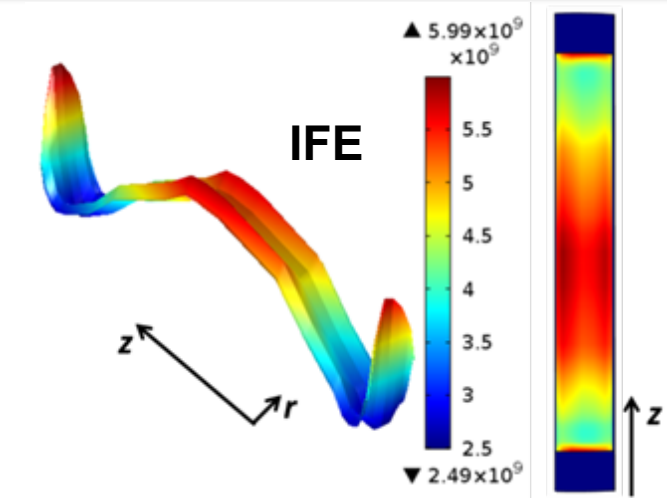
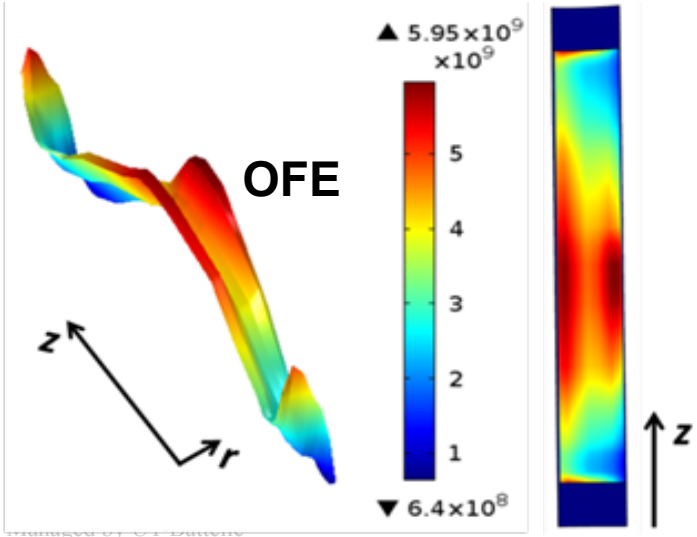
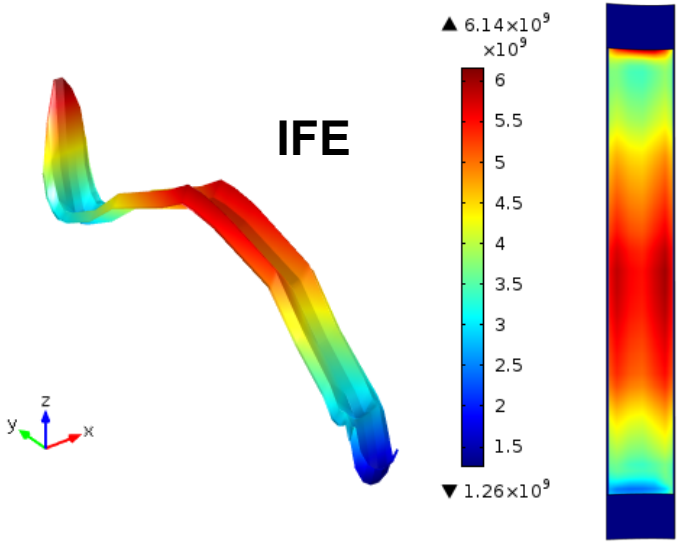
Volumetric Heat Source Distributions

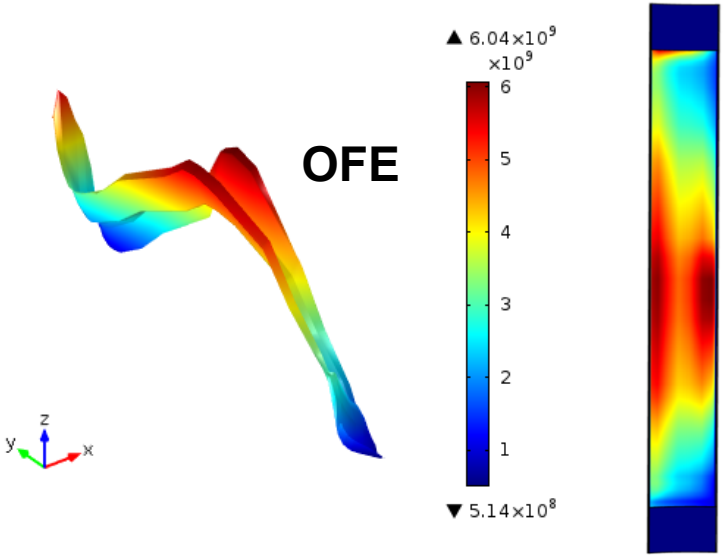
Axially Non-Contoured Fuel Plates





Axially Contoured Fuel Plates





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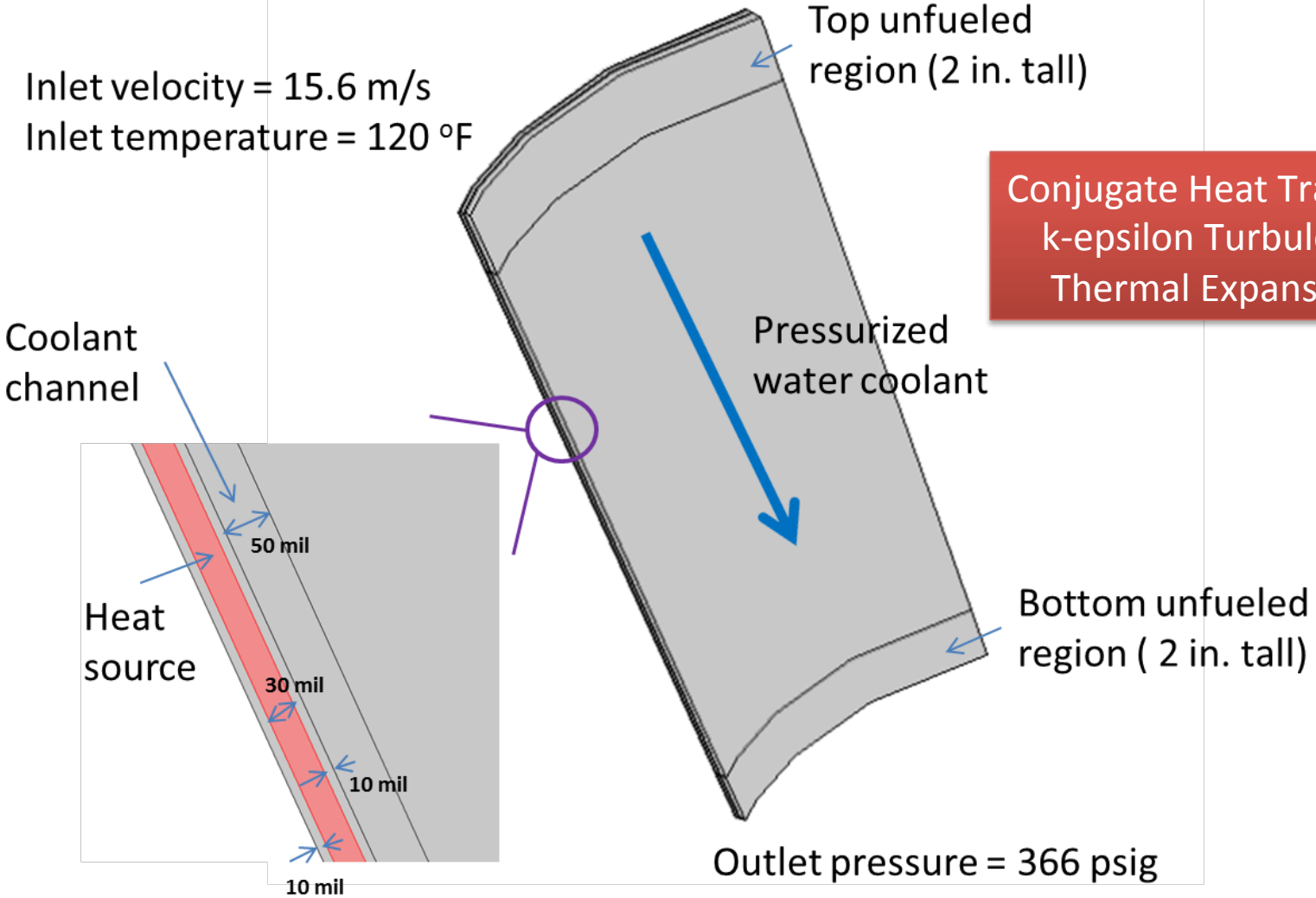
Simulation for Nominal Operation at the Beginning of Reactor Cycle

Inlet velocity = 15.6 m/s
Inlet temperature = 120 °F



Conjugate Heat Transfer Physics
k-epsilon Turbulence Model
Thermal Expansion Physics

Note 1 mil = 0.001 in

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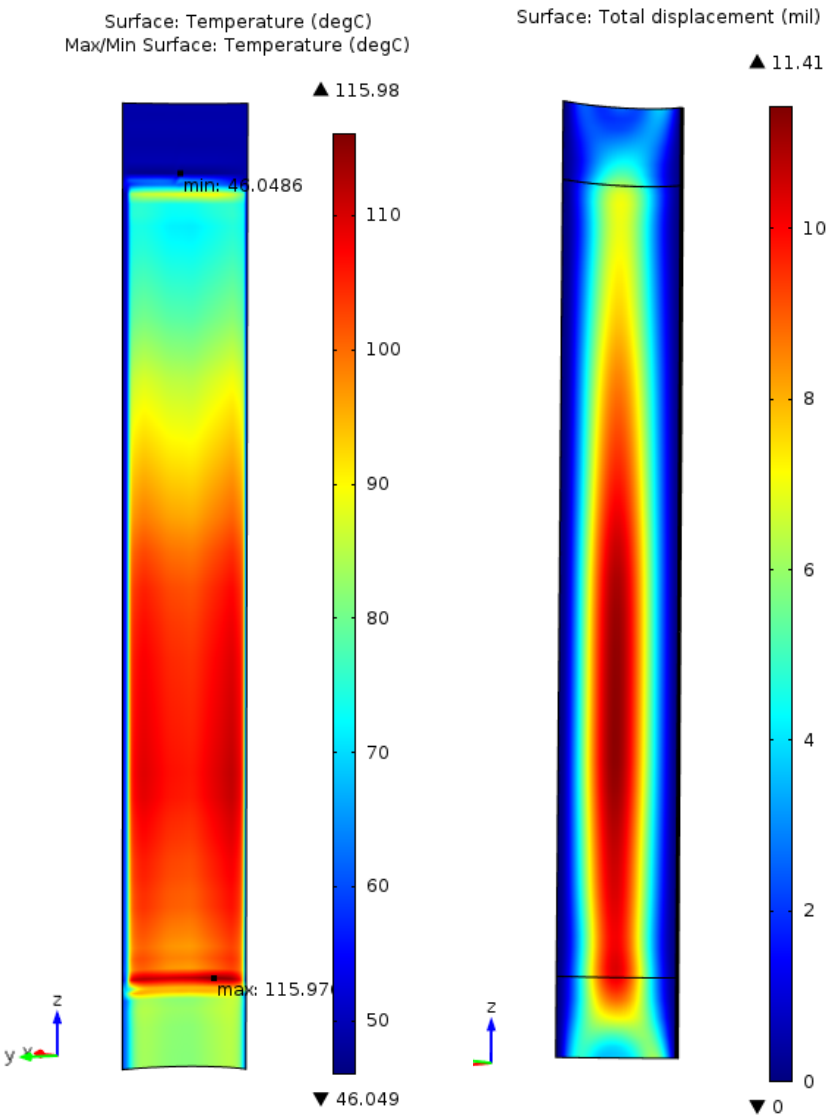
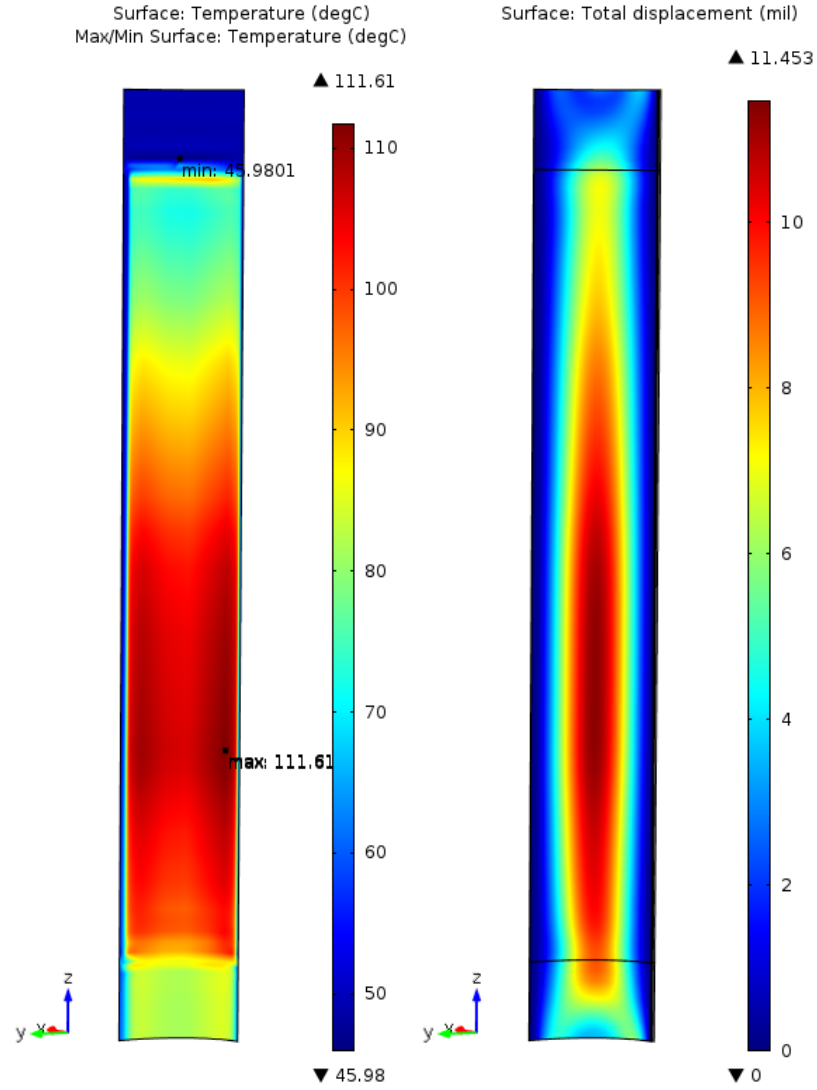
Inner Fuel Element – Nominal Conditions

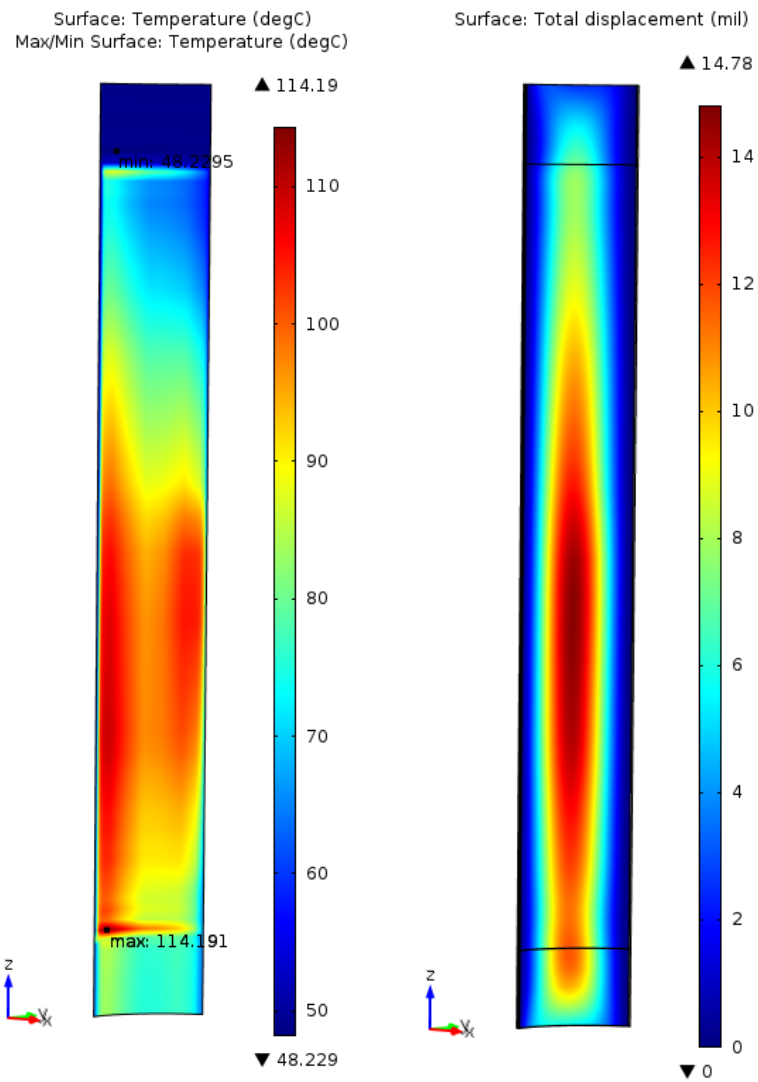


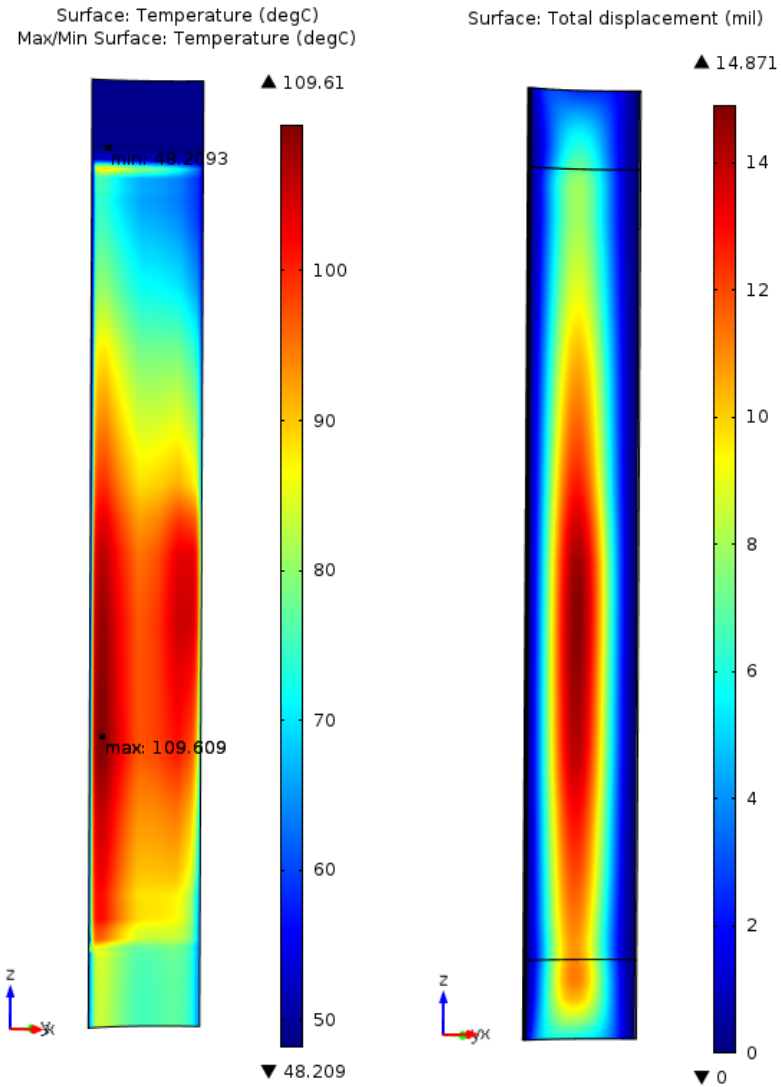
Axially Non-Contoured Fuel Plates



Axially Contoured Fuel Plates

Outer Fuel Element – Nominal Conditions





Axially Non-Contoured Fuel Plates

Axially Contoured Fuel Plates

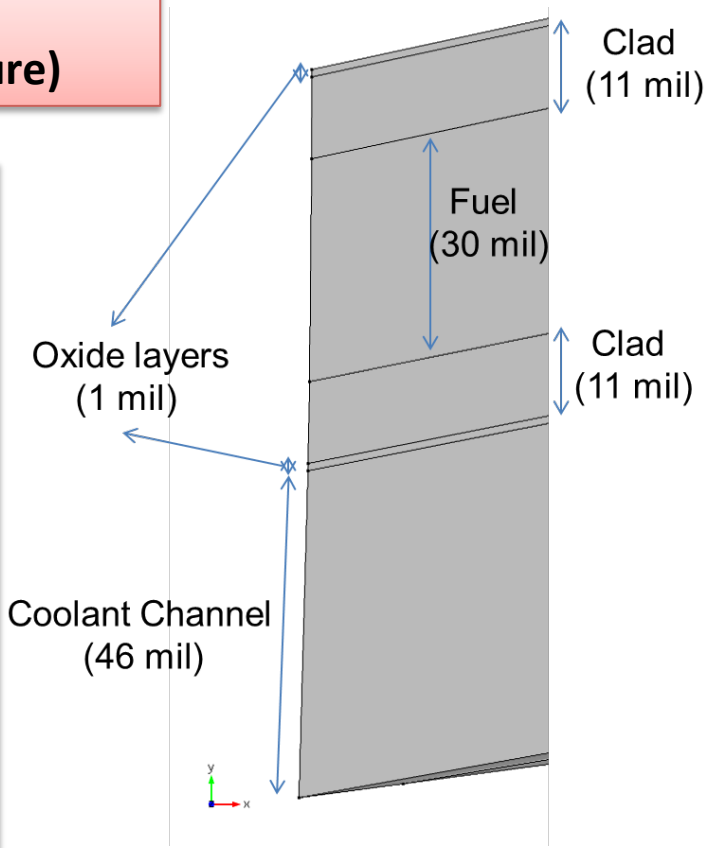
"Hot Channel" Safety Basis Cases at the Beginning Of Cycle

Conservative boundary conditions
(135 ºF inlet temperature and 232.7 psia outlet pressure)

- U2 = Uncertainty in the fissile loading = **1.05**
- U3 = Uncertainty in the power density distribution = **1.199**
- U4 = Uncertainty in average fuel concentration in hot plate = **1.06**
- U18 = Fuel Segregration Flux Peaking = **1.1**

- Ueff = U2*U3*U4*U18 = **1.4679**

- Effective heat source =
  Ueff*PowerFactor*MCNP_Power



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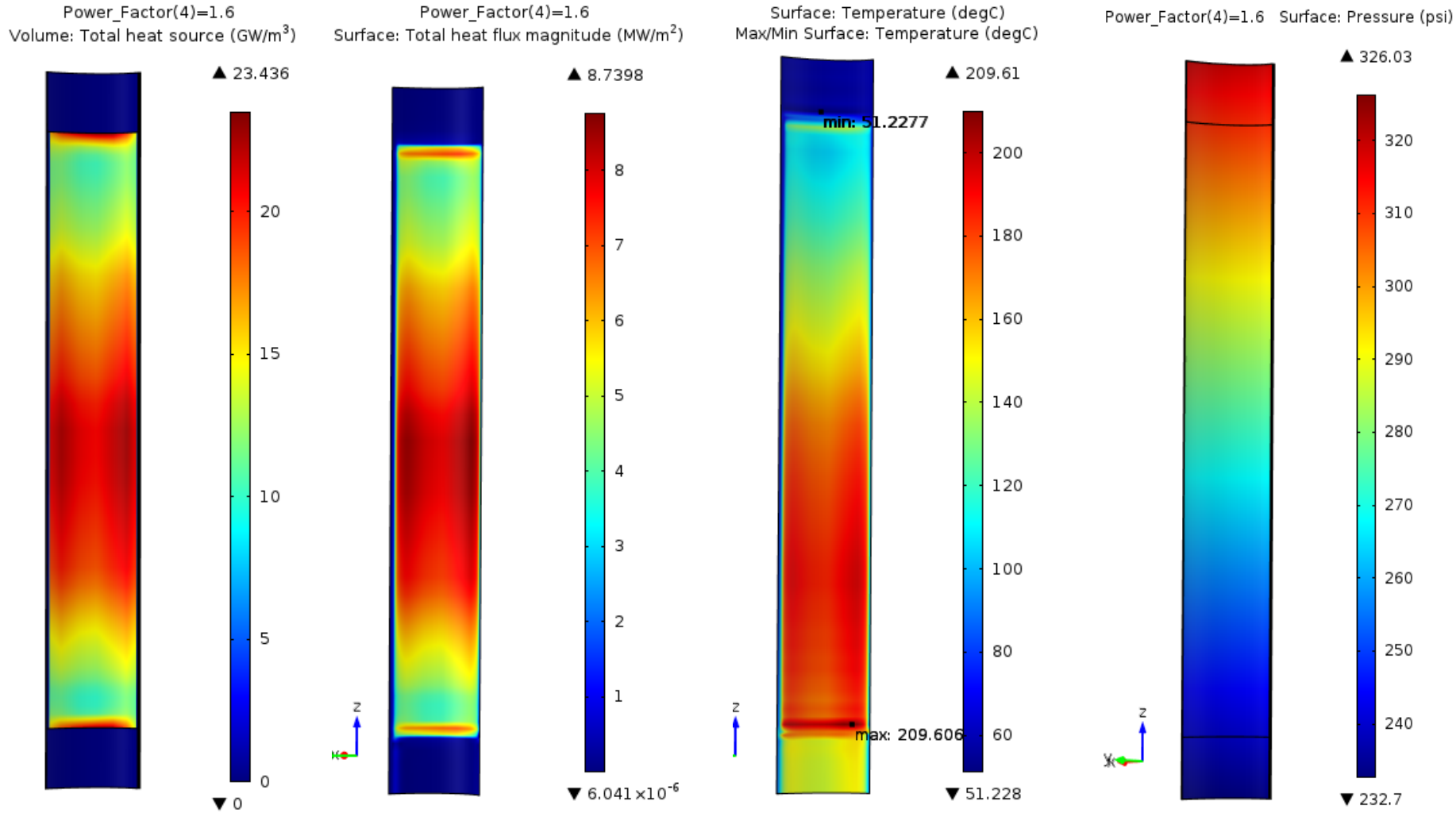
IFE, Axially Non-Contoured LEU Fuel

Power Factor = 1.6



Heat Source (Q"')

Clad Heat Flux (q")

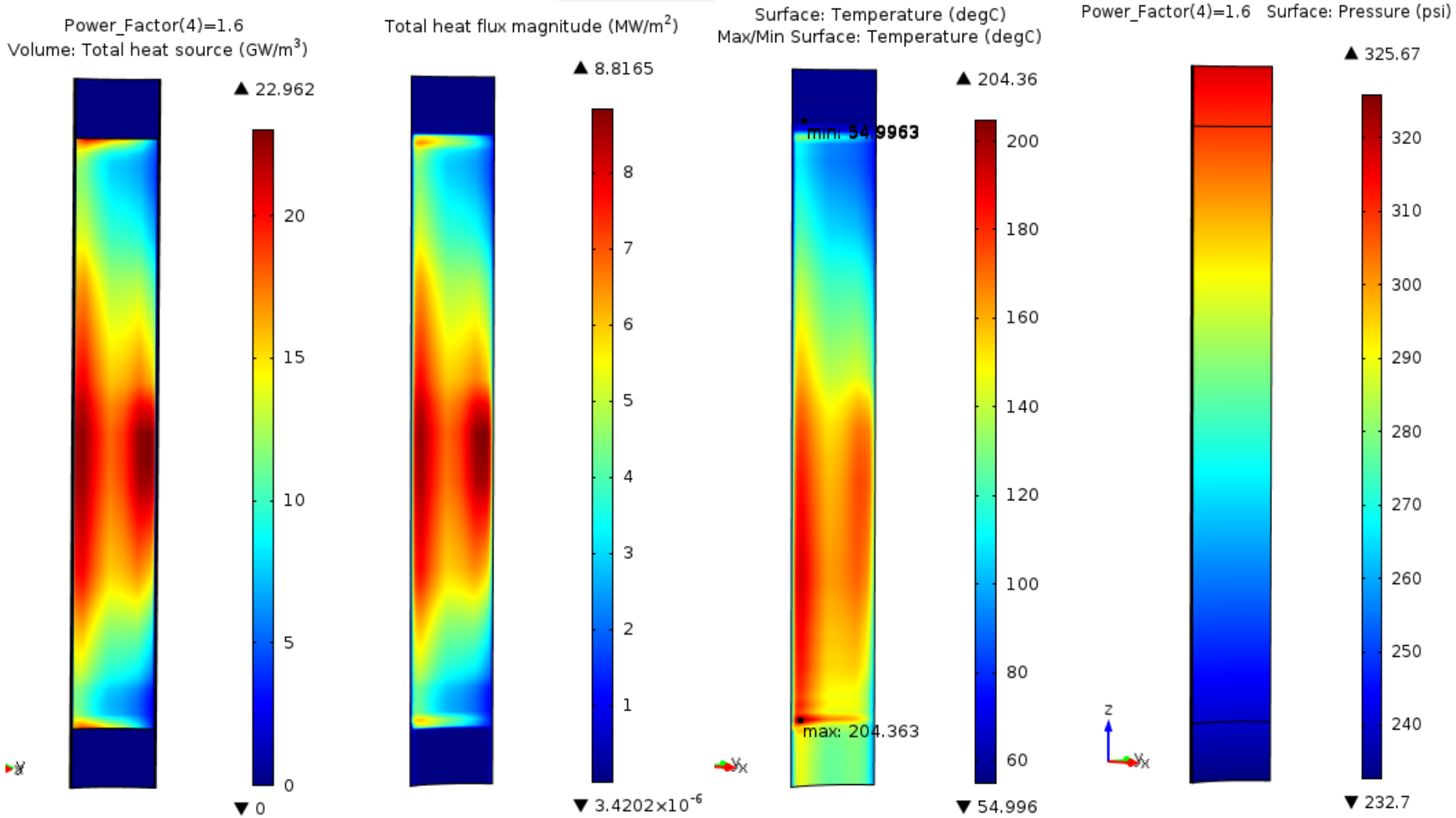
Clad Temperature (T)

Coolant Pressure (P)

of Energy

OFE, Axially Non-Contoured LEU Fuel

Power Factor = 1.6



Heat Source (Q"')

Clad Heat Flux (q")

Clad Temperature (T)

Coolant Pressure (P)

Conclusions and Future Directions

- COMSOL Multiphysics is providing a robust platform to simulate HFIR fuel plates and coolant channels.
- Models developed for IFE and OFE are continually being advanced with a goal to simulate HFIR's safety basis conditions (or, worst possible conditions).
- Preliminary work is also underway to develop a one-dimensional HFIR system model with the primary/secondary piping loops, heat exchangers, pumps, valves and bends. This model is based on HFIR's existing RELAP5 models.
- Coupled CFD/SM models of IFE and OFE could later be coupled with the HFIR system model.
- Parallel and scalable solvers in COMSOL need to be improved and made easier to implement to allow significantly "bigger" HFIR simulations on leadership class computing clusters (e.g., Jaguar/Titan, Kraken etc.).

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Thank you for your attention.

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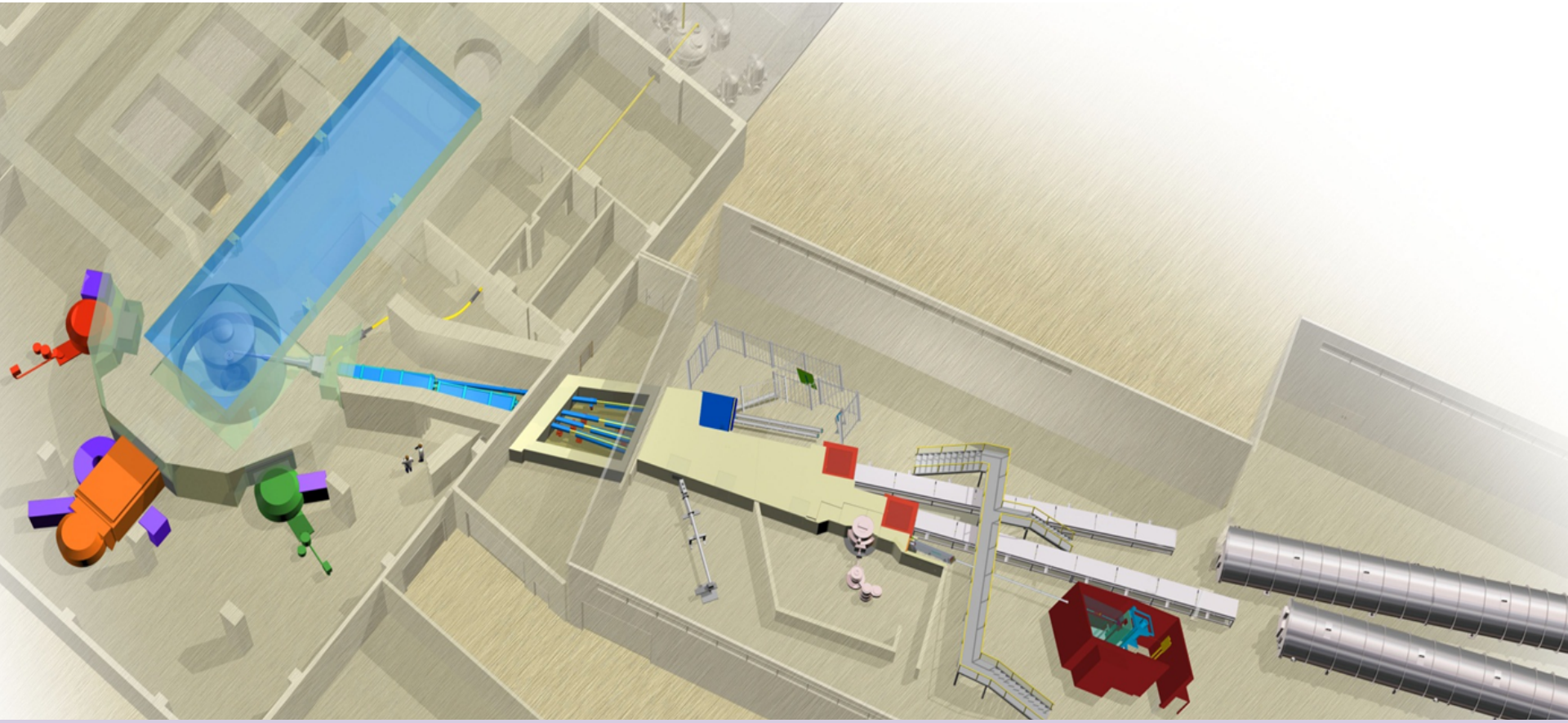

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